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BEFORE THE ARIZONA CORPORATION C

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AZ CORP COMMISSION
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COMMISSIONERS
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MIKE GLEASON
KRISTIN K. MAYES

APPLICATION FOR EXTENSION OF WATER UTILITY OF GREATER TONOPAH, INC., AN ARIZONA CORPORATION FOR AN EXTENSION OF CERTIFICATE OF ITS CONVENIENCE AND NECESSITY TO ENCOMPASS ALL OR PORTIONS OF SECTIONS 15, 17 AND 22, T2N, R5W, G&SRB&M, MARICOPA COUNTY, ARIZONA (AKA THE HASSAYAMPA RANCH DEVELOPMENT)	**DOCKET NO. W-02450A-04-0837** FILING OF SUPPLEMENTAL INFORMATION

Water Utility of Greater Tonopah, Inc. ("WUGT") this date submits supplemental information in response to the Insufficiency Letter from Jim Fisher dated December 7, 2004 filed in the above-captioned matter. The supplemental information includes a letter to Mr. Fisher dated February 4, 2005 together with Exhibits J, K, L and M. With this submittal, WUGT requests the Arizona Corporation Commission find its Application to be administratively complete and

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/ / /

Arizona Corporation Commission
DOCKETED

FEB 04 2005

DOCKETED BY

proceed with the substantive review thereof.

RESPECTFULLY SUBMITTED this 4th day of February, 2005.

CURTIS, GOODWIN, SULLIVAN,
UDALL & SCHWAB, P.L.C.

By: _____
William P. Sullivan, Esq.
2712 North Seventh Street
Phoenix, Arizona 85006-1090
Attorneys for Water Utility of Greater Tonopah, Inc.

PROOF OF AND CERTIFICATE OF MAILING

I hereby certify that on this 4th day of February, 2005, I caused the foregoing document to be served on the Arizona Corporation Commission by delivering the original and thirteen (13) copies of the above to:

Docket Control
Arizona Corporation Commission
1200 West Washington
Phoenix, Arizona 85007

_____

1284/5-3-1/pleadings/supplemental filing

The Law Offices of
CURTIS, GOODWIN, SULLIVAN, UDALL & SCHWAB, P.L.C.
2712 North Seventh Street
Phoenix, Arizona 85006-1090
Telephone (602) 393-1700
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Anja K. Wendel
K. Russell Romney
Ellen M. Van Riper

Of Counsel
Joseph F. Abate
Thomas A. Hine

REFER TO FILE NO. 1284-5-3-2

February 4, 2005

Hand Delivered

Mr. Jim Fisher
Arizona Corporation Commission
1200 West Washington Street
Phoenix, Arizona 85007

Re: **Water Utility of Greater Tonopah, Inc. – Application for an Extension of CC&N Docket No. W-02450A-04-0837**

Dear Jim:

Our office represents Water Utility of Greater Tonopah, Inc. ("WUGT"). We are submitting this letter and the attachments in response to your Insufficiency Letter dated December 7, 2004. Thank you for your comprehensive review of the filing. WUGT's response is as follows:

1. Please provide a request for service from each of the affected property owners.

   A copy of the request for service from the project developer (HRP) was attached as Exhibit F to the Application. Attached hereto as Exhibit J is the Authorization of the landowner permitting the project developer to request water service.

2. Please provide a map of the requested service territory with an identification of the respective property owners requesting service.

   A map of the requested service territory was attached to the Application as Exhibits D and E. As reflected in the application, the service territory is being developed as a single development by HRP. WUGT has been informed that Algene Venture, an Arizona joint venture and PNR Southwest Partnership, an Illinois general partnership, currently own all of the service territory, but have agreed to sell all of it to HRP. WUGT does not know exactly how the land is divided, if at all, between Algene Venture and PNR Southwest

Partnership.

3. Please provide a map of the requested territory in relation to the existing utility's existing service area.

   The requested map is attached as Exhibit K.

4. Please provide a drinking water design report which clarifies how water will be provided to the proposed CC&N.

   WUGT is having the necessary copies of the Hassayampa Ranch Concept Plan and Analysis of Assured Water Supply study attached hereto as Exhibits L and M respectively.

5. Please provide a copy of the Arizona Department of Water Resources Analysis of Adequate Water Supply for the proposed service territory.

   The Arizona Department of Water Resources is still reviewing the application for an Analysis of Assured Water Supply submitted on behalf of Hassayampa Ranch. WUGT will submit the Department's determination when it becomes available. A copy of the Analysis of Assured Water Supply submitted to HRP is attached hereto as Exhibit M.

6. Please provide any other information which will allow the Commission to analyze and conclude that the company has sufficient water production capacity, or can develop enough drinking water capacity to service the existing and future demands from the proposed CC&N.

   The information listed in response to item 4 is believed sufficient to allow the Commission to analyze and conclude that WUGT has sufficient water production capacity, or can develop enough drinking water capacity to service the existing and future demands from the proposed CC&N. The ultimate determination of the question is a substantive decision and is beyond the scope of an administrative sufficiency review.

7. Please provide a set of design plans for the proposed water facilities.

   The conceptual water plans prepared by HRP is attached as Exhibit L. Final design of the facilities necessary to provide water service to the area will be performed by the developer to WUGT's specifications and in consultation with WUGT. Such plans will be submitted in conjunction with Line Extension Agreements, as they are executed.

8. Please provide an estimate of the water facilities costs to WUGT necessary to serve the proposed CC&N extension

   The Engineer's Opinion of Preliminary Costs was provided as Exhibit H to the Application. Estimates associated with two other optional configurations are included in

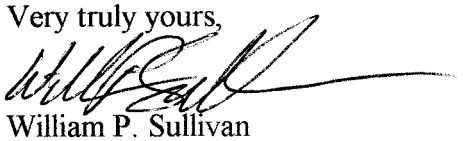
Exhibit L attached hereto. These estimates will be refined in conjunction with the planning of actual developments and the execution of Line Extension Agreements. The financing of water facilities will be negotiated with developers, but will consist primarily of Advances-in-Aid-of-Construction.

9. Please provide a copy of the Municipal Franchise for the requested area.

No Municipal Franchise is currently needed. As noted in Paragraph 18 of the Application WUGT is in the process of making application for Maricopa County Franchise and will submit a copy as soon as it becomes available. A.R.S. §40-282.D. also authorizes the Commission to issue an order preliminary to the issuance of a CC&N if the franchise has not yet been granted.

We trust that with this supplemental filing, the Commission will now be able to finalize its administrative completeness review and commence its substantive review. If you have any questions regarding the information being provided or if there is any additional information that you require, please do not hesitate to contact me. If the question is of a technical nature, please feel free to contact J. John Mihlik at (602) 224-0771. Again, thank you for your efforts in reviewing WUGT's Application.

Very truly yours,



William P. Sullivan
For the Firm

WPS/mw
Enclosures: As noted above

1284/-5-3-1/letters/Jfisher (Response to Insufficiency)

EXHIBIT J

AUTHORIZATIONS

(WATER UTILITY SERVICE AND WASTEWATER UTILITY SERVICE)

To Whom It May Concern:

Algene Venture, an Arizona joint venture, and PNR Southwest Partnership, an Illinois general partnership (collectively, "Seller"), and Harvard Investments, Inc., a Nevada corporation ("Buyer"), have previously entered into that certain Purchase and Sale Agreement dated October 14, 2004 (the "Purchase Agreement"), pursuant to which Seller has agreed to sell and Buyer has agreed to purchase that certain real property located in Maricopa County, Arizona more particularly described on Exhibit "A" attached hereto and incorporated herein by reference (the "Property"), establishing First American Title Insurance Company Escrow No. 773-111755-PHX3.

Seller hereby authorizes and consents to Buyer's undertaking the following actions:

1. Enter into a Line Extension Agreement and related agreements with Water Utility of Greater Tonopah to provide water utility service to the Property, including construction of necessary water facilities, and to submit such materials, provide such information, and do such things as may be necessary or reasonable in connection therewith.

2. Enter into an Advance In Aid of Construction Agreement and related agreements with Water Utility of Greater Tonopah to provide water utility service to the Property, including construction of necessary off-site improvements for water services, and to submit such materials, provide such information, and do such things as may be necessary or reasonable in connection therewith.

3. Enter into a Line/Main Extension Agreement and related agreements with Global Water Management LLC and/or a related entity to provide wastewater utility service to the Property, including construction of necessary wastewater facilities, and to submit such materials, provide such information, and do such things as may be necessary or reasonable in connection therewith.

4. Request and authorize Water Utility of Greater Tonopah and Global Water Management LLC to file applications with the Arizona Corporation Commission to extend their respective Certificates of Convenience and Necessity to provide water and wastewater public utility service to the Property, and to submit such materials, provide such information, and do such things as may be necessary or reasonable in connection therewith.

DATED this 12 day of November, 2004.

ALGENE VENTURE,
an Arizona joint venture

By: SEF/WEST Venture,
an Illinois general partnership,
a general partner

By: The Eugene Freeman Family Limited Partnership,
an Illinois limited partnership,
its general partner

By: Eugene Freedman Revocable Trust under a
Restated Trust Agreement dated October 31, 1996,
its general partner

By: _____
Eugene Freedman, Trustee

By: PNR Southwest Partnership,
an Illinois general partnership,
a general partner

By: Richard Freedman Trust,
under at Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

By: Penny Freedman Trust,
under a Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

By: Nancy Freedman Remak Trust,
under a Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

PNR SOUTHWEST PARTNERSHIP,
an Illinois general partnership

By: Richard Freedman Trust,
under at Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

By: Penny Freedman Trust,
under a Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

By: Nancy Freedman Remak Trust,
under a Trust Agreement dated 1/6/83

By: _____
Gerald A. Weber, Trustee

EXHIBIT K

WATER UTILITY OF GREATER TONOPAH, INC.
DOCKET NO. W-2450-04-837

COUNTY: *Maricopa*

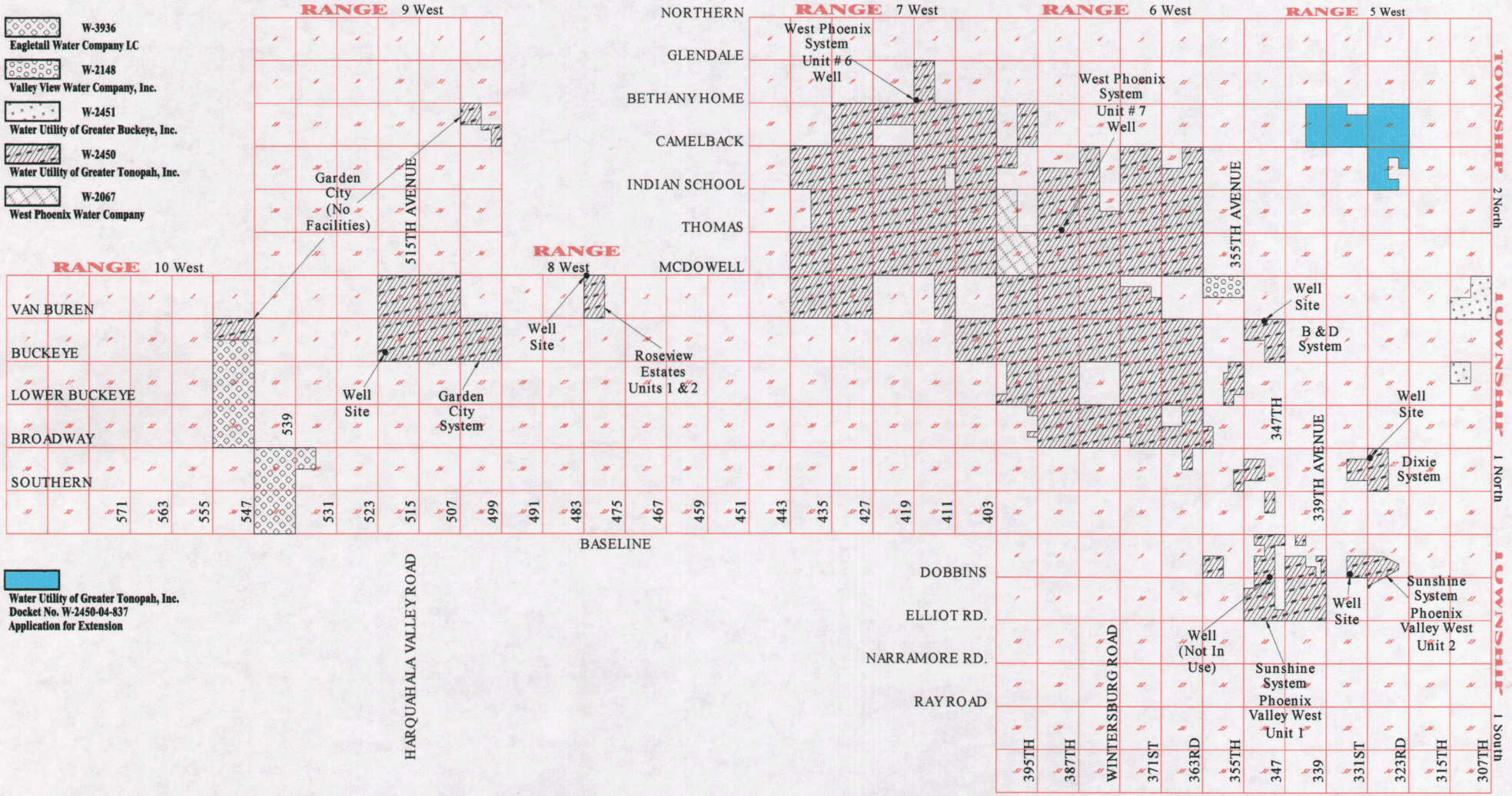


EXHIBIT L

HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPTUAL DEVELOPMENT PLAN

PROJECT DESCRIPTION

The proposed Hassayampa Ranch masterplanned community is comprised of approximately 2050 total acres. The property is located in Maricopa County, Arizona, between 323rd and 343rd avenues, two and one half miles north of Interstate 10. Bethany Home Road is the northern boundary for the site and Camelback Road will bisect the Property, which stretches south to Indian School Road. Project entries are proposed at 339th Avenue and Camelback Road and 331st Avenue and Indian School Road.

The property is being acquired for cash at $13,000 per net acre or an estimated total purchase price of $26,000,000. The purchase agreement permits a 60 day feasibility period followed by a close of escrow 60 days later. The buyer has the right to extend the close of escrow for two 30 day periods by payment of a small fee ($35,000) for each thirty days requested. The payments would not apply to the purchase price. There are two conceptual land plans for the project, the first offering four distinct masterplans aggregating almost 6,000 residential units. While the plan is being designed as a cohesive masterplan, the property can be divided into four sub phases as part of one business model exit strategy. The second conceptual land plan includes almost 5,500 total residential units, of which approximately 2500 units will belong to an active adult village. A golf course and clubhouse, totaling 258 acres, will highlight the active adult community. An additional 279 acres are designated for open space and there is a school site proposed for the family portion of the community. Commercial parcels located along Camelback Road at 331st and 339th avenues total about 59.5-acres.

The initial phase of the project is expected to attract entry-level buyers, value-oriented families and retirees. The amenity package, for both the active adult and family portions of the master plan, will be significant in order to persuade buyers to tolerate longer commute times to the Property. Given the Property's location and access and the number of competitors anticipated to enter the marketplace east of the subject within the Buckeye town limits, we expect low base prices and family-friendly amenities to be the overriding draws to attracting buyers. The non-age restricted portion of Hassayampa Ranch would include landscaped greenbelts, a network of parks and sporting fields, and a community center with a complete spectrum of fitness facilities, lounge area, meeting rooms and an aquatics facility combining a resort-style pool, lap swimming and children's play pool.

Harvard Investments

ARIZONA LAND ADVISORS

LEGEND

Roads

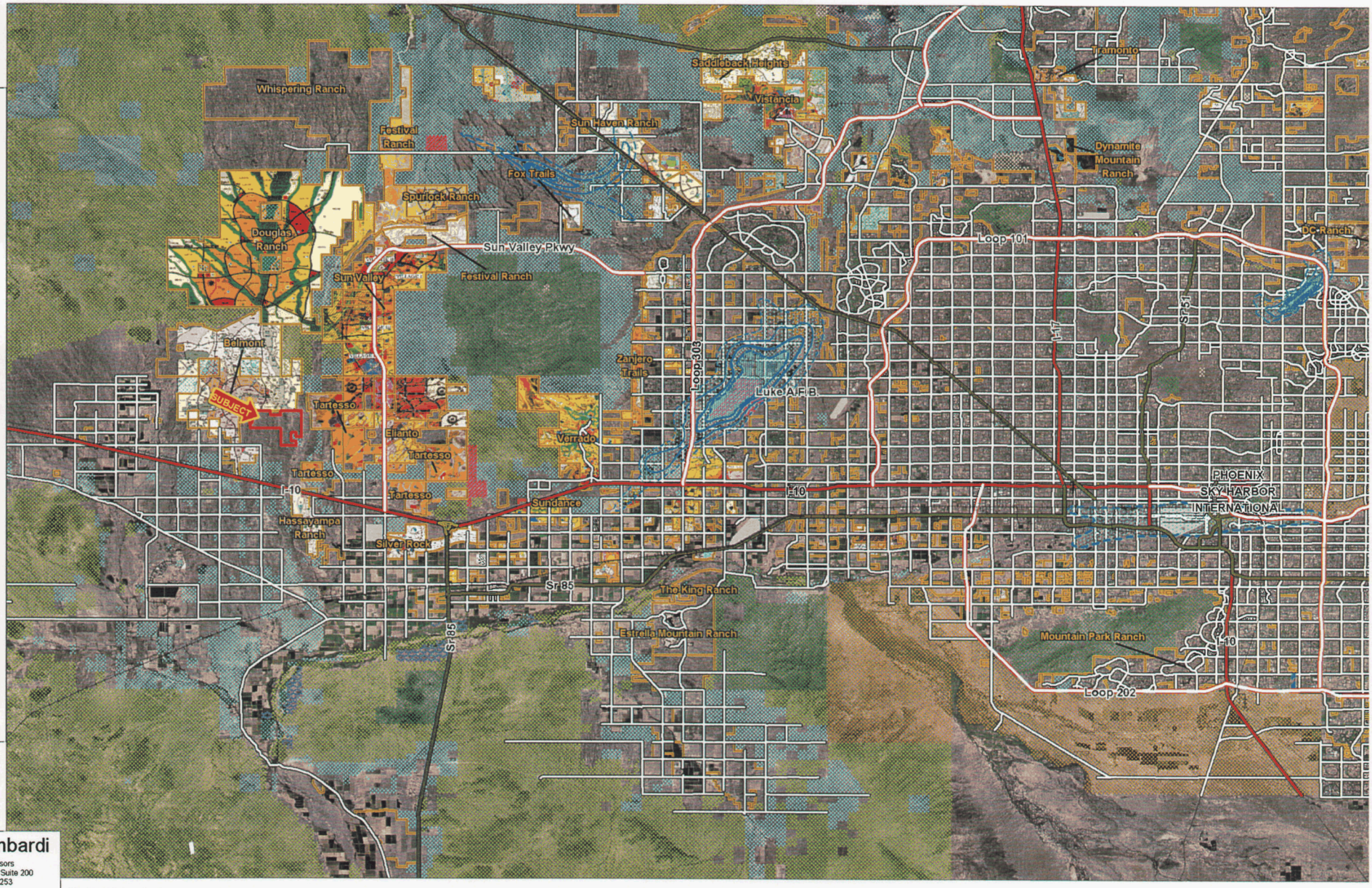
- US Highway
- Interstate
- US Highway
- Loop
- Railroads
- Airports
- Noise Contours

MPC

- Projects

Governmental Ownership

- State Trust
- BLM
- Military



NORTH

ARIZONA LAND ADVISORS

Vogel/Lombardi

Arizona Land Advisors
6710 N. Scottsdale Rd., Suite 200
Scottsdale, AZ 85253
480.483.8100
www.landadvisors.com

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The information contained here is from sources deemed reliable. We have no reason to doubt its accuracy but do not guarantee it. It is the responsibility of the person reviewing this information to independently verify it.

Harvard Investments

ARIZONA LAND ADVISORS

LEGEND

Roads by Type

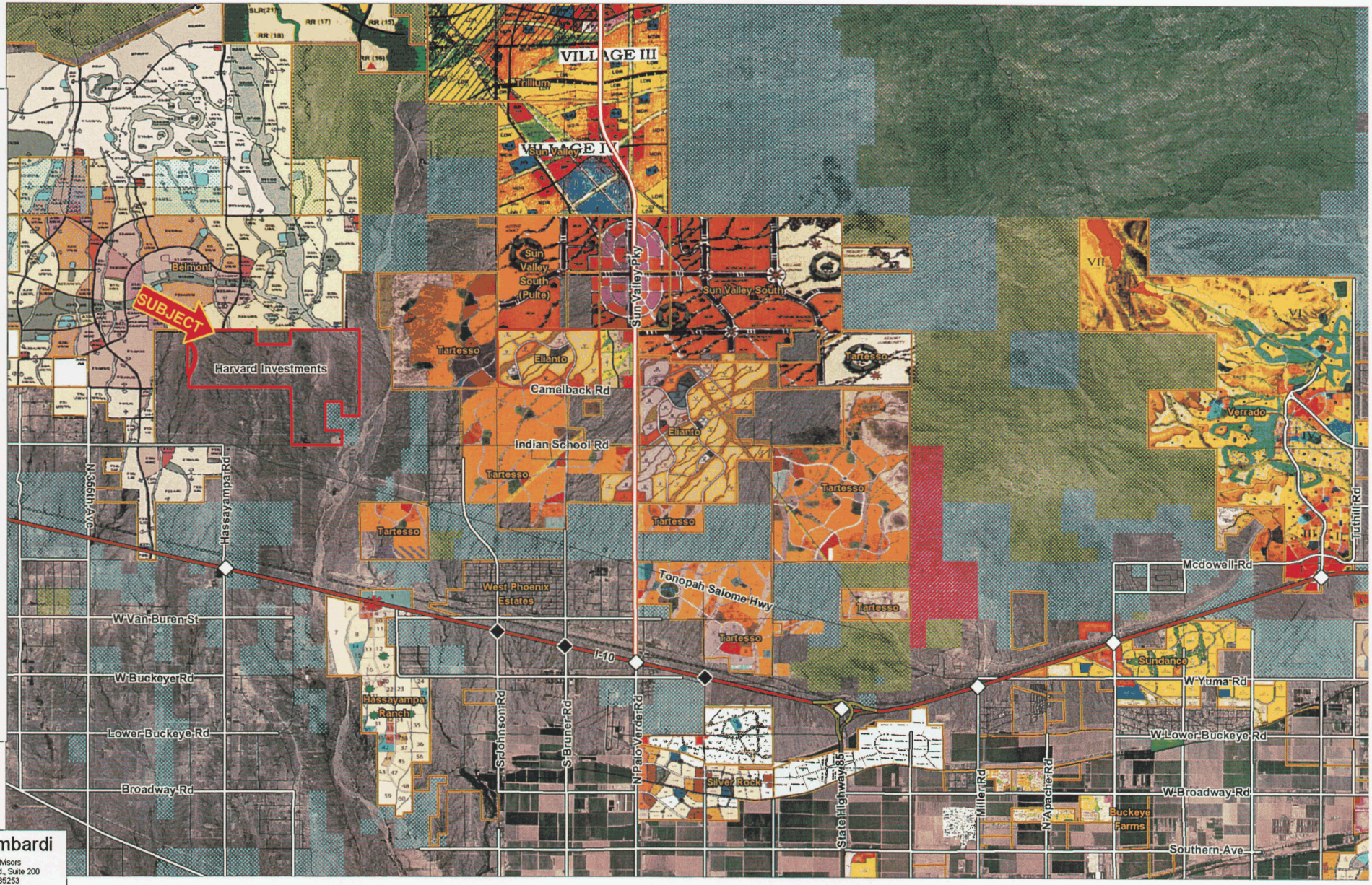
- Arterial
- Highway
- Interstate
- Loop
- Streets

MPC

- Project

Governmental Ownership

- State Trust
- Private
- BLM
- Military



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Concept Plan 1

Harvard Investments

Hassayampa Ranch

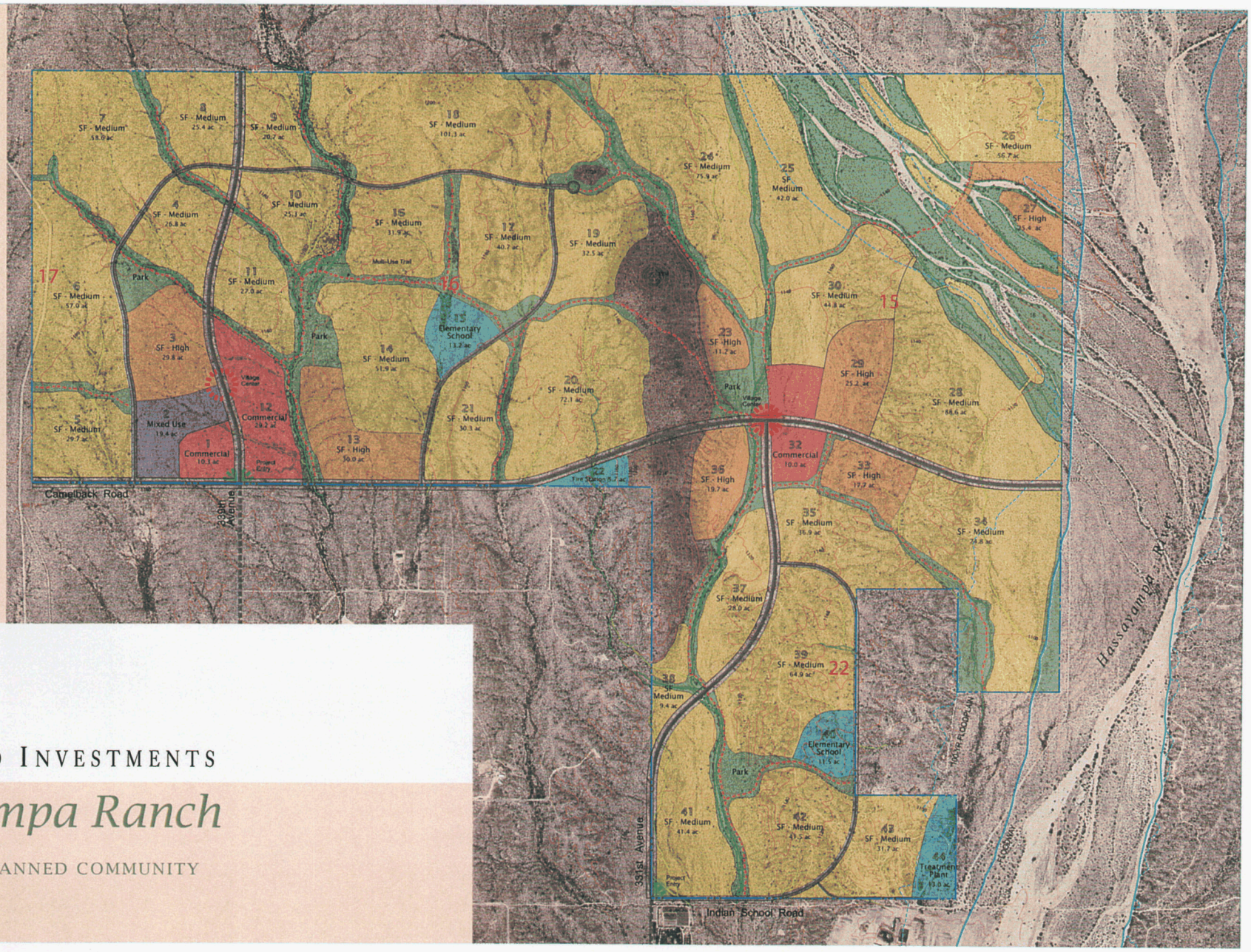
Concept Plan 1

Land Use Allocation

Use	Area, ac
Commercial	59.5
Mixed Use	19.4
Residential	1401.4
Schools	24.7
Public	18.7
Open Space	451.5
Roadways	91.4
Total	2066.6

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	1267.8	4.0	5071
Single Family High Density	133.6	7.0	935
Total	1249.0		6006



HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
CONVENTIONAL PLANNED COMMUNITY

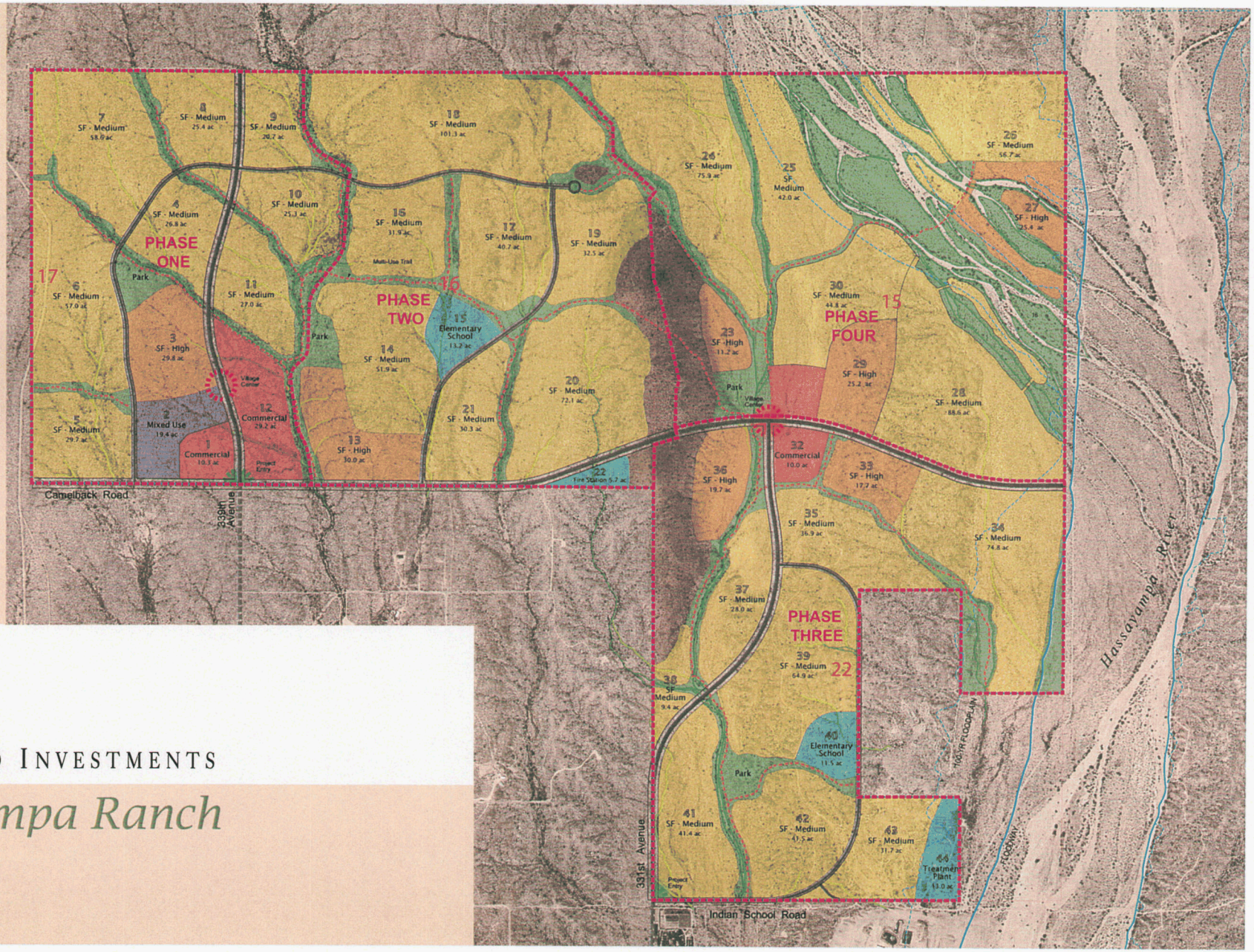
0 300 600 1200

Land Use Allocation

Use	Area, ac
Commercial	59.5
Mixed Use	19.4
Residential	1401.4
Schools	24.7
Public	18.7
Open Space	451.5
Roadways	91.4
Total	2066.6

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	1267.8	4.0	5071
Single Family High Density	133.6	7.0	935
Total	1249.0		6006

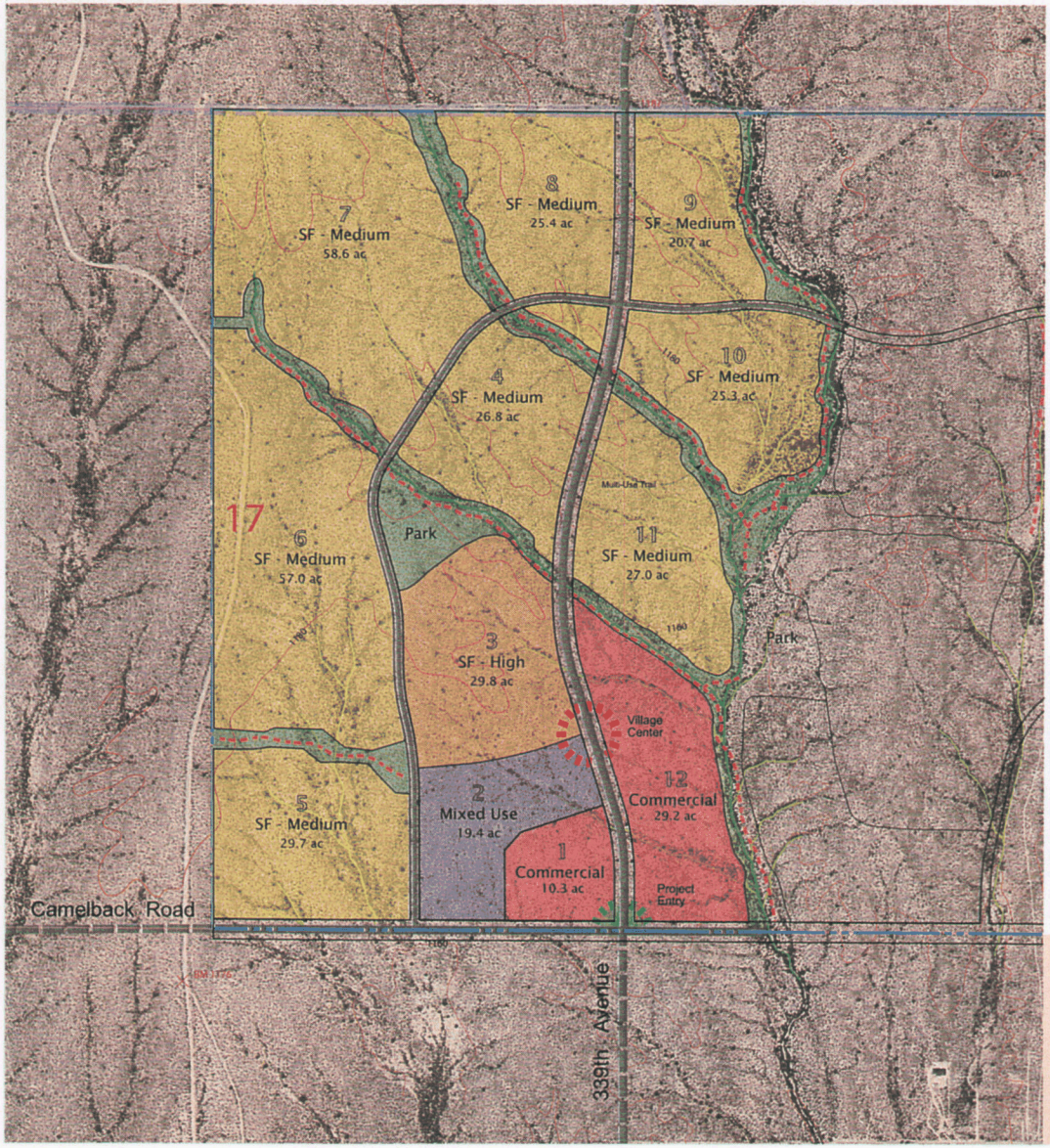


HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
PHASING PLAN

0 300 600 1200



Land Use Allocation

Use	Area, ac
Commercial	39.5
Mixed Use	19.4
Residential	300.3
Open Space	47.1
Roadways	29.9
Total	436.2

Residential Data

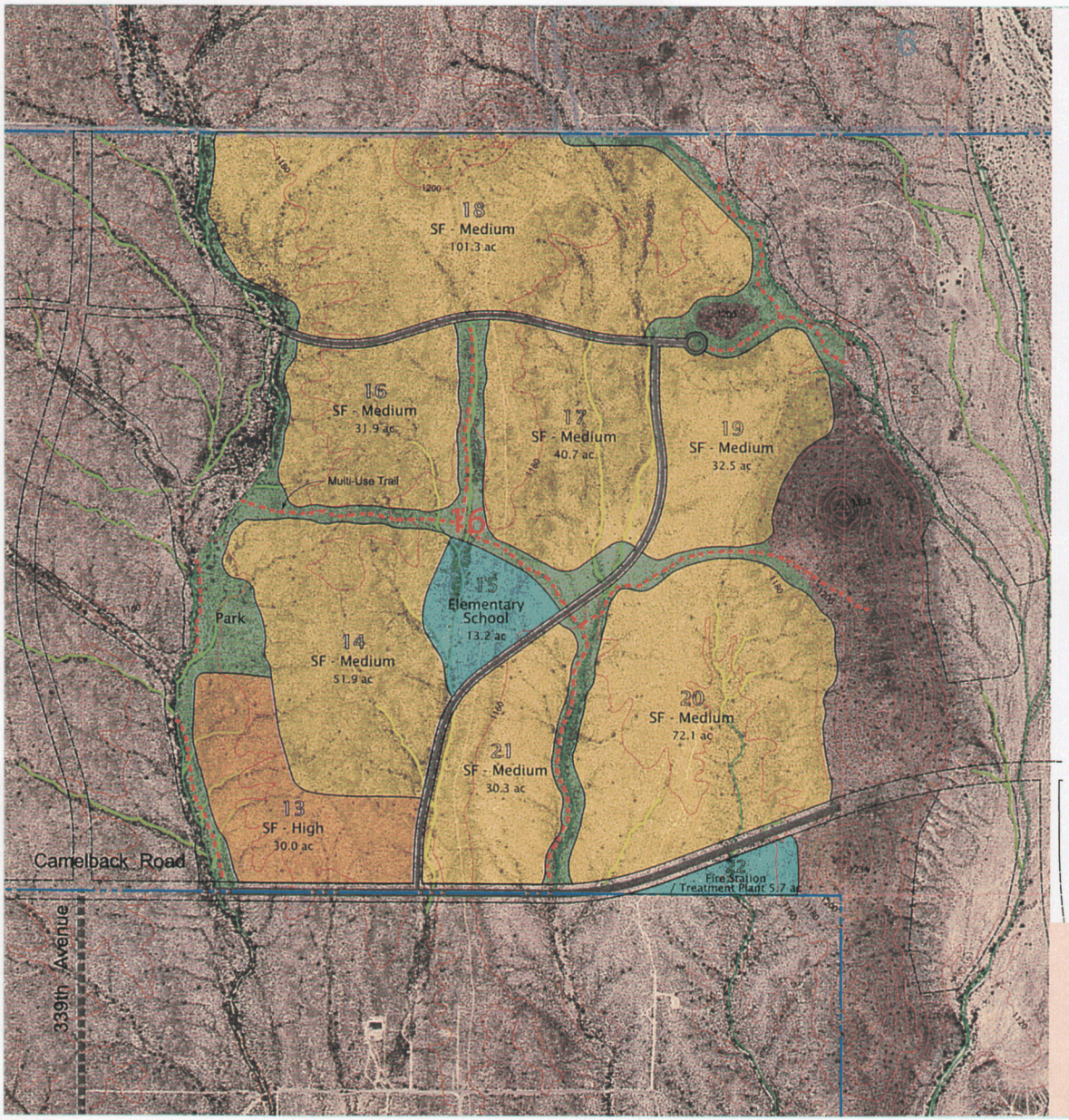
Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	270.5	4.0	1082
Single Family High Density	29.8	7.0	208
Total	300.3		1290

HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
PHASE ONE PRELIMINARY DEVELOPMENT PLAN

0 200 400 800



Land Use Allocation

Use	Area, ac
Residential	390.7
Schools	13.2
Public	5.7
Open Space	84.0
Roadways	19.7
Total	513.3

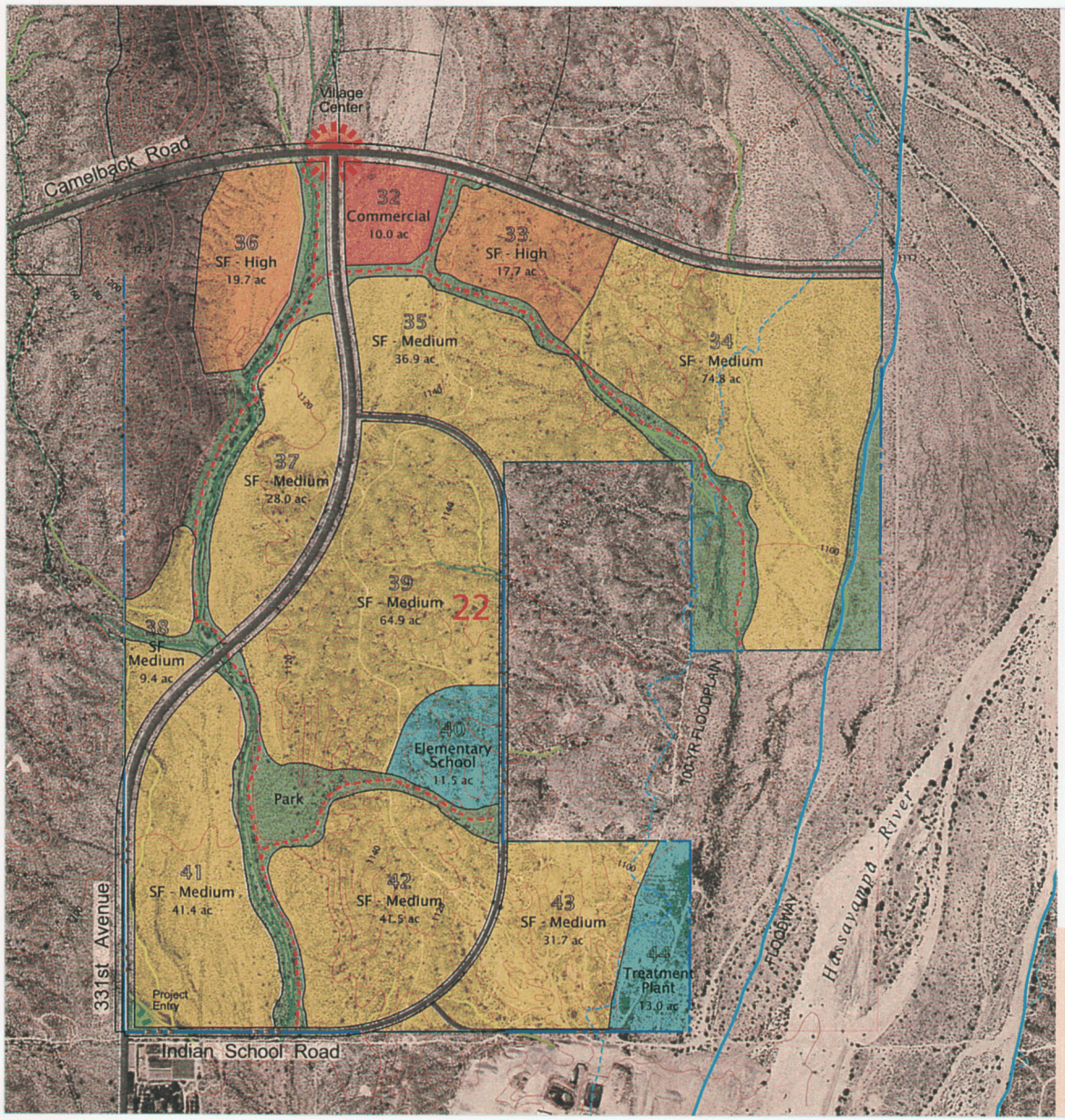
Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	360.7	4.0	1442
Single Family High Density	30.0	7.0	210
Total	390.7		1652

Hassayampa Ranch

CONCEPT ONE
PHASE TWO PRELIMINARY DEVELOPMENT PLAN

0 200 400 800



Land Use Allocation

Use	Area, ac
Commercial	10.0
Residential	366.0
Schools	11.5
Public	13.0
Open Space	95.8
Roadways	41.7
Total	538.0

Residential Data

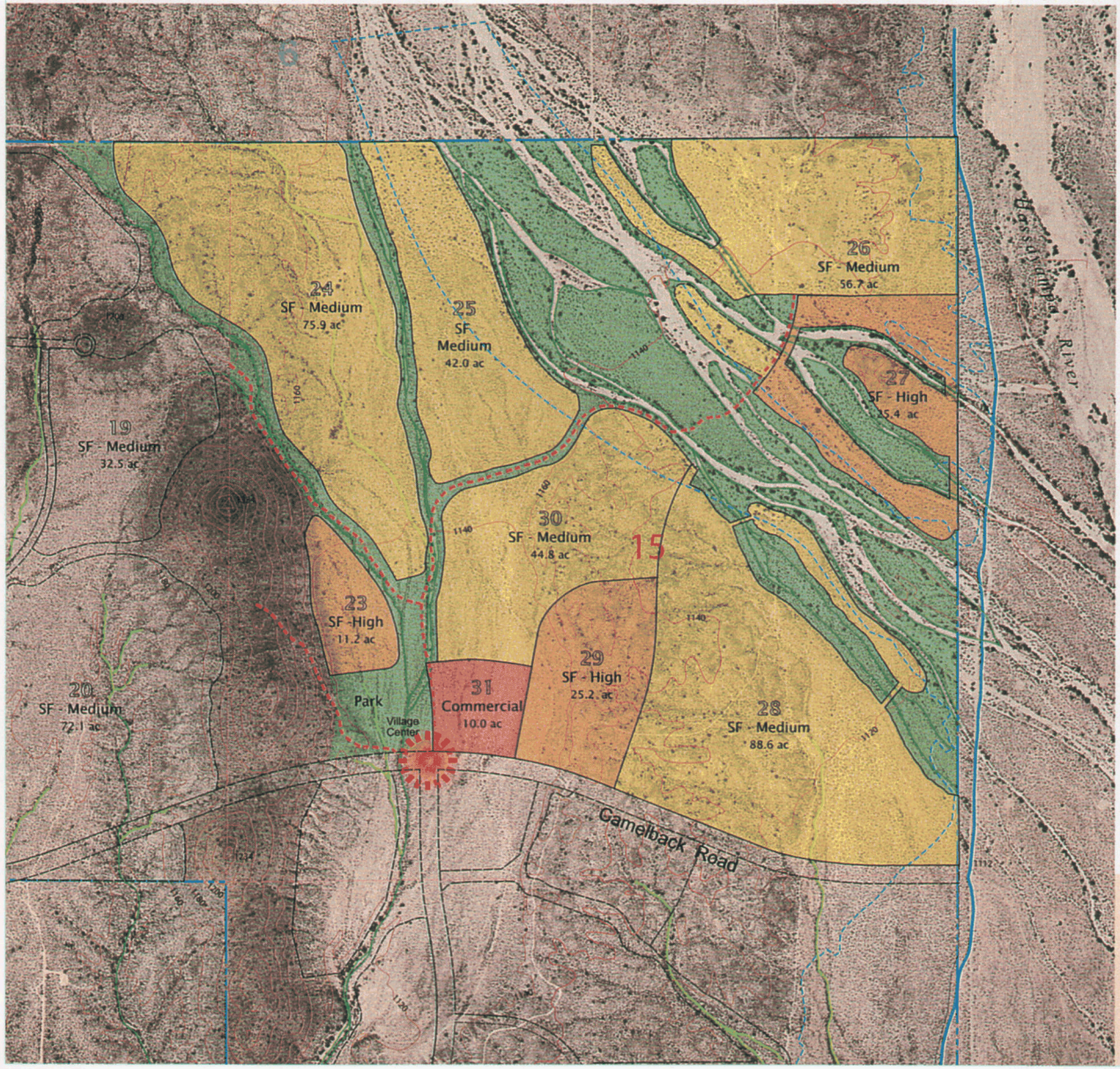
Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	328.6	4.0	1314
Single Family High Density	37.4	7.0	261
Total	366.0		1575

HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
PHASE THREE PRELIMINARY DEVELOPMENT PLAN

0 200 400 800



Land Use Allocation

Use	Area, ac
Commercial	10.0
Residential	369.8
Open Space	199.2
Total	579.0

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	308.0	4.0	1232
Single Family High Density	61.8	7.0	432
Total	369.8		1664

HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
PHASE FOUR PRELIMINARY DEVELOPMENT PLAN

0 200 400 800

CONCEPT PLAN 2

HARVARD INVESTMENTS

Hassayampa Ranch

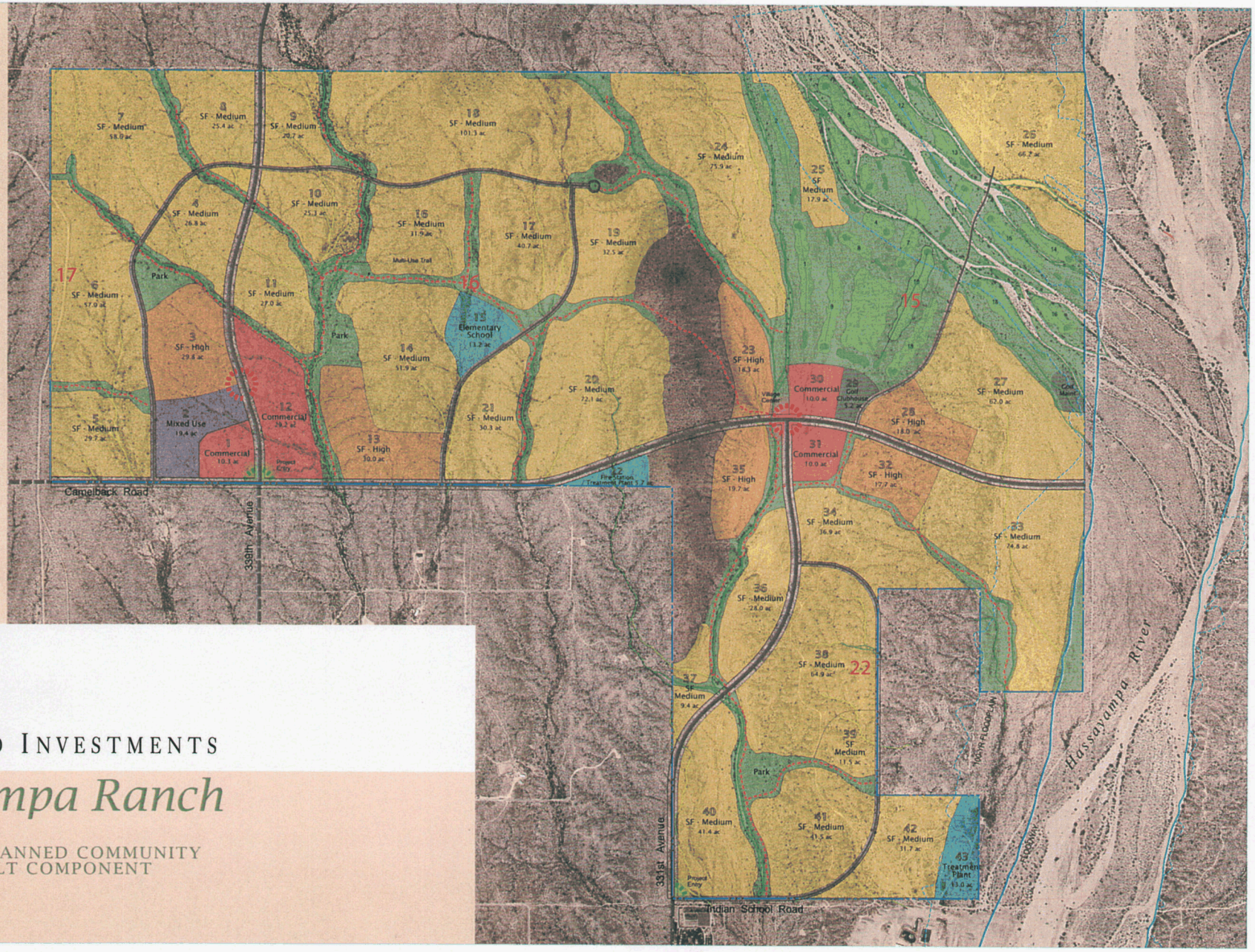
Land Use Allocation

	Area, ac
Commercial	59.5
Mixed Use	19.4
Residential	1326.8
Schools	13.2
Public	18.7
Golf	258.4
Open Space	279.2
Roadways	91.4
Total	2066.6

*Includes Golf Club

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	1193.3	4.0	4773
Single Family High Density	133.5	7.0	934
Total	1326.8		5707



HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT TWO
CONVENTIONAL PLANNED COMMUNITY
WITH ACTIVE ADULT COMPONENT

0 300 600 1200

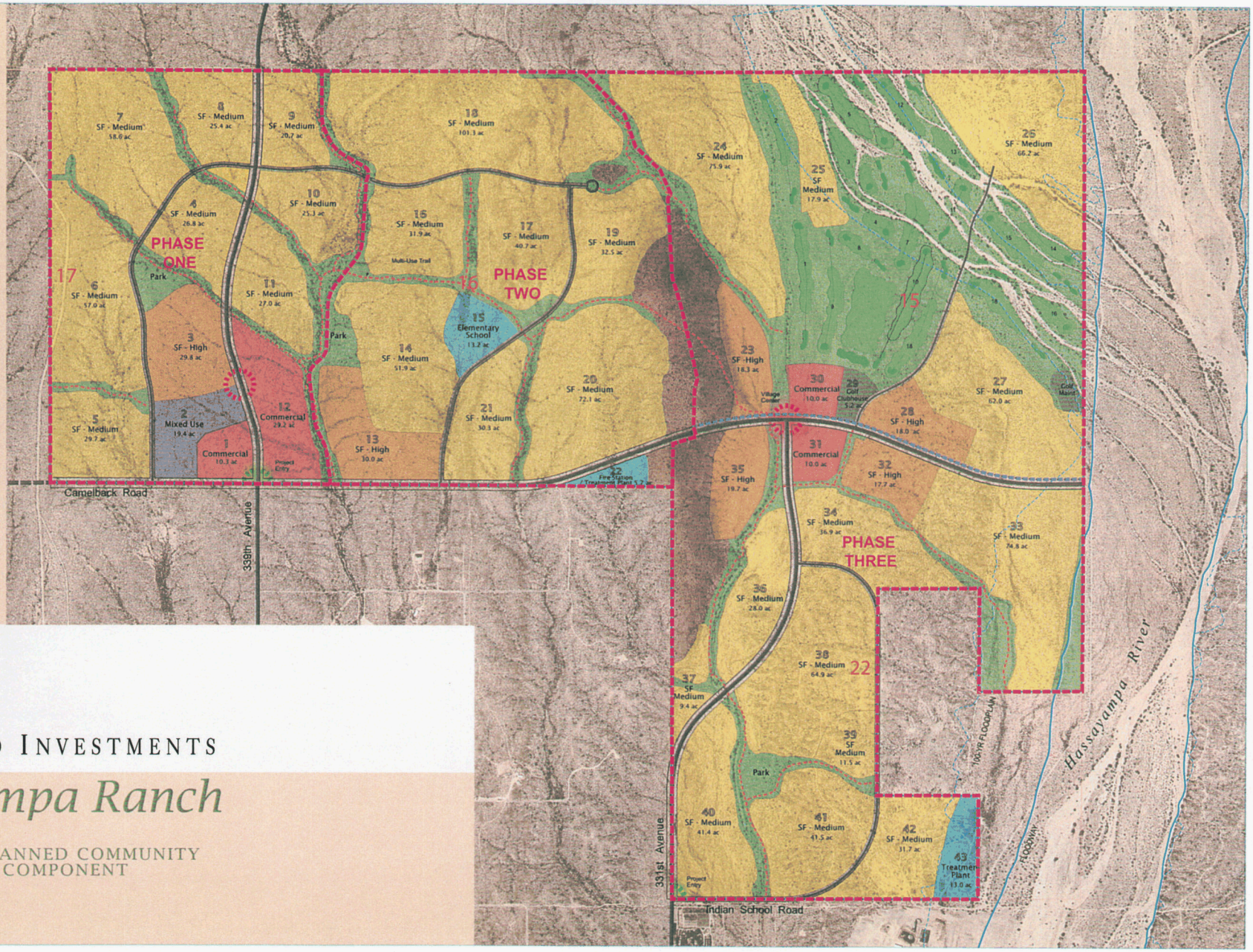
Land Use Allocation

	Area, ac
Commercial	59.5
Mixed Use	19.4
Residential	1326.8
Schools	13.2
Public	18.7
Golf	258.4
Open Space	279.2
Roadways	91.4
Total	2066.6

*Includes Golf Club

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	1193.3	4.0	4773
Single Family High Density	133.5	7.0	934
Total	1326.8		5707

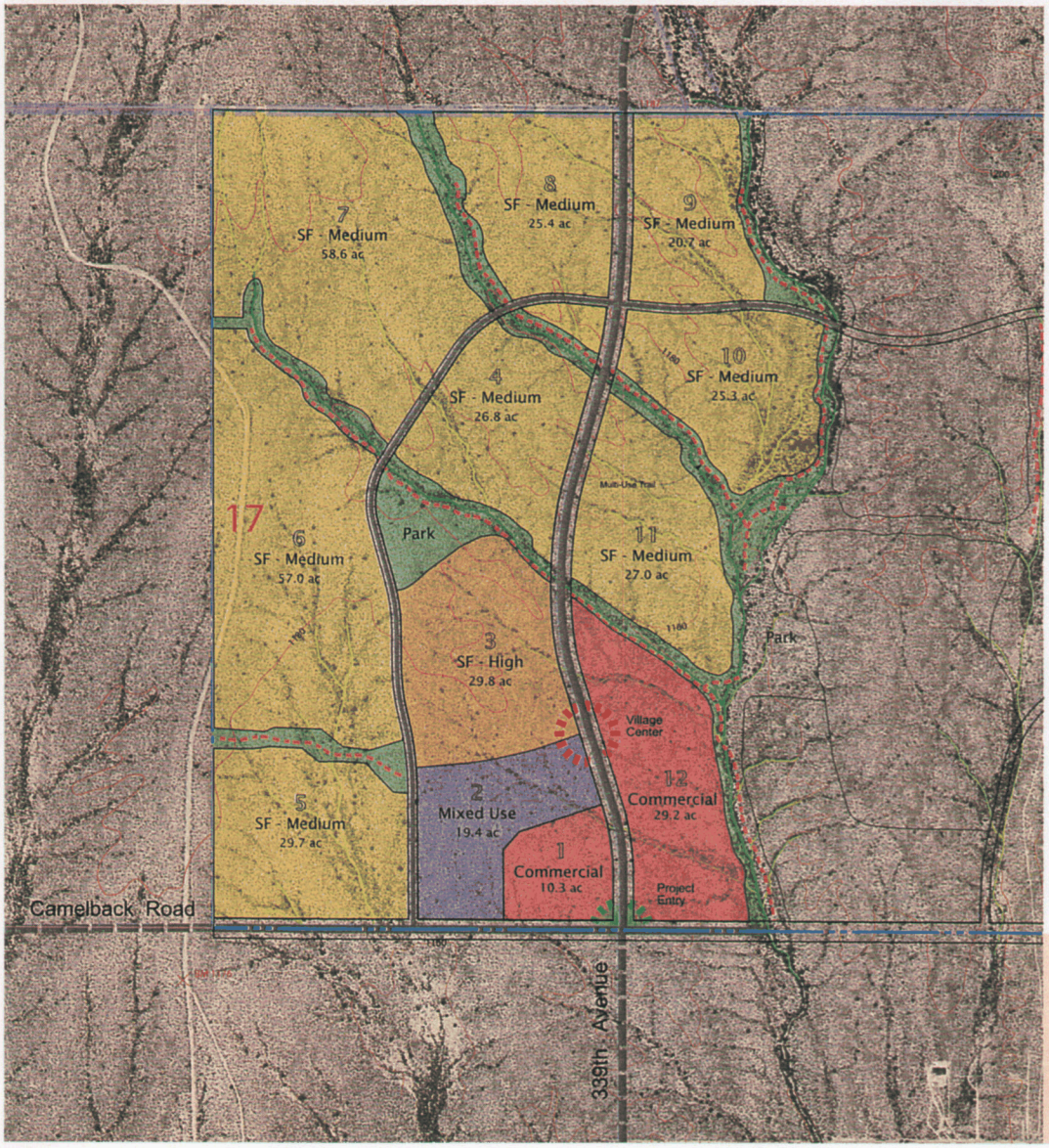


HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT TWO
CONVENTIONAL PLANNED COMMUNITY
WITH RETIREMENT COMPONENT

0 300 600 1200



Land Use Allocation

Use	Area, ac
Commercial	39.5
Mixed Use	19.4
Residential	300.3
Open Space	47.1
Roadways	29.9
Total	436.2

Residential Data

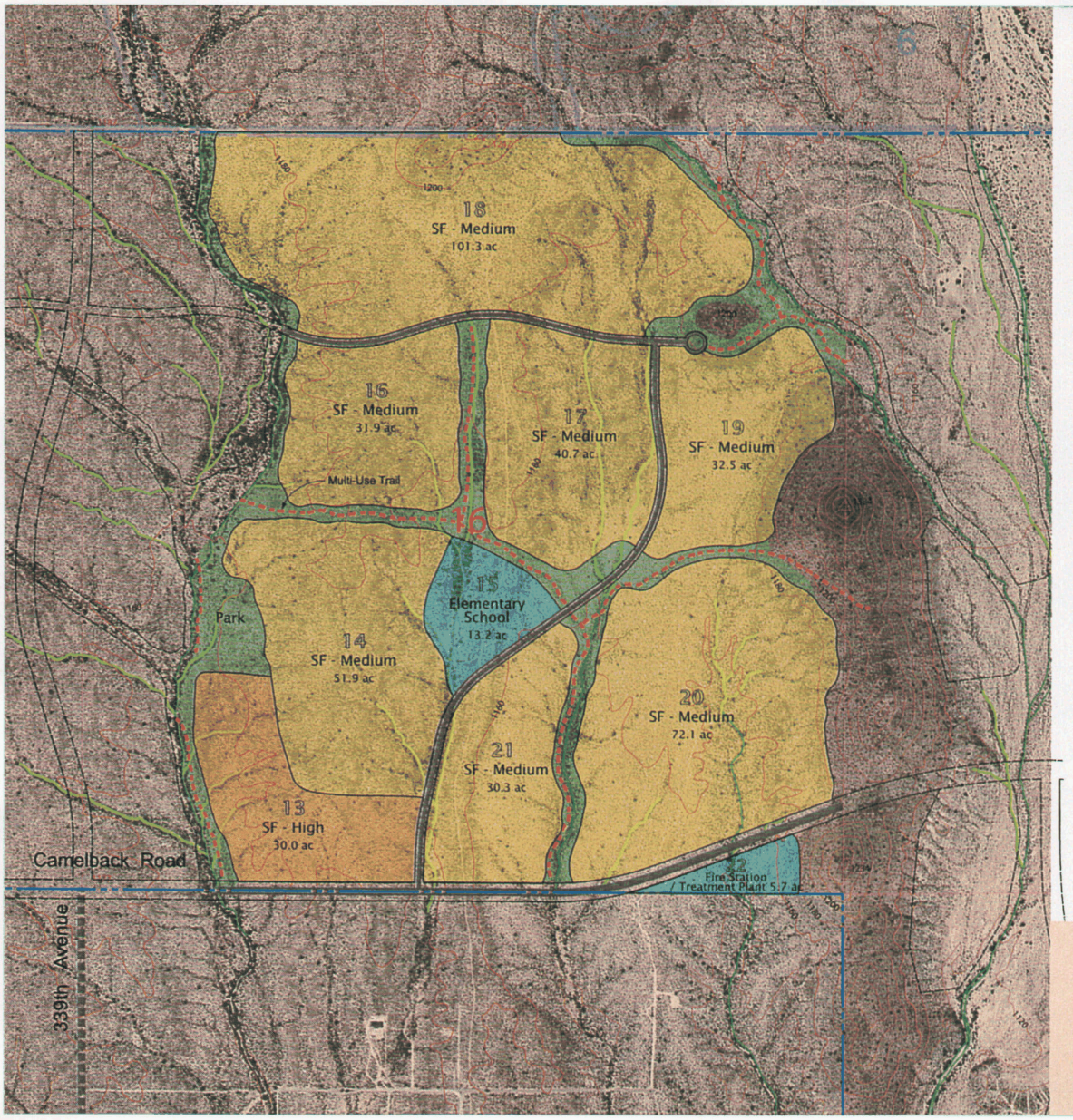
Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	270.5	4.0	1082
Single Family High Density	29.8	7.0	208
Total	300.3		1290

HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT TWO
PHASE ONE PRELIMINARY DEVELOPMENT PLAN

0 200 400 800



Land Use Allocation

Use	Area, ac
Residential	390.7
Schools	13.2
Public	5.7
Open Space	84.0
Roadways	19.7
Total	513.3

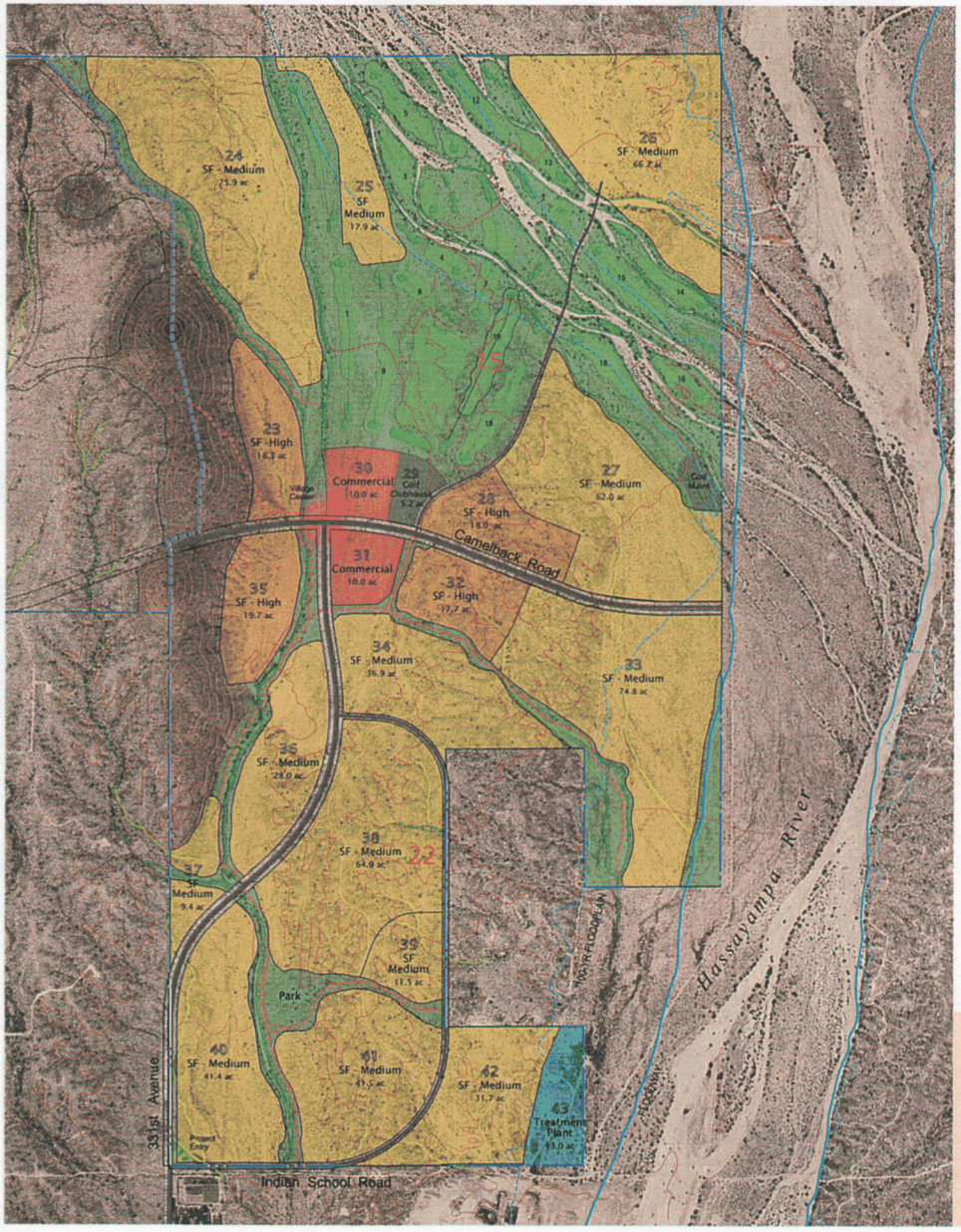
Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	360.7	4.0	1442
Single Family High Density	30.0	7.0	210
Total	390.7		1652

Hassayampa Ranch

CONCEPT TWO
PHASE TWO PRELIMINARY DEVELOPMENT PLAN

0 200 400 800



Land Use Allocation

Use	Area, ac
Commercial	20.0
Residential	635.7
Public	13.0
Golf Course	258.4
Open Space	147.2
Roadways	42.7
Total	1117.1

Residential Data

Use	Area, ac	DU/ ac	No. of Lots
Single Family Medium Density	562.1	4.0	2248
Single Family High Density	73.7	7.0	515
Total	635.8		2763

HARVARD INVESTMENTS

Hassayampa Ranch

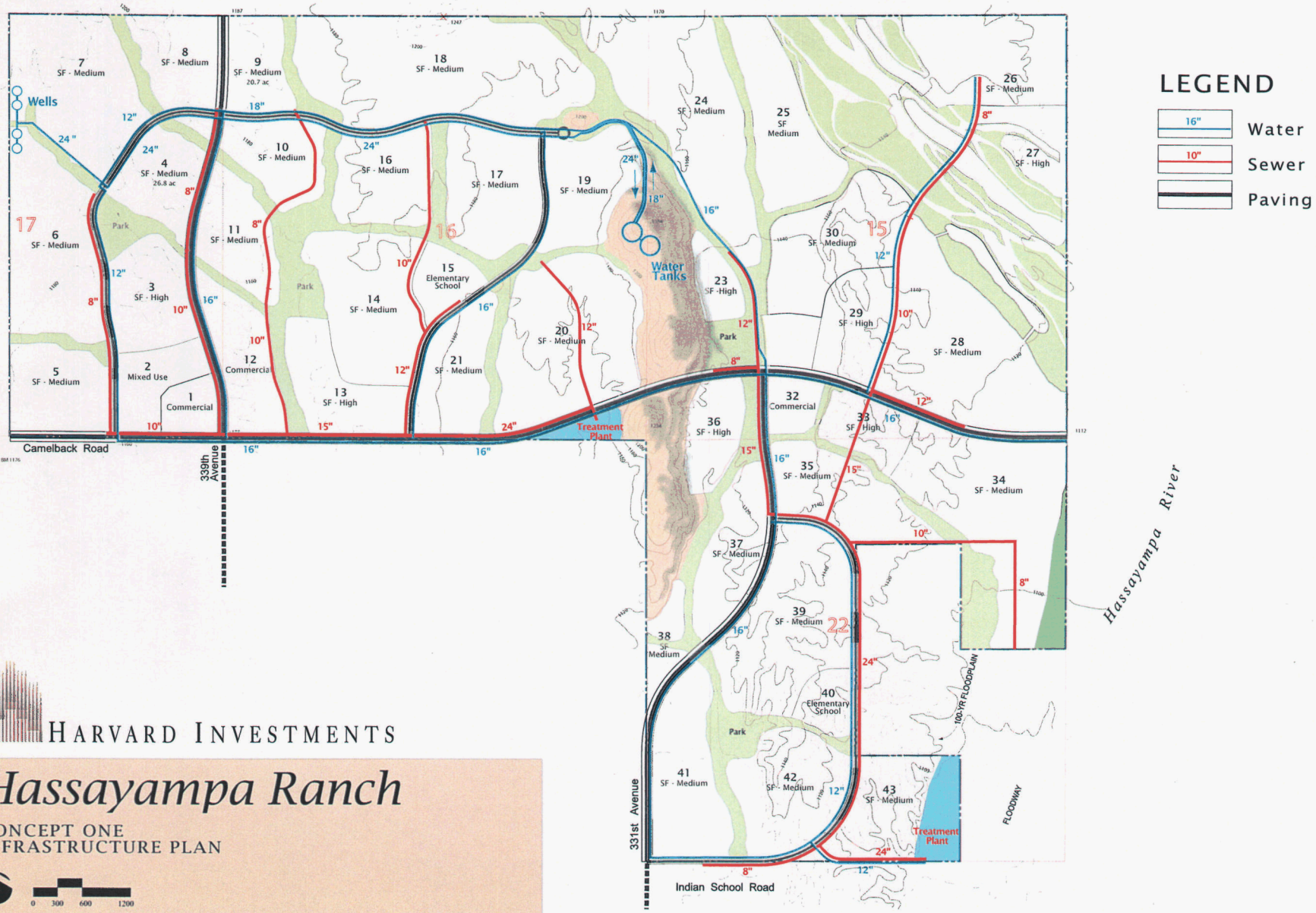
CONCEPT TWO
PHASE THREE PRELIMINARY DEVELOPMENT PLAN

0 300 600 1200

CONCEPT 1
INFRASTRUCTURE

HARVARD INVESTMENTS

Hassayampa Ranch

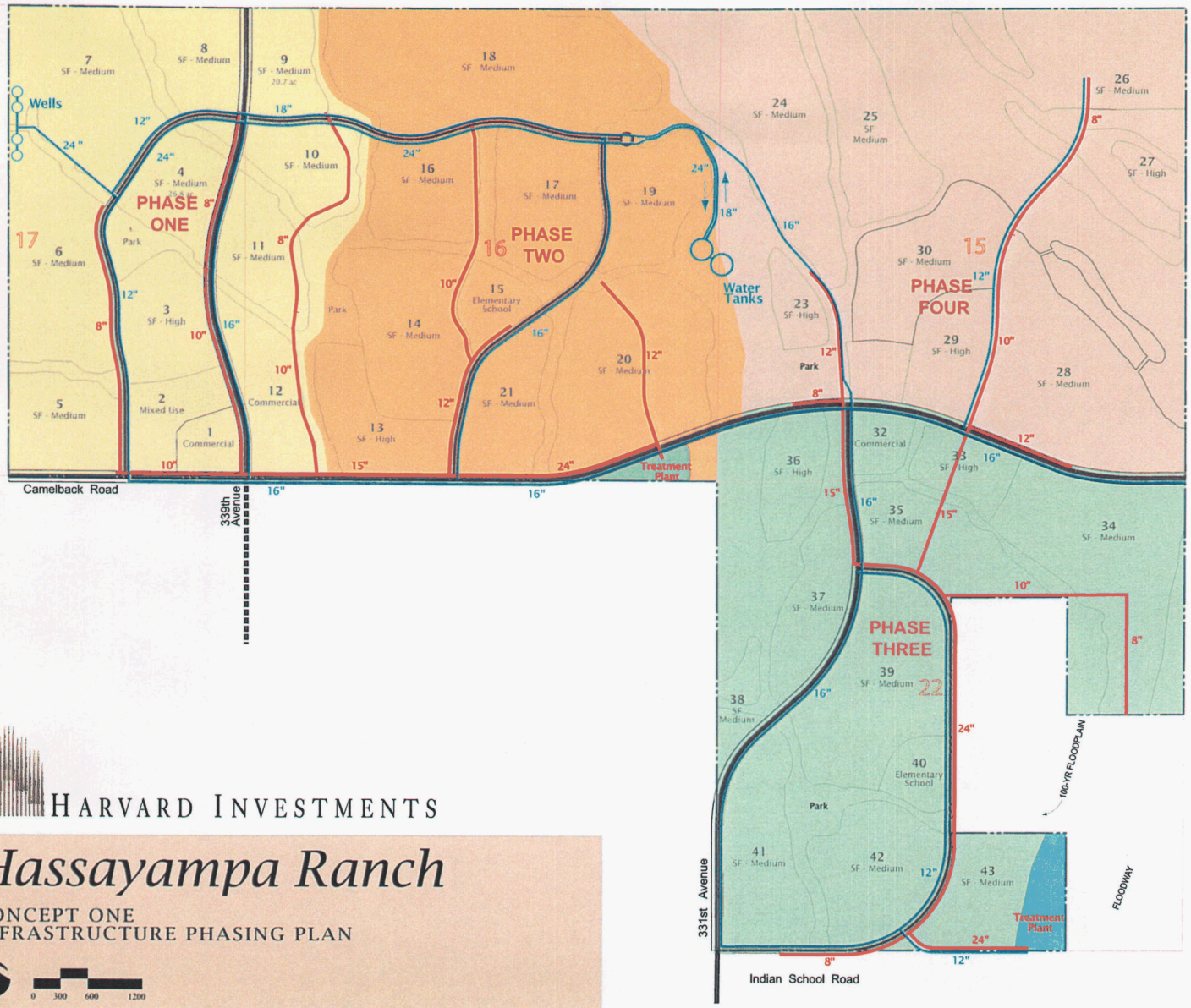


HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
INFRASTRUCTURE PLAN

0 300 600 1200



HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT ONE
INFRASTRUCTURE PHASING PLAN

0 300 600 1200

WRG DESIGN, INC.

PLANNERS * CIVIL ENGINEERS * LANDSCAPE ARCHITECTS * LAND SURVEYORS

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 1

Totals

	Paving	Grading	Drainage	Sewer	Water	Dry Utilities	Miscellaneous	Total
Phase 1	$3,020,798	$528,468	$1,013,544	$4,030,581	$4,846,761	$166,480	$1,658,797	**$15,265,429**
Phase 2	$1,541,330	$267,789	$280,000	$187,216	$163,655	$98,480	$1,403,164	**$3,941,634**
Phase 3	$2,345,948	$442,089	$701,100	$4,148,918	$4,250,398	$180,880	$1,512,888	**$13,582,221**
Phase 4	$454,097	$77,883	$2,640,000	$203,420	$143,330	$43,136	$1,195,855	**$4,757,721**
Total	**$7,362,173**	**$1,316,229**	**$4,634,644**	**$8,570,135**	**$9,404,144**	**$488,976**	**$5,770,704**	

Total	**$37,547,005**
Engineering Fees - 9%	$3,379,230
Contingency - 10%	$3,754,701
Grand Total	**$44,680,936**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 1 - Phase 1 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	168,051	sy	$13.45	$2,260,285.95
2	3' Valley Gutter M.A.G. Std. 240 and Apron	1,320	sf	$5.00	$6,600.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	41,620	lf	$6.25	$260,125.00
4	6" Vertical Curb with Depressed Lip	28,532	lf	$6.25	$178,325.00
5	Sidewalk Ramp	8	ea	$140.00	$1,120.00
6	5' Sidewalk M.A.G. Std. 230	142,660	sf	$1.45	$206,857.00
7	4' Sidewalk M.A.G. Std. 230	52,352	sf	$1.40	$73,292.80
8	Survey Marker - M.A.G. 120-1 "B"	42	ea	$100.00	$4,200.00
9	Survey Marker - M.A.G. 120-1 "A"	1	ea	$250.00	$250.00
10	Street & stop signs	9	ea	$175.00	$1,575.00
11	Sign bases	9	ea	$110.00	$990.00
12	Fire hydrant pavement markers	61	ea	$17.00	$1,037.00
13	Adjust Manhole Frame and Cover	46	ea	$250.00	$11,500.00
14	Adjust Water Valve/Cleanout, Frame and Cover	61	ea	$240.00	$14,640.00
				Total	**$3,020,797.75**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	176,156	cy	$3.00	**$528,468.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	42" R.G.R.C.P. Class III Storm Sewer Pipe	222	lf	$72.00	$15,984.00
4	48" R.G.R.C.P. Class III Storm Sewer Pipe	134	lf	$80.00	$10,720.00
5	10' x 4' Box Culvert	2,044	lf	$360.00	$735,840.00
6	6' x 4' Box Culvert	88	lf	$250.00	$22,000.00
7	6' x 3' Box Culvert	712	lf	$250.00	$178,000.00
8	Pipe Inlet Wing	3	ea	$2,500.00	$7,500.00
9	Pipe Outlet Wing	3	ea	$2,500.00	$7,500.00
10	Box Inlet Wing	6	ea	$3,000.00	$18,000.00
11	Box Outlet Wing	6	ea	$3,000.00	$18,000.00
				Total	**$1,013,544.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	46	ea	$2,100.00	$96,600.00
2	24" ASTM D-3034 SDR35 PVC	2585	lf	$51.00	$131,835.00
3	15" ASTM D-3034 SDR35 PVC	2324	lf	$29.00	$67,396.00
5	10" ASTM D-3034 SDR35 PVC	3678	lf	$20.00	$73,560.00
6	8" ASTM D-3034 SDR35 PVC	8955	lf	$18.00	$161,190.00
7	Treatment Plant 1	1	ea	$3,500,000.00	$3,500,000.00
				Total	**$4,030,581.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	24" D.I.P.	7644	lf	$63.00	$481,572.00
2	18" D.I.P.	5508	lf	$52.00	$286,416.00
3	16" D.I.P.	12353	lf	$41.00	$506,473.00
4	12" D.I.P.	5040	lf	$30.00	$151,200.00
6	24" Gate Valve Box and Cover	15	ea	$4,500.00	$67,500.00
7	18" Gate Valve Box and Cover	11	ea	$1,200.00	$13,200.00
8	16" Gate Valve Box and Cover	25	ea	$4,500.00	$112,500.00
9	12" Gate Valve Box and Cover	10	ea	$1,200.00	$12,000.00
11	Fire Hydrant (Complete)	61	ea	$1,900.00	$115,900.00
12	Well 1	1	ea	$800,000.00	$800,000.00
13	Well 2	1	ea	$800,000.00	$800,000.00
16	Reservoir Tank 1	1500000	gal	$1.00	$1,500,000.00
				Total	**$4,846,761.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	20810	lf	$8.00	**$166,480.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	615924	sf	$1.00	**$615,924.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	27660	sf	$1.55	**$42,873.00**

Miscellaneous Total **$1,658,797.00**

Phase 1 Total	**$15,265,429**
Engineering Fees - 9%	$1,373,889
Contingency - 10%	$1,526,543
Phase 1 Grand Total	**$18,165,860**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 1 - Phase 2 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	83,273	sy	$13.45	$1,120,021.85
2	3' Valley Gutter M.A.G. Std. 240 and Apron	9,680	sf	$5.00	$48,400.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	24,620	lf	$6.25	$153,875.00
4	6" Vertical Curb with Depressed Lip	8,810	lf	$6.25	$55,062.50
5	Sidewalk Ramp	4	ea	$140.00	$560.00
6	5' Sidewalk M.A.G. Std. 230	44,050	sf	$1.45	$63,872.50
7	4' Sidewalk M.A.G. Std. 230	63,240	sf	$1.40	$88,536.00
8	Survey Marker - M.A.G. 120-1 "B"	25	ea	$100.00	$2,500.00
10	Street & stop signs	6	ea	$175.00	$1,050.00
11	Sign bases	6	ea	$110.00	$660.00
12	Fire hydrant pavement markers	6	ea	$17.00	$102.00
13	Adjust Manhole Frame and Cover	21	ea	$250.00	$5,250.00
14	Adjust Water Valve/Cleanout, Frame and Cover	6	ea	$240.00	$1,440.00
				Total	**$1,541,329.85**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	89,263	cy	$3.00	**$267,789.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
6	6' x 4' Box Culvert	1,072	lf	$250.00	$268,000.00
10	Box Inlet Wing	2	ea	$3,000.00	$6,000.00
11	Box Outlet Wing	2	ea	$3,000.00	$6,000.00
				Total	**$280,000.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	21	ea	$2,100.00	$44,100.00
4	12" ASTM D-3034 SDR35 PVC	3809	lf	$24.00	$91,416.00
5	10" ASTM D-3034 SDR35 PVC	2585	lf	$20.00	$51,700.00
				Total	**$187,216.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	16" D.I.P.	3055	lf	$41.00	$125,255.00
8	16" Gate Valve Box and Cover	6	ea	$4,500.00	$27,000.00
11	Fire Hydrant (Complete)	6	ea	$1,900.00	$11,400.00
				Total	**$163,655.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	12310	lf	$8.00	**$98,480.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	307870	sf	$1.00	**$307,870.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	61480	sf	$1.55	**$95,294.00**

Miscellaneous Total **$1,403,164.00**

Phase 2 Total	**$3,941,634**
Engineering Fees - 9%	$354,747
Contingency - 10%	$394,163
Phase 2 Grand Total	**$4,690,544**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 1 - Phase 3 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	139,266	sy	$13.45	$1,873,127.70
2	3' Valley Gutter M.A.G. Std. 240 and Apron	1,320	sf	$5.00	$6,600.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	39,828	lf	$6.25	$248,925.00
4	6" Vertical Curb with Depressed Lip	5,392	lf	$6.25	$33,700.00
5	Sidewalk Ramp	8	ea	$140.00	$1,120.00
6	5' Sidewalk M.A.G. Std. 230	70,540	sf	$1.45	$102,283.00
7	4' Sidewalk M.A.G. Std. 230	34,008	sf	$1.40	$47,611.20
8	Survey Marker - M.A.G. 120-1 "B"	45	ea	$100.00	$4,500.00
9	Survey Marker - M.A.G. 120-1 "A"	2	ea	$250.00	$500.00
10	Street & stop signs	7	ea	$175.00	$1,225.00
11	Sign bases	7	ea	$110.00	$770.00
12	Fire hydrant pavement markers	48	ea	$17.00	$816.00
13	Adjust Manhole Frame and Cover	53	ea	$250.00	$13,250.00
14	Adjust Water Valve/Cleanout, Frame and Cover	48	ea	$240.00	$11,520.00
				Total	**$2,345,947.90**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	147,363	cy	$3.00	**$442,089.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	24" R.G.R.C.P. Class III Storm Sewer Pipe	134	lf	$50.00	$6,700.00
2	30" R.G.R.C.P. Class III Storm Sewer Pipe	88	lf	$60.00	$5,280.00
4	48" R.G.R.C.P. Class III Storm Sewer Pipe	88	lf	$80.00	$7,040.00
5	10' x 4' Box Culvert	1,803	lf	$360.00	$649,080.00
8	Pipe Inlet Wing	3	ea	$2,500.00	$7,500.00
9	Pipe Outlet Wing	3	ea	$2,500.00	$7,500.00
10	Box Inlet Wing	3	ea	$3,000.00	$9,000.00
11	Box Outlet Wing	3	ea	$3,000.00	$9,000.00
				Total	**$701,100.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	53	ea	$2,100.00	$111,300.00
2	24" ASTM D-3034 SDR35 PVC	6276	lf	$51.00	$320,076.00
3	15" ASTM D-3034 SDR35 PVC	3720	lf	$29.00	$107,880.00
5	10" ASTM D-3034 SDR35 PVC	1974	lf	$20.00	$39,480.00
6	8" ASTM D-3034 SDR35 PVC	3899	lf	$18.00	$70,182.00
8	Treatment Plant 2	1	ea	$3,500,000.00	$3,500,000.00
				Total	**$4,148,918.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	16" D.I.P.	15708	lf	$41.00	$644,028.00
4	12" D.I.P.	8509	lf	$30.00	$255,270.00
8	16" Gate Valve Box and Cover	31	ea	$4,500.00	$139,500.00
9	12" Gate Valve Box and Cover	17	ea	$1,200.00	$20,400.00
11	Fire Hydrant (Complete)	48	ea	$1,900.00	$91,200.00
14	Well 3	1	ea	$800,000.00	$800,000.00
15	Well 4	1	ea	$800,000.00	$800,000.00
17	Reservoir Tank 2	1500000	gal	$1.00	$1,500,000.00
				Total	**$4,250,398.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	22610	lf	$8.00	**$180,880.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	488320	sf	$1.00	**$488,320.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	15850	sf	$1.55	**$24,567.50**

Miscellaneous Total **$1,512,887.50**

Phase 3 Total	**$13,582,220**
Engineering Fees - 9%	$1,222,400
Contingency - 10%	$1,358,222
Phase 3 Grand Total	**$16,162,842**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 1 - Phase 4 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	25,163	sy	$13.45	$338,442.35
3	6" Vertical Curb M.A.G. Std. 220 "A"	5,392	lf	$6.25	$33,700.00
4	6" Vertical Curb with Depressed Lip	5,393	lf	$6.25	$33,706.25
6	5' Sidewalk M.A.G. Std. 230	26,960	sf	$1.45	$39,092.00
8	Survey Marker - M.A.G. 120-1 "B"	11	ea	$100.00	$1,100.00
12	Fire hydrant pavement markers	8	ea	$17.00	$136.00
13	Adjust Manhole Frame and Cover	24	ea	$250.00	$6,000.00
14	Adjust Water Valve/Cleanout, Frame and Cover	8	ea	$240.00	$1,920.00
				Total	**$454,096.60**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	25,961	cy	$3.00	**$77,883.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
10	Bridge	24,000	sf	$110.00	**$2,640,000.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	24	ea	$2,100.00	$50,400.00
4	12" ASTM D-3034 SDR35 PVC	3221	lf	$24.00	$77,304.00
5	10" ASTM D-3034 SDR35 PVC	2290	lf	$20.00	$45,800.00
6	8" ASTM D-3034 SDR35 PVC	1662	lf	$18.00	$29,916.00
				Total	**$203,420.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
4	12" D.I.P.	3951	lf	$30.00	$118,530.00
9	12" Gate Valve Box and Cover	8	ea	$1,200.00	$9,600.00
11	Fire Hydrant (Complete)	8	ea	$1,900.00	$15,200.00
				Total	**$143,330.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	5392	lf	$8.00	**$43,136.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	91664	sf	$1.00	**$91,664.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	67220	sf	$1.55	**$104,191.00**

Miscellaneous Total **$1,195,855.00**

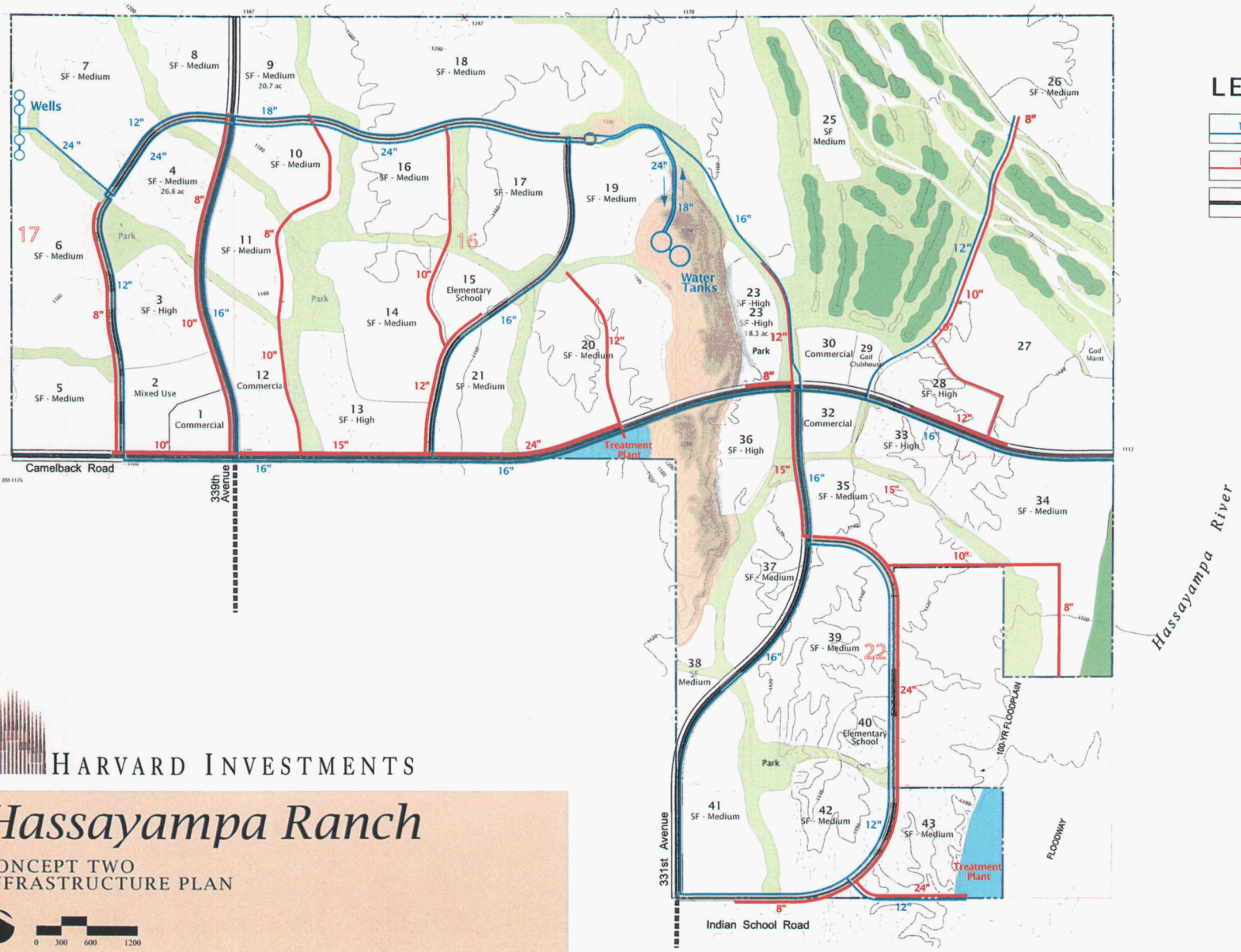
Phase 4 Total	**$4,757,721**
Engineering Fees - 9%	$428,195
Contingency - 10%	$475,772
Phase 4 Grand Total	**$5,661,688**

Concept 2 Infrastructure

Harvard Investments

Hassayampa Ranch

Concept 2 Infrastructure

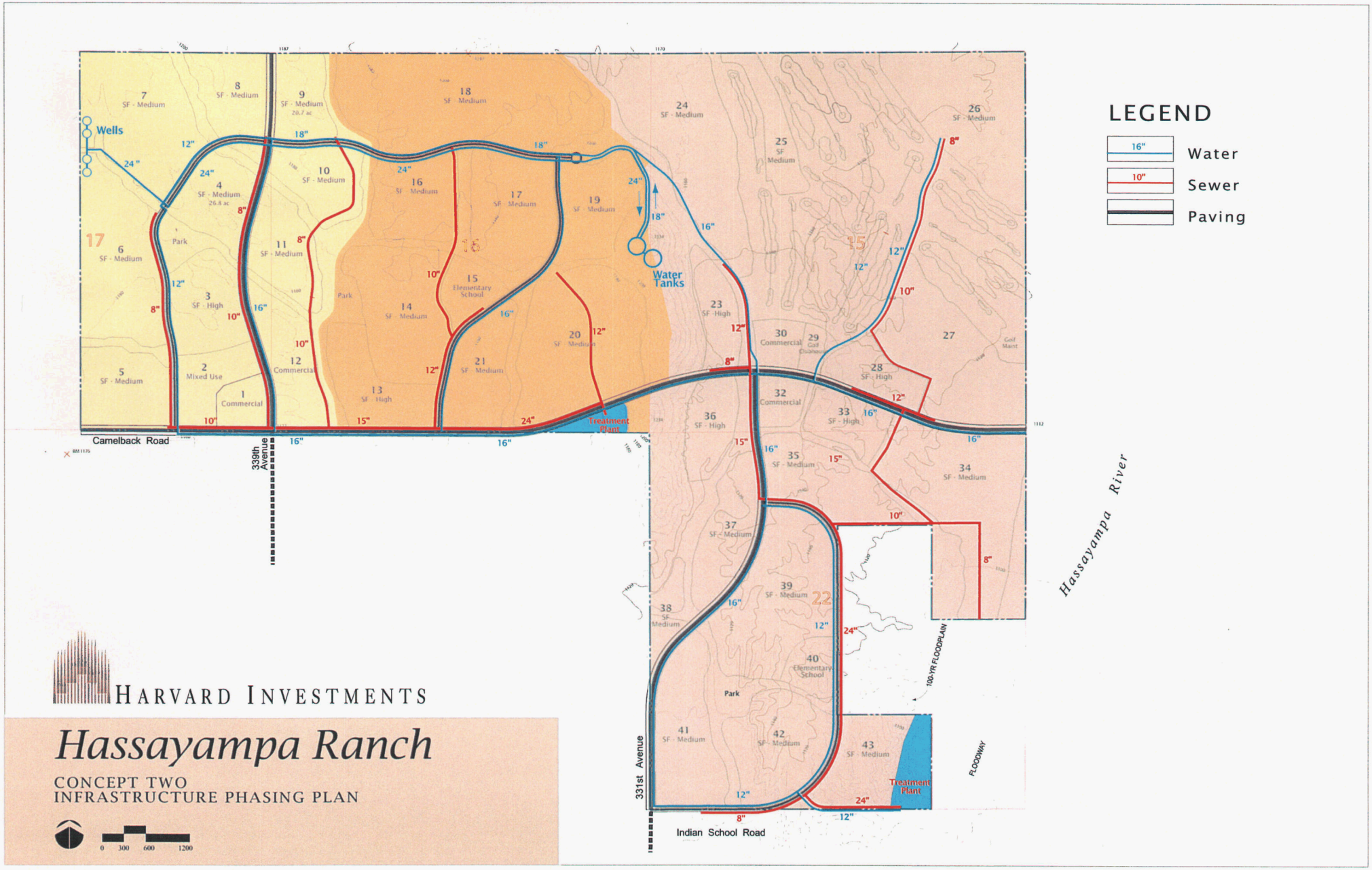


HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT TWO
INFRASTRUCTURE PLAN

0 300 600 1200



HARVARD INVESTMENTS

Hassayampa Ranch

CONCEPT TWO
INFRASTRUCTURE PHASING PLAN

0 300 600 1200

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 2

Totals

	Paving	Grading	Drainage	Sewer	Water	Dry Utilities	Miscellaneous	Total
Phase 1	$3,020,798	$528,468	$1,013,544	$4,030,581	$4,846,761	$166,480	$1,658,797	**$15,265,429**
Phase 2	$1,541,330	$267,789	$280,000	$187,216	$163,655	$98,480	$1,403,164	**$3,941,634**
Phase 3	$3,291,597	$590,391	$3,341,100	$4,352,338	$4,393,728	$180,880	$14,208,743	**$30,358,777**
Total	**$7,853,725**	**$1,386,648**	**$4,634,644**	**$8,570,135**	**$9,404,144**	**$445,840**	**$17,270,704**	

Total	**$49,565,840**
Engineering Fees - 9%	$4,460,926
Contingency - 10%	$4,956,584
Grand Total	**$58,983,350**

WRG DESIGN, INC.

PLANNERS * CIVIL ENGINEERS * LANDSCAPE ARCHITECTS * LAND SURVEYORS

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 2 - Phase 1 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	168,051	sy	$13.45	$2,260,285.95
2	3' Valley Gutter M.A.G. Std. 240 and Apron	1,320	sf	$5.00	$6,600.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	41,620	lf	$6.25	$260,125.00
4	6" Vertical Curb with Depressed Lip	28,532	lf	$6.25	$178,325.00
5	Sidewalk Ramp	8	ea	$140.00	$1,120.00
6	5' Sidewalk M.A.G. Std. 230	142,660	sf	$1.45	$206,857.00
7	4' Sidewalk M.A.G. Std. 230	52,352	sf	$1.40	$73,292.80
8	Survey Marker - M.A.G. 120-1 "B"	42	ea	$100.00	$4,200.00
9	Survey Marker - M.A.G. 120-1 "A"	1	ea	$250.00	$250.00
10	Street & stop signs	9	ea	$175.00	$1,575.00
11	Sign bases	9	ea	$110.00	$990.00
12	Fire hydrant pavement markers	61	ea	$17.00	$1,037.00
13	Adjust Manhole Frame and Cover	46	ea	$250.00	$11,500.00
14	Adjust Water Valve/Cleanout, Frame and Cover	61	ea	$240.00	$14,640.00
				Total	**$3,020,797.75**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	176,156	cy	$3.00	**$528,468.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	42" R.G.R.C.P. Class III Storm Sewer Pipe	222	lf	$72.00	$15,984.00
4	48" R.G.R.C.P. Class III Storm Sewer Pipe	134	lf	$80.00	$10,720.00
5	10' x 4' Box Culvert	2,044	lf	$360.00	$735,840.00
6	6' x 4' Box Culvert	88	lf	$250.00	$22,000.00
7	6' x 3' Box Culvert	712	lf	$250.00	$178,000.00
8	Pipe Inlet Wing	3	ea	$2,500.00	$7,500.00
9	Pipe Outlet Wing	3	ea	$2,500.00	$7,500.00
10	Box Inlet Wing	6	ea	$3,000.00	$18,000.00
11	Box Outlet Wing	6	ea	$3,000.00	$18,000.00
				Total	**$1,013,544.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	46	ea	$2,100.00	$96,600.00
2	24" ASTM D-3034 SDR35 PVC	2585	lf	$51.00	$131,835.00
3	15" ASTM D-3034 SDR35 PVC	2324	lf	$29.00	$67,396.00
5	10" ASTM D-3034 SDR35 PVC	3678	lf	$20.00	$73,560.00
6	8" ASTM D-3034 SDR35 PVC	8955	lf	$18.00	$161,190.00
7	Treatment Plant 1	1	ea	$3,500,000.00	$3,500,000.00
				Total	**$4,030,581.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	24" D.I.P.	7644	lf	$63.00	$481,572.00
2	18" D.I.P.	5508	lf	$52.00	$286,416.00
3	16" D.I.P.	12353	lf	$41.00	$506,473.00
4	12" D.I.P.	5040	lf	$30.00	$151,200.00
6	24" Gate Valve Box and Cover	15	ea	$4,500.00	$67,500.00
7	18" Gate Valve Box and Cover	11	ea	$1,200.00	$13,200.00
8	16" Gate Valve Box and Cover	25	ea	$4,500.00	$112,500.00
9	12" Gate Valve Box and Cover	10	ea	$1,200.00	$12,000.00
11	Fire Hydrant (Complete)	61	ea	$1,900.00	$115,900.00
12	Well 1	1	ea	$800,000.00	$800,000.00
13	Well 2	1	ea	$800,000.00	$800,000.00
16	Reservoir Tank 1	1500000	gal	$1.00	$1,500,000.00
				Total	**$4,846,761.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	20810	lf	$8.00	**$166,480.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	615924	sf	$1.00	**$615,924.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	27660	sf	$1.55	**$42,873.00**

Miscellaneous Total **$1,658,797.00**

Phase 1 Total	**$15,265,429**
Engineering Fees - 9%	$1,373,889
Contingency - 10%	$1,526,543
Phase 1 Grand Total	**$18,165,860**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS**. Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 2 - Phase 2 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over'10" A.B.C.	83,273	sy	$13.45	$1,120,021.85
2	3' Valley Gutter M.A.G. Std. 240 and Apron	9,680	sf	$5.00	$48,400.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	24,620	lf	$6.25	$153,875.00
4	6" Vertical Curb with Depressed Lip	8,810	lf	$6.25	$55,062.50
5	Sidewalk Ramp	4	ea	$140.00	$560.00
6	5' Sidewalk M.A.G. Std. 230	44,050	sf	$1.45	$63,872.50
7	4' Sidewalk M.A.G. Std. 230	63,240	sf	$1.40	$88,536.00
8	Survey Marker - M.A.G. 120-1 "B"	25	ea	$100.00	$2,500.00
10	Street & stop signs	6	ea	$175.00	$1,050.00
11	Sign bases	6	ea	$110.00	$660.00
12	Fire hydrant pavement markers	6	ea	$17.00	$102.00
13	Adjust Manhole Frame and Cover	21	ea	$250.00	$5,250.00
14	Adjust Water Valve/Cleanout, Frame and Cover	6	ea	$240.00	$1,440.00
				Total	**$1,541,329.85**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	89,263	cy	$3.00	**$267,789.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
6	6' x 4' Box Culvert	1,072	lf	$250.00	$268,000.00
10	Box Inlet Wing	2	ea	$3,000.00	$6,000.00
11	Box Outlet Wing	2	ea	$3,000.00	$6,000.00
				Total	**$280,000.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	21	ea	$2,100.00	$44,100.00
4	12" ASTM D-3034 SDR35 PVC	3809	lf	$24.00	$91,416.00
5	10" ASTM D-3034 SDR35 PVC	2585	lf	$20.00	$51,700.00
				Total	**$187,216.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	16" D.I.P.	3055	lf	$41.00	$125,255.00
8	16" Gate Valve Box and Cover	6	ea	$4,500.00	$27,000.00
11	Fire Hydrant (Complete)	6	ea	$1,900.00	$11,400.00
				Total	**$163,655.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	12310	lf	$8.00	**$98,480.00**

Miscellaneous

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	307870	sf	$1.00	**$307,870.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	61480	sf	$1.55	**$95,294.00**

Miscellaneous Total **$1,403,164.00**

Phase 2 Total	**$3,941,634**
Engineering Fees - 9%	$354,747
Contingency - 10%	$394,163
Phase 2 Grand Total	**$4,690,544**

Preliminary Engineer's Opinion of Probable Costs

These unit costs are **APPROXIMATIONS.** Use discretion when applying these numbers, since not all applications or installations are the same.

Concept 2 - Phase 3 Infrastructure

Paving

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	4" A.C. over 10" A.B.C.	185,554	sy	$13.45	$2,495,701.30
2	3' Valley Gutter M.A.G. Std. 240 and Apron	1,760	sf	$5.00	$8,800.00
3	6" Vertical Curb M.A.G. Std. 220 "A"	53,142	lf	$6.25	$332,137.50
4	6" Vertical Curb with Depressed Lip	10,784	lf	$6.25	$67,400.00
5	Sidewalk Ramp	10	ea	$140.00	$1,400.00
6	5' Sidewalk M.A.G. Std. 230	141,080	sf	$1.45	$204,566.00
7	4' Sidewalk M.A.G. Std. 230	99,704	sf	$1.40	$139,585.60
8	Survey Marker - M.A.G. 120-1 "B"	53	ea	$100.00	$5,300.00
9	Survey Marker - M.A.G. 120-1 "A"	2	ea	$250.00	$500.00
10	Street & stop signs	9	ea	$175.00	$1,575.00
11	Sign bases	9	ea	$110.00	$990.00
12	Fire hydrant pavement markers	56	ea	$17.00	$952.00
13	Adjust Manhole Frame and Cover	77	ea	$250.00	$19,250.00
14	Adjust Water Valve/Cleanout, Frame and Cover	56	ea	$240.00	$13,440.00
				Total	**$3,291,597.40**

Grading

Index	Service	Quantity	Unit	Cost Per Unit	Total
1	Balanced Cut/Fill	196,797	cy	$3.00	**$590,391.00**

Drainage Facilities

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	24" R.G.R.C.P. Class III Storm Sewer Pipe	134	lf	$50.00	$6,700.00
2	30" R.G.R.C.P. Class III Storm Sewer Pipe	88	lf	$60.00	$5,280.00
4	48" R.G.R.C.P. Class III Storm Sewer Pipe	88	lf	$80.00	$7,040.00
5	10' x 4' Box Culvert	1,803	lf	$360.00	$649,080.00
8	Pipe Inlet Wing	3	ea	$2,500.00	$7,500.00
9	Pipe Outlet Wing	3	ea	$2,500.00	$7,500.00
10	Box Inlet Wing	3	ea	$3,000.00	$9,000.00
11	Box Outlet Wing	3	ea	$3,000.00	$9,000.00
10	Bridge	24,000	sf	$110.00	$2,640,000.00
				Total	**$3,341,100.00**

Utilities - Sewer

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	5' Diameter Manhole, Type "A" Top	77	ea	$2,100.00	$161,700.00
2	24" ASTM D-3034 SDR35 PVC	6276	lf	$51.00	$320,076.00
3	15" ASTM D-3034 SDR35 PVC	3720	lf	$29.00	$107,880.00
4	12" ASTM D-3034 SDR35 PVC	3221	lf	$24.00	$77,304.00
5	10" ASTM D-3034 SDR35 PVC	4264	lf	$20.00	$85,280.00
6	8" ASTM D-3034 SDR35 PVC	5561	lf	$18.00	$100,098.00
8	Treatment Plant 2	1	ea	$3,500,000.00	$3,500,000.00
				Total	**$4,352,338.00**

Utilities - Water

Index	Material	Quantity	Unit	Cost Per Unit	Total
3	16" D.I.P.	15708	lf	$41.00	$644,028.00
4	12" D.I.P.	12460	lf	$30.00	$373,800.00
8	16" Gate Valve Box and Cover	31	ea	$4,500.00	$139,500.00
9	12" Gate Valve Box and Cover	25	ea	$1,200.00	$30,000.00
11	Fire Hydrant (Complete)	56	ea	$1,900.00	$106,400.00
14	Well 3	1	ea	$800,000.00	$800,000.00
15	Well 4	1	ea	$800,000.00	$800,000.00
17	Reservoir Tank 2	1500000	gal	$1.00	$1,500,000.00
				Total	**$4,393,728.00**

Utilities - Dry

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Gas, Electric, Cable, Telephone	22610	lf	$8.00	**$180,880.00**

Miscellaneous

Golf Course

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Golf Course	1	ea	$7,500,000.00	$7,500,000.00
2	Golf Clubhouse	1	ea	$5,000,000.00	$5,000,000.00
				Total	**$12,500,000.00**

Landscape

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	579984	sf	$1.00	**$579,984.00**

Parks

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	Landscaping	1	ea	$1,000,000.00	**$1,000,000.00**

Trails

Index	Material	Quantity	Unit	Cost Per Unit	Total
1	10' Colored concrete	83070	sf	$1.55	**$128,758.50**

Miscellaneous Total **$14,208,742.50**

Phase 3 Total	**$30,358,777**
Engineering Fees - 9%	$2,732,290
Contingency - 10%	$3,035,878
Phase 3 Grand Total	**$36,126,945**

EXHIBIT M

ANALYSIS OF ASSURED WATER SUPPLY

HASSAYAMPA RANCH

Maricopa County, Arizona

Prepared for:

Harvard Investments, Inc.
17700 North Pacesetter Way
Scottsdale, Arizona 85255

Prepared by:

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November 9, 2004

REGISTERED GEOLOGIST
CERTIFICATE NO.
17065
STEPHEN D.
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Date Signed 11/9/04
ARIZONA, U.S.A.

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1.0 INTRODUCTION

The following hydrogeologic investigation of the Hassayampa Ranch development near 339th Avenue and Camelback Road (The Project Area) has been prepared by Southwest Ground-water Consultants, Inc. (SGC) in order to evaluate the ground-water resources available to Harvard Investments, Inc. and to establish if these resources satisfy the projected water demand of future development. Hassayampa Ranch consists of 2,067 acres located southeast of the Belmont Mountains and west of the Hassayampa River. The Project Area is located within Township 2 North, Range 5 West, in the northwestern region of the Hassayampa Sub-basin of the Phoenix Active Management Area (AMA). A site location map is presented as Figure 1.

This report has been organized into five sections. Section 2.0 consists of a discussion of the projected water demand for the proposed development. The water resources available in the study area are presented in Section 3.0. The projected ground-water development impact on the regional aquifer is presented in Section 4.0. References cited throughout this report are listed in Section 5.0.

2.0 WATER DEMAND

2.1 LAND USE

The land use plan for the Hassayampa Ranch development was provided by WRG Design, Inc. The property consists of 2,067 acres that have been divided according to the following land use categories:

Use	Approximate Acreage	Approximate # of Units
Residential	1,326.8	5,707
Commercial	59.5	
Mixed Use	19.4	
Schools	13.2	
Public	18.7	
Roadways	91.4	
Open Space	279.2	
Golf	258.4	

Source: WRG Design, Inc. (2004)

The preliminary development master plan includes a total of 5,707 dwelling units (du). Based on an estimated home occupant density estimate of 3.2 capita per dwelling unit, the total population is projected to be 18,262 people.

2.2 DEMAND

The water demand has been estimated based on Phoenix AMA Third Management Plan water requirements (ADWR, 1999). A summary of the water demand estimate is presented in Table 1.

2.2.1 Residential

The estimated residential demand for the proposed development is 2,304 acre-feet per year (ac-ft/yr). This demand is based on the following assumptions and unit rates.

- Interior water use is 57 gallons per capita per day (gpc/d) (ADWR, 1999).

- Exterior water use for single family homes is 178 gallons per day per dwelling unit (gpd/du) (ADWR, 1999). It is estimated that no lots will exceed 10,000 square feet.
- Total number of dwelling units is 5,707 single-family homes (WRG Designs, Inc., 2004).
- Per capita occupancy rate is 3.2 capita per dwelling unit.

Therefore:

- The average dwelling unit demand is 360 gpd/du.
- The total residential (indoor and outdoor) demand is 2,304 ac-ft/yr.

2.2.2 Non-residential

The estimated non-residential demand for the Project is 1,438 ac-ft/yr. This total is the sum of the demands for commercial, schools, open space, roadways, public facilities, golf course, mixed use, construction, and system losses as outlined below.

Commercial, Public Facilities, and Mixed Use

The water demand associated with the 98 acres designated for commercial, public facilities, and mixed use, was estimated based on a rate of 2.25 ac-ft/ac. The resulting estimated demand for commercial, public facilities, and mixed use is 219.6 ac-ft/yr.

Schools

The indoor demand for the proposed schools was estimated using a rate of 25 gallons per student per day, for the elementary schools. The demand for the proposed high schools was estimated using a rate of 45 gallons per student per day. The number of elementary school students was determined based on a rate of 0.65 students per dwelling unit, and the number of high school students was determined based on a rate of 0.25 students per dwelling unit.

The outdoor water demand associated with the schools was calculated using a water use rate of 4.9 ac-ft/ac/yr for turf acreage and 1.5 ac-ft/ac/yr for low water use landscaping (lwul) (ADWR, 1999). A total of 25% of the designated school acreage is irrigated with turf, and 10% was estimated as lwul.

According to current proposed land uses (WRG Designs, Inc., 2004), Hassayampa Ranch has 13.2 acres designated for elementary schools, and 13.2 acres designated for high schools. The estimated numbers of students are 3,710 elementary school students and 1,427 high school students. Accordingly, the estimated water demand is 122 ac-ft/yr for elementary schools and 90 ac-ft/yr for high schools.

Golf Course

According to current proposed land uses (WRG Designs, Inc., 2004), Hassayampa Ranch has a total of 258 acres designated for a golf course. The demand associated with the golf course is 456.62 ac-ft/yr based on Phoenix AMA Third Management Plan water requirements (ADWR, 1999).

Roadways

A total of 6% (5.5 acres) of the total roadway acreage is estimated as lwul. The water demand associated with the 5.5 acres designated for roadways was estimated based on a rate of 1.5 ac-ft/ac. The resulting estimated demand for roadways is 8 ac-ft/yr.

Open Space

A total of 10% (28 acres) of the total open space acreage is estimated as turf and 15% (42 acres) is estimated as lwul. The water demand associated with the 70 acres designated for open space was calculated based on a rate of 1.5 ac-ft/ac for lwul and 4.9 ac-ft/ac for turf. The resulting estimated demand for open space is 200 ac-ft/yr.

Construction

The amount of water required for construction purposes is estimated to be 10,000 gallons per dwelling unit and 15,000 gallons per commercial acre (ADWR Office of Assured and Adequate Water Supply). This amounts to 175 ac-ft for the 5,707 dwelling units, and 4 ac-ft for the 79

commercial and mixed use acres. Since this is a one-time use, the value is divided by 100 for a construction demand total of 1.79 ac-ft/yr.

System Losses

System losses are estimated to be 10% of the total demand. Summing all of the water demand components yields a total system demand of 3,402 ac-ft/yr, therefore, the system losses are calculated to be 340 ac-ft/yr.

2.2.3 Total Project Demand

The estimated total demand for the Project at final build-out, based on the proposed land uses, is 3,742 ac-ft/yr (2,320 gpm annual average). A summary of the water demand estimate is presented in Table 1.

3.0 WATER SUPPLY

3.1 BACKGROUND

During the conduct of this investigation, SGC collected and reviewed pertinent published and unpublished geologic and hydrogeologic data from various sources. Data sources consisted of the following:

Arizona Department of Water Resources (ADWR)
Arizona Geological Survey
U.S. Bureau of Reclamation (USBR)
U.S. Geological Survey (USGS)
Southwest Ground-water Consultants, Inc. corporate files

The most detailed site specific data for the Project Area were presented in reports prepared for the nearby Belmont Development (SGC, 2003 and Halpenny, 1989). Other reports documenting the hydrogeology in the region include a series by Leonard C. Halpenny and Philip C. Halpenny (1986a, 1987 and 1988) regarding Sun Valley, reports by Hargis & Associates, Inc. (1985 and 1987), Paul A. Manera (1971 and 1984) and Southwest Ground-water Consultants, Inc. (2001) regarding Douglas Ranch, and a hydrogeologic report of the Hassayampa Plain by Water Resources Associates, Inc. (1991).

Basic data concerning ground-water surface elevations and lithology (drillers reports) for the study area were obtained from ADWR and USGS.

Brief descriptions of the available reports reviewed by SGC are presented below:

Southwest Ground-water Consultants

Prepared hydrogeologic investigation for the Belmont development (February 28, 2003). Analyzed the 100-year aquifer impact of Belmont as part of Physical Availability Demonstration.

Water Development Corporation

Preliminary Evaluation of Groundwater Resources Available to BRM Project Master Plan Area, October 1989 (Halpenny and Halpenny, 1989). Presented the results of an onsite well drilling and testing program and projected the impact of the Belmont Project (formerly known as BRM Project) on the aquifer below.

Progress Report - Results of Phase I Test Drilling, July, 1986. Basic Data Report - Test of existing well along edge of CAP adequate at Hassayampa Pumping Station, October 1986 (Halpenny and Halpenny, 1986b).

Evaluation of adequacy of ground-water supply for Sun Valley Project November, 1987.

Supplemental Report - Sun Valley Project range of potential figures for ground water in storage and of long-term water level drawdown from projected demand, May 1988 (Halpenny, 1988). Evaluation of ground-water supply at Sun Valley Project, March 1988, Revised May 1988 (Halpenny and Halpenny, 1988). Projected impact of the Sun Valley Project on the aquifer beneath Belmont ranged from 50 to 100 feet. Halpenny also estimated the ground-water outflow from the Hassayampa Plain to be approximately 32,000 ac-ft/yr.

Hargis & Associates

Prepared hydrogeologic evaluation of the Douglas Ranch (December 17, 1985). Estimated the volume of ground water beneath the Ranch in storage to be 900,000 acre-feet.

Updated developable ground-water resources at the Douglas Ranch to 2,928,000 acre-feet following the installation and testing (short-term) of 6 wells (July 28, 1987). Documented aquifer coefficient values, and water quality.

Manera

Prepared hydrologic investigation of the Douglas Ranch (March 22, 1971). Conducted electrical resistivity surveys documenting the lithology of the aquifer. Estimated the volume of recharge into the aquifer and developable ground-water resources.

Provided update of 1971 report in letter report of 1984. Included an estimate of ground-water recharge over the entire basin to be 3,900 ac-ft/yr.

Southwest Ground-water Consultants

Prepared hydrogeologic investigation of the Douglas Ranch (May 14, 2001). Evaluated previously conducted lithologic and geophysical logs of exploratory boreholes, as well as aquifer tests and water quality samples of previously installed wells, and analyzed the 100-year aquifer impact of Douglas Ranch.

Representative wells of the study area have been plotted on Figure 2 and the well registry reports for those wells are referenced as Appendix A.

3.2 GEOLOGY

The Project Area is located in the Hassayampa sub-basin of the Phoenix Active Management Area. The Hassayampa sub-basin is situated within the Basin and Range Physiographic Province of Arizona. This province is characterized generally by northwest-trending fault bounded mountain ranges separated by alluvium-filled intervening basins (Figure 3). The Hassayampa sub-basin is further divided into two distinct hydrologic sub-basins, the Hassayampa Plain and the Tonopah Desert. The Project Area is situated primarily within the Tonapah Desert. The thickness of alluvial sediments within the vicinity of the Project Area ranges in thickness from 0 feet at the mountain fronts to over 3,200 feet (Oppenheimer and Sumner, 1980). A depth to bedrock map is

presented in Figure 4. The basin fill material consists of interbedded alluvial deposits consisting of clay, silt, sand, gravel, and conglomerate.

3.2.1 Stratigraphy

The Project Area is underlain by a sequence of alluvial fan sedimentary deposits. These deposits grade from a very coarse mountain-front boulder zone into finer grained sediments and conglomerate material identified out into the sub-basins. The thickness of these deposits ranges from 0 at the mountain fronts to greater than 3,200 feet (Oppenheimer and Sumner, 1980). Stulik (1974) and Stulik and Laney (1976) inferred that the maximum depth (and subsequent thickness of alluvium) of the basin is approximately 1,200 feet.

Details on the drilling of seven test wells (Wells 1 through 7) for the Belmont development in the vicinity of the Project Area were presented by Halpenny and Halpenny (1989). Bedrock was encountered during the drilling of wells 1 and 2, which were drilled within the Tonopah Desert sub-basin, at depths of 410 and 710 feet below land surface (ft bls), respectively. Wells 4, 5, 6 and 7 were drilled to depths of 615, 840, 690 and 795 ft bls, respectively without encountering bedrock. Bedrock was encountered at 530 ft bls during the drilling of well 3, which was drilled in the Hassayampa Plain sub-basin. The location of the test wells is shown in Figure 2 and schematic diagrams of well construction and borehole lithology for those same wells are presented in Appendix B.

The proposed well field for the Hassayampa Ranch development lies within the western portion of the Project Area. Test wells 2 and 7 are within 1.5 miles of the proposed well field. The depth to bedrock of 710 feet bls encountered in well 2, and greater than 795 feet bls in well 7, correlate with the results of the gravitational analysis (Figure 4, Oppenheimer & Sumner, 1980). An alluvial thickness of 800 feet, as indicated by the gravitational analysis for the location of the proposed well field, was used in calculations conducted for this report.

3.2.2 Structure

The dominant orientation of faulting in the Hassayampa Plain and the Tonopah Desert is northwest-southeast. This structural grain is clearly evident in the topography developed in the Belmont, White Tank, and Vulture Mountains. The roughly east-west fault system described by Halpenny (1988) along the southern margin of the Vulture Mountains is not apparent and probably does not exist as a major range-bounding structure. Instead, this region is most likely altered by the dominant northwest-oriented geologic structures. As such, the geologic structure (hence the bedrock surface) near the mouth of the Hassayampa River is most likely steeply-sloping toward the south and west. The structure along the western margin of the White Tanks and in the Vulture mountains has been further complicated by low-angle detachment faulting and block rotation (S. Reynolds, personal communication in Water Resources Associates, 1991).

The Hassayampa Plain alluvial basin is a cone-shaped depression trending south through the narrow graben located between the Belmont Mountains to the west and the White Tank Mountains to the east (Oppenheimer and Sumner, 1980). The trend continues south through the Tonopah Desert alluvial basin past the Palo Verde Hills and into the lower Centennial Wash basin. Shallow bedrock outcrops exist in the central portion of the Project Area.

Interpretative geologic cross-sections of the subsurface lithology in the vicinity of the Project Area were presented by Water Development Corporation (Halpenny and Halpenny, 1989) based on the lithology of drill cuttings from the onsite exploratory wells. Copies of those cross-sections and a cross-section location map are presented in Appendix B.

3.3 HYDROGEOLOGY

3.3.1 Ground-water Surface

Depth to ground water has been measured in study area wells erratically over the years. Basin wide measurements have been conducted generally in association with published reports or maps. The most recent extensive survey was conducted by ADWR during the winter of 1991, with more

recent spot measurements conducted in 1997. Those data are presented in Appendix C.

A ground-water surface map, prepared based on the 1991 water level data (Hammett and Herther, 1995), is presented in Figure 5. The spot 1997 ground-water elevations are also shown on the water surface map. Review of the water level data indicates that the depth to ground water ranges from 122 to 143 ft bls in the vicinity of the Project Area. The ground-water surface has remained relatively stable throughout the basin over the past 10 years. Calculations in this report assume a depth to ground water of 150 ft bls.

3.3.2 Historic Ground-water Level Trends

Pumping in the Tonopah Desert has been focused primarily in the north portion of the Tonopah Desert and in the southeast portion of the Tonopah Desert approximately five miles west of the Hassayampa River. Hydrographs of three wells in the Tonopah Desert and one well in the Hassayampa Plain Area are presented in Figure 6. Water levels in well B(2-5) 29dac declined at 0.2 feet per year (ft/yr) over the past 35 years. Review of hydrographs of two wells located west of the Project Area indicates that ground-water levels declined at about -4.0 ft/yr between 1950 and 1980. Between 1980 and 1999, those levels rose at rates of +4.0 ft/yr and +2.0 ft/yr in wells B(2-6)23aba and B(2-6)21bba respectively. Review of the hydrograph for the well B(3-5)26 daa, suggests a gradual rise in water levels of +0.1 ft/yr since 1950, however the water level record cuts off in 1987.

Ground-water development in the Tonopah Desert, the Buckeye area, and in the northwest portion of the western Salt River Valley has not adversely impacted the ground-water resource in the Hassayampa Plain and Lower Hassayampa Plain study area. The local geology, hydrogeology, and land uses associated with the basin discharge areas have limited ground-water pumping impacts from outside the basin on the study area.

3.3.3 Aquifer Parameters

3.3.3.1 Aquifer Thickness

An estimate of the saturated aquifer thickness below the proposed Project Area well field in the Tonopah Desert was made by subtracting the estimated depth to ground water from the estimated alluvial thickness. Based on 1997 ground-water level data (Figure 5; ADWR, 2001), the approximate depth to water beneath the Project Area is 150 feet below land surface (ft bls). Based on an estimated depth to bedrock presented by Oppenheimer and Sumner (1980), the estimated average alluvial thickness beneath the proposed well field is 800 ft bls. The saturated aquifer thickness beneath the proposed well field has been estimated at 650 feet.

3.3.3.2 Aquifer Transmissivity

Estimates of average aquifer transmissivity for the vicinity of the Project Area, were based on a nearby drilling program (Belmont wells) presented by Halpenny and Halpenny (1989). Aquifer testing of 6 wells yielded an area-weighted average transmissivity of 54,000 gallons per day per foot (gpd/ft). The area-weighted transmissivity calculation is presented in Table 2. This value was used in calculating the long-term yield of the aquifer beneath the Project Area (Section 4.0).

3.3.3.3 Specific Yield

Halpenny and Halpenny (1989) calculated an area-weighted average specific yield of 0.13 for the Tonopah Desert. The specific yield values incorporated into that analysis were based on review of lithologic data for the Belmont exploratory wells. A specific yield of 0.13 was employed in the aquifer impact analysis of the Project Area (Section 4.0).

3.3.4 Ground-water Quality

Ground-water samples were collected from the Belmont exploratory wells (Wells 2, 3, 4, 5, 6 and 7) drilled in the vicinity of the Project Area (Halpenny and Halpenny, 1989). The samples were

analyzed for major cations and anions, trace metals, and radiological content. The locations of the exploratory wells are shown on Figure 2. Results of those analyses are presented in Appendix D.

Review of the analytical results indicates that the ground-water quality meets current EPA and ADEQ standards for the constituents tested except for fluoride, which was detected at a concentration of 5.2 milligrams per liter (mg/1) in exploratory well No. 4 (Halpenny and Halpenny, 1989). The ADEQ maximum contaminant level (MCL) for fluoride is 4.0 mg/l.

For permitting purposes, concentrations in ground-water samples collected from new production wells must meet drinking water standards for all of the constituents that comprise ADEQ's New Source Approval.

3.4 BASIN RECHARGE

Review of the 1991 ground-water surface indicates that recharge into the Hassayampa Plain enters the basin primarily from the Hassayampa River to the north and Jackrabbit Wash to the northwest. Immediately south of the Belmont mountains, ground-water flows diverge, with a portion flowing to the northwest toward a pumping center in the Tonopah Desert, another portion flowing eastward around the south end of the White Tank Mountains, and the remainder continuing south southwest between the Palo Verde Hills and the Buckeye Hills.

3.4.1 Hassayampa Plain

Recharge into the Hassayampa Plain sub-basin via the Hassayampa River flows has been estimated to range from approximately 3,900 ac-ft/yr (Manera, 1971) to 16,000 ac-ft/yr (Halpenny, 1987). Halpenny (1987, 1988) also reported that the total ground-water recharge into the basin was approximately 32,000 ac-ft/yr. Review of the ADWR files reveals that the Department's estimate of ground-water recharge is approximately 17,000 ac-ft/yr, while Montgomery and DATS (1988), conducting a study on behalf of ADWR, evaluated the surface water inflow to the Buckeye Valley from the Hassayampa River to be 26,500 ac-ft/yr.

Water Resources Associates (1991) estimated the volume of basin recharge based on conducting Darcy Strip analyses at the two basin discharge points (Hassayampa River and Trilby Wash) using the 1985-1986-1987 ground-water surface and hydraulic conductivity values used in the ground-water flow model. The total WRA basin recharge value was estimated to be approximately 36,600 ac-ft/yr where approximately 23,400 ac-ft/yr passes south in the narrows area beneath the Hassayampa River, and 13,200 ac-ft/yr passes north of the White Tank Mountains to the east in the Trilby Wash area.

3.4.2 Tonopah Desert

Based on a review of the water surface of 1991 ground-water level data (Figure 5), mountain front recharge occurs primarily in the northwest portion of the Tonopah Desert. Ground water generally flows toward a pumping center located west of the Project Area. A large portion of the ground water recharging the Tonopah Desert from the Hassayampa Plain flows northwest to this cone of depression.

3.5 EFFLUENT

Effluent generated by the development will be available for either direct re-use (turf, open space, roads right-of-way, parks), or for recharge into the regional aquifer. The volume of available effluent from the project has been estimated at 1,049 ac-ft/yr, which is 90% of the indoor residential demand. The re-use of effluent was not considered in the aquifer impact analysis presented in Section 4.0.

4.0 GROUND-WATER DEVELOPMENT IMPACT

An estimate of the impact of pumping on the regional aquifer was calculated using the THWELLS v 4.01 multi-Theis analysis software (van der Heijde, 1996). The program THWELLS calculates the drawdown or buildup of piezometric head due to the combined effect of multiple discharge and recharge wells in a confined, leaky-confined, or unconfined aquifer. The calculations for total drawdown are based on the Theis equation for non-equilibrium flow in an isotropic, homogeneous aquifer (van der Heijde, 1996), with the option of applying the Jacob water table correction (Jacob, 1946) to better simulate unconfined aquifer conditions. The proposed well field for the Project Area is within the Tonopah Desert sub-basin.

In order to establish the projected 100-year depth to ground water at the Project Area in the Tonopah Desert, impacts of ground-water production to meet the water demands of the Project Area were added to the impacts associated with existing ground-water users (by projecting the background ground-water level decline trend), and the most current ground-water levels available (1997). The estimated impact of the Belmont development was added to the impacts associated with the Project Area.

4.1 MODEL GRID

The model grid extends north and northeast to areas of shallow bedrock associated with the Belmont Mountains and covers approximately 100 square miles. The nodal grid spacing is 660 feet in both the X and Y directions. The grid values are in units of feet and in the Universal Transverse Mercator (Zone 12, NAD 1927) coordinate system.

4.2 AQUIFER PARAMETERS

Based on an area-weighted average of aquifer transmissivity and specific yield values in the Tonopah Desert presented by Halpenny and Halpenny (1989), a transmissivity of 54,000 gallons per day per foot (gpd/ft) and a specific yield of 0.13 were incorporated into the impact analysis. The transmissivity values used in the area-weighted average originated from aquifer tests

conducted in Belmont exploratory wells, and the specific yield values were based on review of lithologic cuttings of those wells. In order to account for the effects of unconfined conditions on the aquifer impact, the THWELLS unconfined aquifer option was selected for the analysis. Based on ground-water level data and reported alluvial thickness in the Tonopah Desert, the saturated aquifer thickness used to make the water table correction in the analysis was 650 feet. No water table gradient or recharge has been assumed for the simulation, thereby resulting in a greater calculated impact.

4.3 PUMPING WELLS

Ground-water production in the Project Area was simulated by assigning 3 potential pumping well locations. Each pumping well was assigned an average pumping rate of 773 gallons per minute (gpm), which is based on a total annual demand (Section 2.0) of 3,742 ac-ft/yr (2,320 gpm). The pumping rate of 773 gpm assigned to each well assumes no use of effluent or CAP water.

Because of the proximity of bedrock outcrops and associated shallow bedrock associated with the Belmont Mountains and a shallow impermeable clay zone, three image well boundaries were incorporated into the analysis that simulate the impermeable hydrologic boundaries. Including image wells, the analysis included a total of 9 pumping well locations. The location of the 3 pumping wells, 6 image wells, and image well boundaries are displayed in Figure 7.

4.4 MODEL OUTPUT

The analysis is based on continuous pumping for a period of 36,500 days (100 years). The maximum aquifer impact is 116 feet. The 100-year aquifer impact contour map displaying the results of this analysis is presented in Figure 7. The output file for the analysis is presented in Appendix E.

4.5 100-YEAR WATER LEVEL

The maximum calculated 100-year depth to water occurs at the simulated pumping well location B(2-5)17 dbb. The projected 100-year depth to ground water is 591 feet below land surface (bls). The maximum impact on the aquifer is outlined in the chart below.

Static Water Level (1997 GWSI Data)	150 ft bls
100-Year Ground-water Decline @ -0.2 ft/yr*	20 feet
Belmont Development Impact	305 feet
Project Area Impact	116 feet
Project Area 100-Year Depth to Water	**591 ft bls**

* 100-year decline rate of -0.2 ft/yr was assigned to the impact analysis in order to be conservative. Actual ground-water surface has been observed to be relatively flat or even rising over time.

The projected maximum impact on the regional aquifer beneath the Project Area as a result of ground-water pumping is 591 ft bls. This 100-year impact is within the ADWR Phoenix AMA 100-year depth to ground water limit of 1,000 ft bls based on ADWR Rule R12-15-703. In addition, this calculated impact is conservative because the analysis:

- assumes the full water demand will be met by pumping only 3 wells,
- assumes no re-use or recharge of effluent,
- does not consider a planned artificial recharge project in the Tonopah Desert (CAWCD, 2003),
- does not take into account natural recharge into the aquifer system,
- assumes no water table gradient,
- assumes a background ground-water level decline rate of 0.2 feet per year, and
- assumes 100% build-out at day one.

4.6 CONCLUSION

Based on the impact analysis presented, sufficient ground water is available to meet the water demands of the proposed development for at least 100 years.

5.0 REFERENCES

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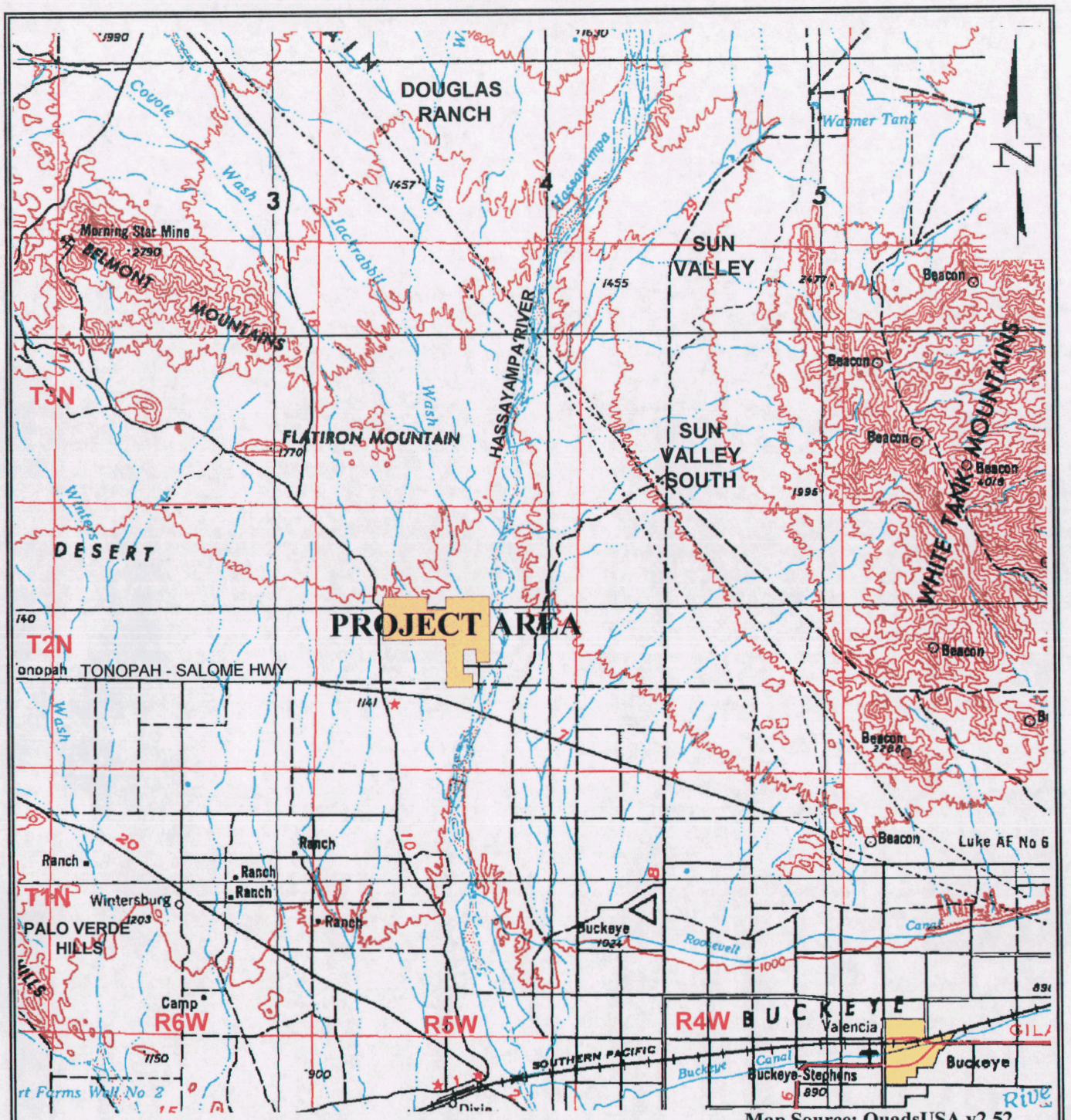
FIGURES

FIGURES



Map Source: QuadsUSA v2.52

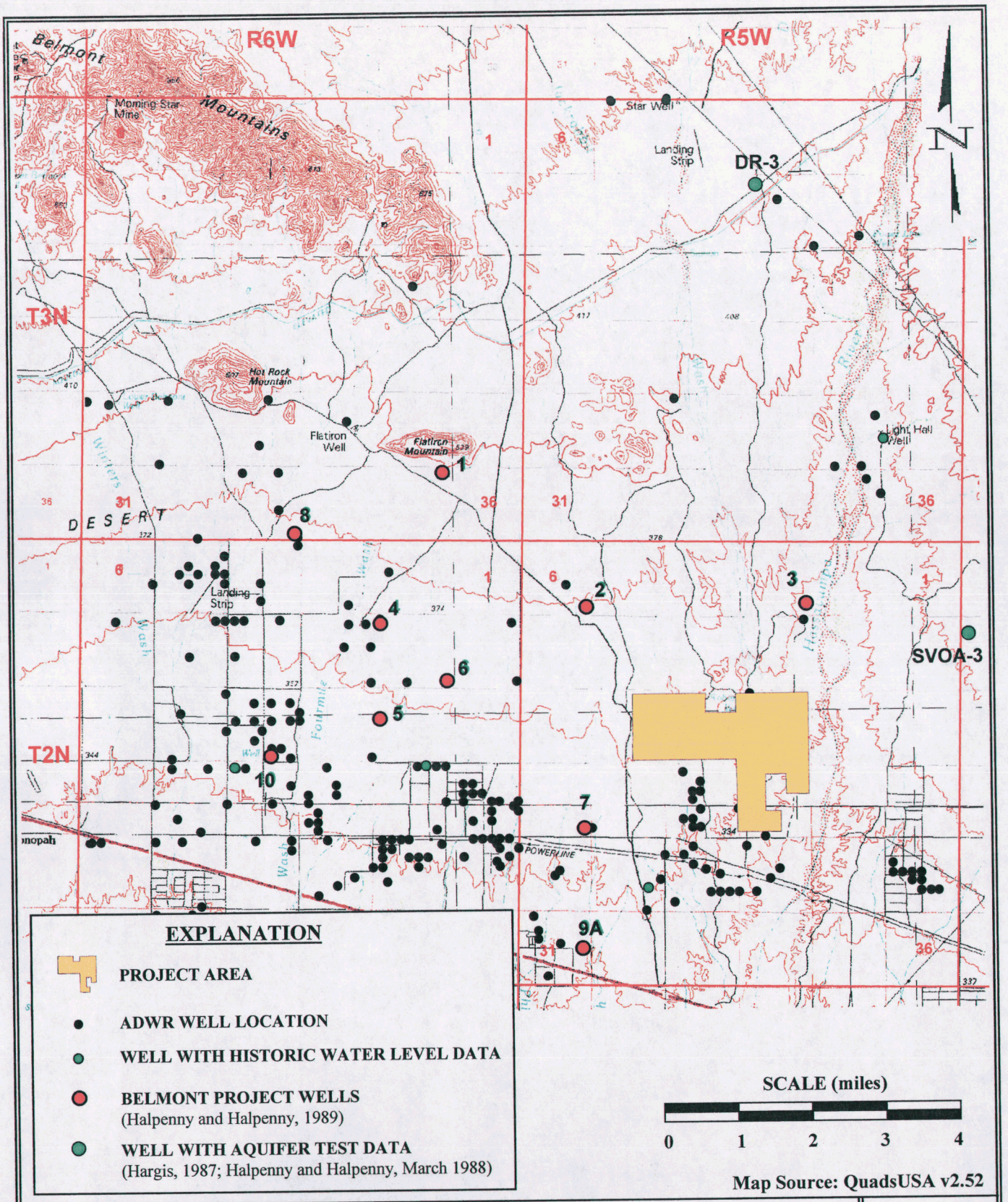
EXPLANATION

PROJECT AREA

SCALE (miles)

0 3 6

Southwest Ground-water Consultants, Inc. November 1, 2004 Project B.941	**SITE LOCATION MAP** Hassayampa Ranch Maricopa County, Arizona	**Figure 1**



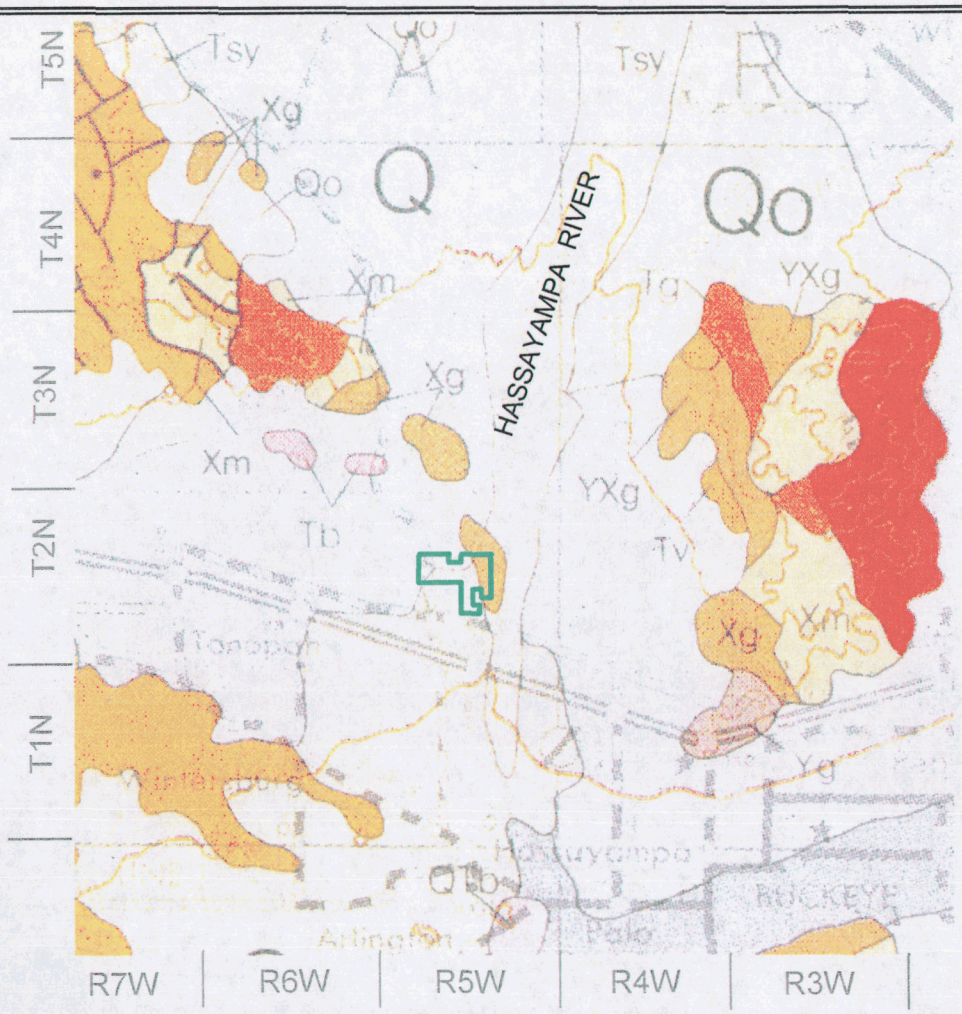
Southwest Ground-water Consultants, Inc.

November 2, 2002 Project B.941

WELL LOCATION MAP

Hassayampa Ranch
Maricopa County, Arizona

Figure 2



GEOLOGIC MAP UNITS

Q — **SURFICIAL DEPOSITS** (Holocene to middle Pleistocene) - Alluvium in present-day valleys and piedmonts, eolian deposits, and local glacial deposits.

Qo — **OLDER SURFICIAL DEPOSITS** (middle Pleistocene to latest Pliocene) - Alluvium with less abundant talus and eolian deposits.

Tb — **BASALTIC ROCKS** (late to middle Miocene; 8 to 16 Ma) - Units, such as the Hickey formation, erupted after most mid-Tertiary volcanism and tectonism.

Tg — **GRANATOID ROCKS** (early Miocene to Oligocene; 18 to 38 Ma) .

Xg — **GRANITOID ROCKS** (Early Proterozoic; 1650 to 1750 Ma) - Granite, granodiorite, tonalite, quartz diorite, diorite, and gabbro; commonly foliated.

Xm — **METAMORPHIC ROCKS** (Early Proterozoic; 1650 to 1800 Ma). Undifferentiated metasedimentary, metavolcanic, and gneissic rocks.

EXPLANATION

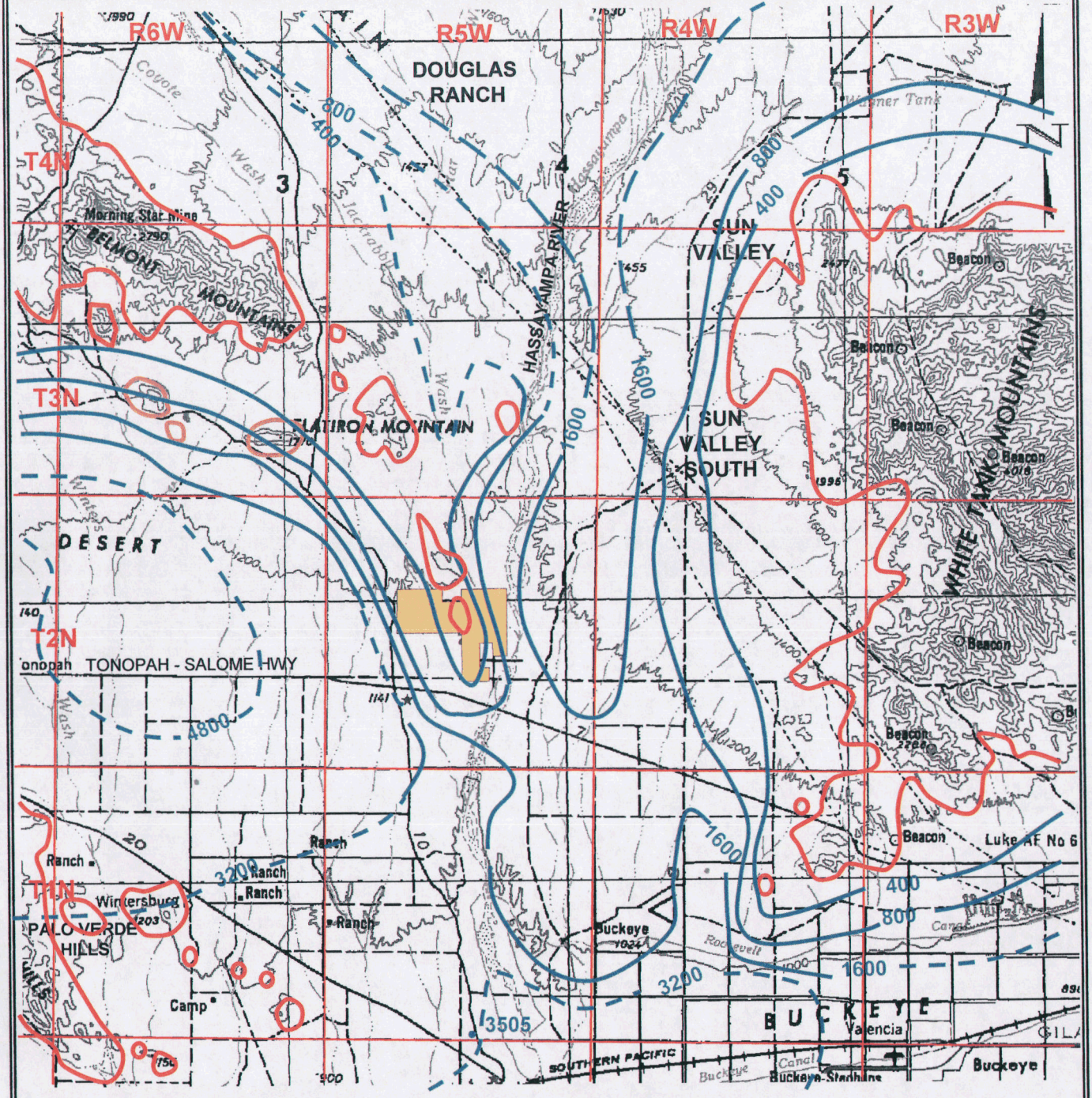
PROJECT AREA

SCALE (miles)

0 2 4 6 8

Map Source: Arizona Geological Survey Map 26 (Reynolds, 1988)

Southwest Ground-water Consultants, Inc. **November 1, 2004 Project B.941**	**GEOLOGIC MAP** **Hassayampa Ranch** **Maricopa County, Arizona**	**Figure 3**



EXPLANATION

- PROJECT AREA
- ESTIMATED ROCK OUTCROP BOUNDARY
- ESIMATED QUATERNARY BASALT BOUNDARY
- DEPTH-TO-BEDROCK CONTOUR

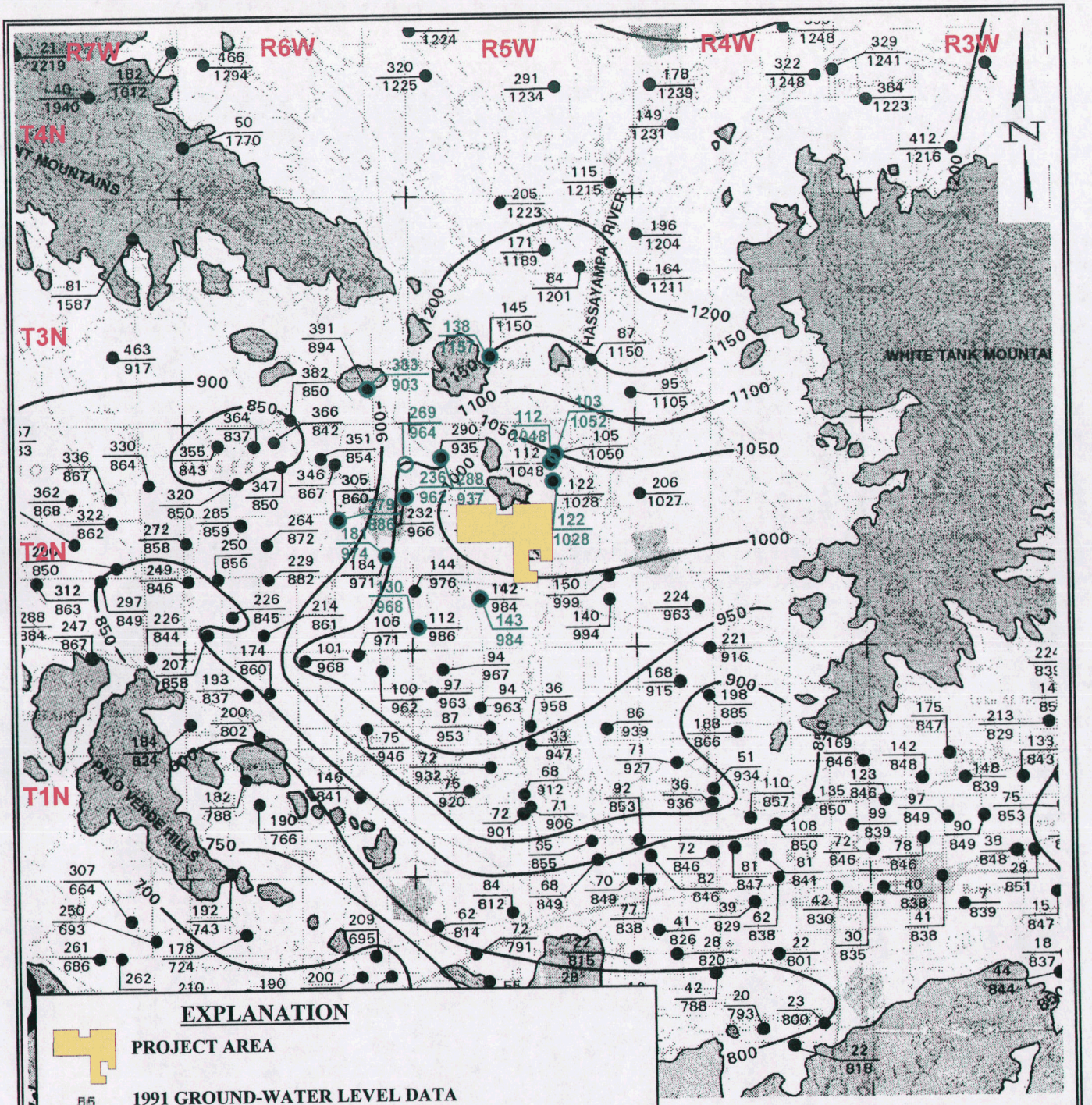
SOURCE: OPPENHEIMER SUMNER, 1980

SCALE (miles)

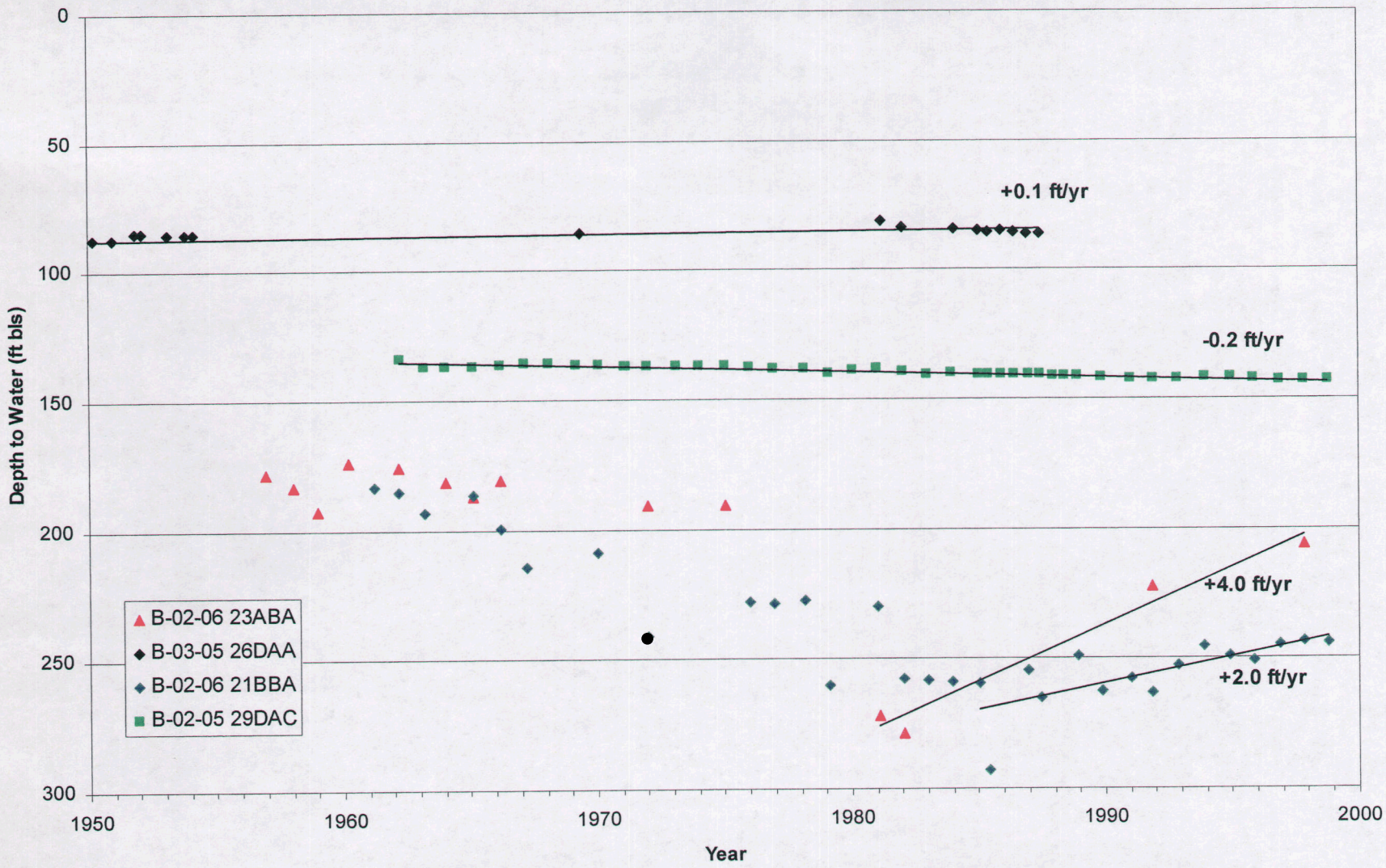
0 3 6

BASE MAP: QuadsUSA v2.52

Southwest Ground-water Consultants, Inc.	DEPTH TO BEDROCK MAP	Figure 4
November 1, 2004 Project B.941	Hassayampa Ranch Maricopa County, Arizona	



Southwest Ground-water Consultants, Inc. November 1, 2004 Project B.941	**GROUND-WATER SURFACE MAP** Hassayampa Ranch Maricopa County, Arizona	**Figure 5**



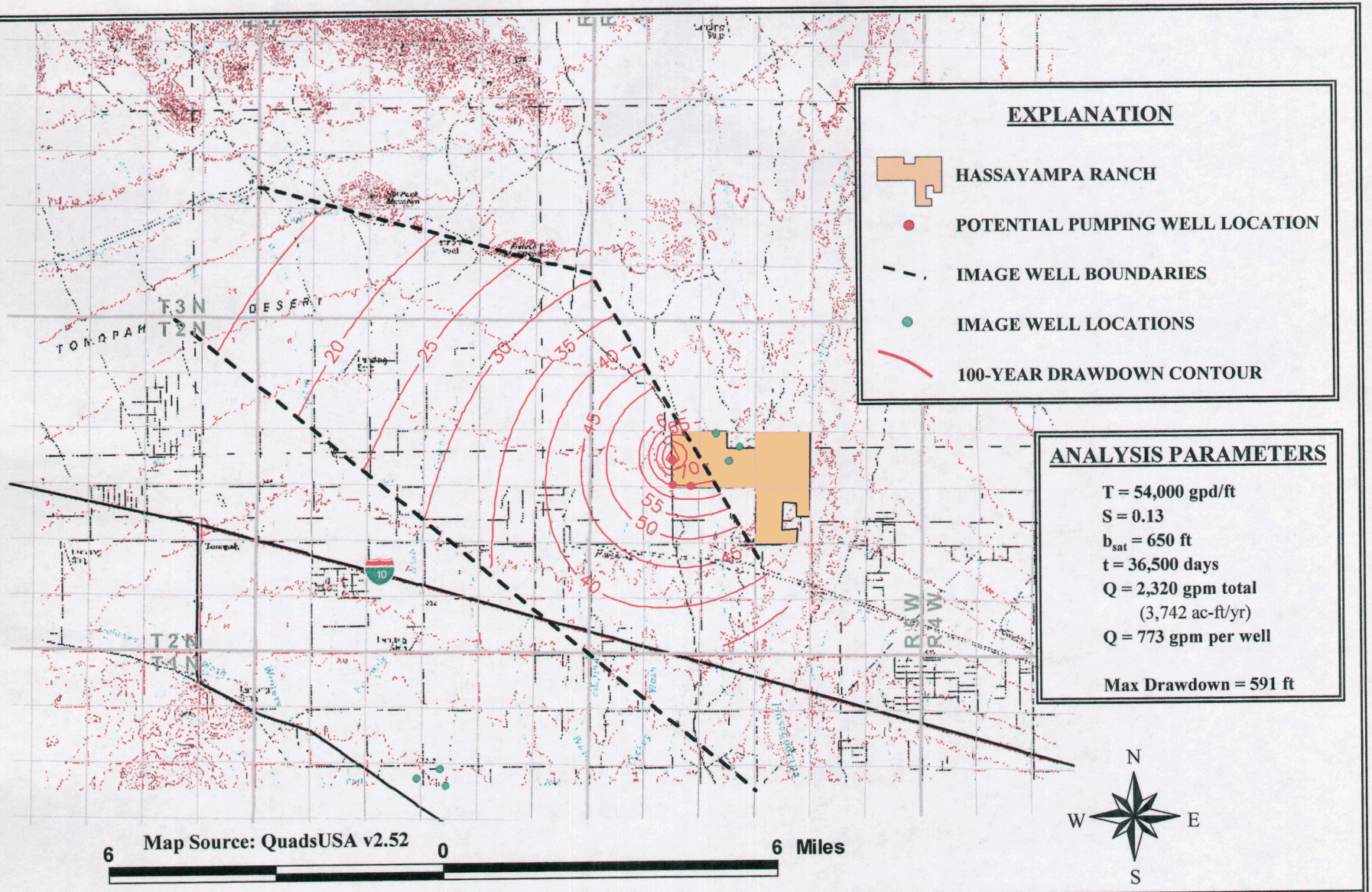
Southwest Ground-water Consultants, Inc.

November 2, 2004 Project B.941

GROUND-WATER HYDROGRAPHS

Hassayampa Ranch
Maricopa County, Arizona

Figure 6



Map Source: QuadsUSA v2.52

Southwest Ground-water Consultants, Inc. November 8, 2004 Project B.941	**100-YEAR AQUIFER IMPACT ANALYSIS** Hassayampa Ranch, Maricopa County, Arizona	**Figure 7**

TABLES

TABLES

TABLE 1
Demand Calculations
Hassayampa Ranch
Harvard Investments

Item	Units	Rate	Demand (ac-ft/yr)
Residential			
Standard Single Family Indoor[1]	5,707 du	57 gpd/c 3.2 c/du	1,166.02
Standard Single Family Outdoor[1]	5,707 du	178 gpd/du	1,137.89
Large Lot Correction[2]	0 du 0 sq ft lot	4.9 ac-ft/ac(turf) 1.5 ac-ft/ac(lwul)	-
Total Residential Demand			**2,303.91**
Non-residential			
Elementary Schools[3]	3,710 students	25 gal/stu/day	122.03
	3.3 ac turf	4.9 ac-ft/ac (turf)	
	1.3 ac lwul	1.5 ac-ft/ac (lwul)	
High Schools[4]	1,427 students	45 gal/stu/day	90.04
	3.3 ac turf	4.9 ac-ft/ac (turf)	
	1.3 ac lwul	1.5 ac-ft/ac (lwul)	
Open Space[5]	27.9 ac turf	4.9 ac-ft/ac(turf)	199.56
	41.9 ac lwul	1.5 ac-ft/ac(lwul)	
Roadways[5]	5.5 ac	1.5 ac-ft/ac	8.25
Commercial, Public Facilities, Mixed Use	97.6 ac	2.25 ac-ft/ac	219.60
Golf Course			456.62
Total Non-residential Demand			**1,096.10**
SF Construction[6]	5,707 du	10,000 g/du	1.75
MF Construction	0 du	5,000 g/du	-
Commercial Construction	79 ac	15,000 g/ac	0.04
Total Construction Demand			**1.79**
System Losses	3,402 ac-ft/yr	10 %	**340.20**
Total Demand			**3,742.00**

[1] No. Of dwelling units (du) per land use plan (WRG, 2004)

[2] Estimated that no lots will exceed 10,000 square feet in size

[3] No. of elementary school students estimated at 0.65 students per du, acreage based on Land Use Plan
On 13.2-acre school site, 25% of acreage estimated as turf, 10% estimated as low water use landscaping (lwul), and 65% estimated as non irrigated

[4] No. of high school students estimated at 0.25 students per du, school acreage based on Land Use Plan
On 13.2-acre school site, 25% of acreage estimated as turf, 10% estimated as low water use landscaping (lwul), and 65% estimated as non irrigated

[5] 10% turf and 15% lwul applied to 279.2 open space acres
6% of roadway acreage estimated as low water use landscaping

[6] Construction demand divided by 100, since construction will only occur once in 100 years

Table 2. Calculation of Area-weighted Average Aquifer Transmissivity

Well #	Transmissivity from Recovery Test (gpd/ft)	Weighting Factor	Column b * c
(a)	(b)	(c)	(d)
2	95,500	0.20	19,100
4	27,400	0.15	4,110
5	47,300	0.15	7,095
6	40,700	0.15	6,105
7	18,900	0.25	4,725
8	128,200	0.10	12,820
Area-weighted average Transmissivity (gpd/ft):			**54,000**

APPENDICES

APPENDICES

APPENDIX A

APPENDIX A

REPORT OF WELL DRILLER – LOG OF WELL

AND

WELL REGISTRY REPORT

STATE OF ARIZONA

DEPARTMENT OF
WATER RESOURCES

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner Butler Dairy
Name
Rt. 2 Box 320 Buckeye Az 85326
Address

2. Lessee or Operator
Name
Address

3. Driller Boots Harder
Name
23,728 Hwy. 85 Buckeye, Az 85326
Address

4. Location of well: NENENE T2N R6W Sec23

5. Permit No. (if issued)

DESCRIPTION OF WELL

6. Total depth of hole 1500 ft.
7. Type of Casing Steel
8. Diameter and length of casing 16 in. from 0 to 1000', in from to .
9. Method of sealing at reduction points
10. Perforated from to , from to , from to
11. Size of cuts Number of cuts per foot
12. If screen was installed: Length 500 ft. Diam 8 in. Type Johnson 100 mesh
13. Method of construction Drilled
drilled, dug, driven, bored, jetted, etc.
14. Date started 11 - 14 - 80
Month day year
15. Date completed 11 29 80
Month day year
16. Depth to water ft. (If flowing well, distinguish
17. Describe point from which depth measurements were made, and give sea-level elevation if available.

18. If flowing well, state method of flow regulation

19. REMARKS: well Deepned from 1000' to 1500' 20' 10" Pipe welded on top of screen over laped from 980'

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
Registration No. 55-85958
Received By
Entered 2-4-81 By
File No. B(2-6)23aaa

(Well log to appear on Reverse side)

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
1000'	1080	Fine Grey sand
1080	1160	Coarse sand + streaks Gravel
1160	1240	sand + small angler Gravel
1240	1320	sand
1320	1400	sand Slightly Cemented
1400	1450	sand + Gravel streaks

ARIZONA WATER COMMISSION
'81 JAN 21 P3:13

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller F.B. Harden
Name

P.O. Box 447 Buckeye
Address

Date 1-5-81

2-73

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
99 EAST VIRGINIA AVENUE
PHOENIX, ARIZONA 85004

RECEIVED JUN 30 1988 DEPT. OF WATER RESOURCES

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner MARICOPA COUNTY ATTORNEY % GENE NEIL
Name
111 W. MONROE STREET, PHOENIX, ARIZONA 85003
Mailing Address

2. Driller ODOM'S INC.
Name
327 N. 1st STREET, BUCKEYE, ARIZONA 85326
Mailing Address

3. Location of well: (C-1-5) 3dab 7 MW-5UA

4. Permit No. 55-521058
(if issued)

DESCRIPTION OF WELL

5. Total depth of hole 95 ft.

6. Type of casing STEEL

7. Diameter and length of casing 12 in. from 0 to 19, 8 in from 0 to 62, 4-inch casing from 0 to 95

8. Method of sealing at reduction points

9. Perforated from 65 to 95, from to , from to .

10. Size of cuts 3" x 1/8" Number of cuts per foot 16

11. If screen was installed: Length ft. Diam in. Type

12. Method of construction DRILLED - MUD ROTARY
drilled, dug, driven, bored, jetted, etc.

13. Date started MAY 9 1988
Month Day Year

14. Date completed MAY 25 1988
Month Day Year

15. Depth to water 73 ft. (If flowing well, so state.)

16. Describe point from which depth measurements were made, and give sea-level elevation if available TEMPORARY MEASURING POINT - TOP OF 4-INCH CASING.

17. If flowing well, state method of flow regulation:

18. Remarks:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
REG. NO. 55-521058
File No. C(1-5)3dab 7
ENTERED JUL 11 1988
Entered By

DWR-55-6-Rev. 8/85

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	22	Gravelly, Silty Sand
22	31	Silty Sand
31	44	Sandy, Clayey Silt
44	51	Silty Clay
51	72	Basalt
72	80	Clayey Silt
80	92	Clayey, Silty Sand
92	95	Sandy, Silty Clay

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller E. R. Parker

Name E. RAY PARKER

327 N. 1st STREET

Address

BUCKEYE, ARIZONA 85326

City State Zip

Date JUNE 27, 1988

DEPARTMENT OF WATER RESOURCES
15 South 15th Avenue
Phoenix, Arizona 85007

Registration No. 55-521058

File No. (C-1-5)3dab7[Mw-5UA]

COMPLETION REPORT

1. Per A.R.S. §45-600, the Completion Report is to be filed with the Department within 30 days after installation of pump equipment by the registered well owner.
2. Drawdown of the water level for a non-flowing well should be measured in feet after not less than 4 hours of continuous operation and while still in operation and for a flowing well the shut-in pressure should be measured in feet above the land or in pounds per square inch at the land surface.
3. The static groundwater level should be measured in feet from the land surface immediately prior to the well capacity test.
4. The tested pumping capacity of the well in gallons per minute for a non-flowing well should be determined by measuring the discharge of the pump after continuous operation for at least 4 hours and for a flowing well by measuring the natural flow at the land surface.

RECEIVED FEB 3 1989 DEPT. OF WATER RESOURCES

LOCATION OF THE WELL:

1 South	5 West	3	NW NE SE
Township	Range	Section	¼ ¼ ¼

EQUIPMENT INSTALLED:

Kind of pump Submersible
Turbine, centrifugal, etc.

Kind of power Electric H.P. Rating of Motor 1/3
Electric, natural gas, gasoline, etc.

Pumping Capacity 6.2 Date pump installed: 8-9-88
Gallons per minute

WELL TEST:

Test pumping capacity 5.2 Date Well Tested: 6-30-88
Gallons per minute

Method of Discharge Measurement Calibrated bucket and stopwatch
Weir, orifice, current meter, etc.

Static Groundwater Level 81.12 ft. Drawdown 12.41 ft.

Total Pumping Lift 83 ft. Drawdown _____ lbs.
(Flowing Well)

I HEREBY CERTIFY that the above statements are true to the best of my knowledge and belief.

Maricopa County Attorney c/o Gene Neil
Print Well Owner's Name

February 1, 1989
Date

William R. Vietz (Consultant)
Signature of Well Owner or Agent

Maricopa County Attorney c/o Gene Neil
111 West Monroe Street
Phoenix, Arizona 85003

ERROL L. MONTGOMERY & ASSOCIATES, INC.
Address
1075 East Fort Lowell Road, Suite B
Tucson, Arizona 85719
City State Zip

DWR-55-7-11/88

ENTERED FEB 08 1989

ARIZONA DEPARTMENT OF WATER RESOURCES
500 North Third Street
Phoenix, Arizona 85004

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within ~~30 days following~~ completion of the well.

RECEIVED OCT 30 2000 RECORDS MGT

1. Drilling Firm: LAYNE CHRISTENSEN COMPANY
12030 E. RIGGS ROAD
CHANDLER, AZ 85249

2. Owner Name: Triple G Farms

Address: 29111 W. Broadway
Buckeye, Az. 85326
City State Zip Telephone Number

3. Location: 1 N/S 4 E/W 29 SE 3 NW 3 NW 3
Township Range Section 10-acre 40-acre 160-acre

4. Well Registration No. 55-582083 (Required)
5. Permit No. _____ (If issued)

DESCRIPTION OF WELL

6. Total depth of hole 1500 ft.
7. Type of casing
8. Diameter and length of casing 16 in. from +2' to 1500 in from _____ to
9. Method of sealing at reduction points
10. Perforated from 898 to 1480, from _____ to _____, from _____ to
11. Size of cuts 1/10" x 2.5 Number of cuts per foot 24
12. If screen was installed: Length _____ ft. Diameter _____ in. Type
13. Method of construction Reverse Air
14. Date started 8-19-2000
15. Date completed 9-26-2000
16. Depth to water 121 ft. (If flowing well, so state)
17. Describe point from which depth measurements were made, and give sea-level elevation if available 2' above Ground
18. If flowing well, state method of flow regulation:
19. Remarks: _____

DO NOT WRITE IN THIS SPACE
OFFICE RECORD

Registration No. 55-582083
File No. B (1-4) 29 BBD
Received _____ By
Entered _____ By

DWR-55-55-3/2000 (Rev.)

ANSWERED NOV 22 2000

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	
0	280	Sand Grave
280	580	Red Clay, Gravel / Sand layers
580	700	Sandstone Clay
700	866	Small Gravel, Sand and Clay
866	1400	Rocks Gravel and Sand
1400	1500	Sand Gravel Rocks - Some Clay

I hereby certify that this well was drilled by me (or under my supervision), and that each and all statements herein contained are true to the best of my knowledge and belief.

Drilling Firm: Layne Christensen Company

Signature of Qualifying Party: Don Sawada Date: 10/26/2000

Street: 12030 E. Riggs Rd.

City: Chandler State: AZ Zip: 85249

DWR 55-55 (Rev 1/99)

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
99 EAST VIRGINIA AVENUE
PHOENIX, ARIZONA 85004

STATE OF ARIZONA

DEPARTMENT OF WATER RESOURCES

MAY 1985

DEPARTMENT OF WATER RESOURCES

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner Empire Farms Co.
Name

Po. Box 698 Eloy Az. 85231
Address

2. Lessee or Operator
Name

Address

3. Driller J. O. Barnes Casa Grande - Sub. Cont. Thompson Drilling
Name

St. Rt. 2 Box 668 Tonopah Az. 85354
Address

4. Location of well: Toltec Rd.

5. Permit No. (if issued)

DESCRIPTION OF WELL

6. Total depth of hole 2,000 ft.

7. Type of Casing Steel

8. Diameter and length of casing 16 in. from 0' to 2,000, in from to .

9. Method of sealing at reduction points none

10. Perforated from 1400 to 2,000, from to , from to

11. Size of cuts 3/16 x 3 Number of cuts per foot 32

12. If screen was installed: Length ft. Diam in. Type

13. Method of construction Drilled
drilled, dug, driven, bored, jetted, etc.

14. Date started 2 (Month) 29 (day) 84 (year)

15. Date completed 4 (Month) 24 (day) 84 (year)

16. Depth to water approx. 450 ft. (If flowing well, so state.)

17. Describe point from which depth measurements were made, and give sea-level elevation if available.:

18. If flowing well, state method of flow regulation

19. REMARKS: 20' of Surface pipe set and Cemented

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
Registration No. 55-507366
Received By
Entered 6.6.85 By
File No. B(1-5)28 bbb

(Well log to appear on Reverse side)

DWR-55-6-5/83

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	40	Surface sand & Gravel
40	137	Pea Gravel With Boulders & sand
137	358	sand, gravel with streaks of clay
358	800	sandy clay &silt
800	1480	silty clay with small streaks of gravel
1480	1720	silty sand with streaks of clay
1720	1848	silty clay & gravel
1848	2000	fine gravel

I hereby certify that this well was drilled by me (or under my supervison), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller Eldon Thompson
Name

ST. RT. 2 Box 168
Address

TONOPAH AZ. 85354
City State Zip

Date 5-8-85

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
15 South 15th Avenue
Phoenix, Arizona 85007

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner BRM Project
   Name
   4520 North Central Ave Suite #500 Phoenix, Arizona 85012
   Mailing Address
2. Driller Universal Drilling
   Name
   P.O. Box 1027 Wickenburg, Arizona 85358
   Mailing Address
3. Location of well: 2N, 6W, 7Sec, NE,NE,NW
4. Permit No. 55-525593
   (If issued)

DESCRIPTION OF WELL

5. Total depth of hole 1200 ft.
6. Type of casing Steel
7. Diameter and length of casing 8 in. from 0 to 20, 6 in from 0 to 807.
8. Method of sealing at reduction points Cement grout
9. Perforated from 280 to 800, from ____ to ____, from ____ to ____.
10. Size of cuts 3/16 X 3 Number of cuts per foot 18
11. If screen was installed: Length N/A ft. Diam ____ in. Type ____
12. Method of construction Drilled
    drilled, dug, driven, bored, jetted, etc
13. Date started Oct (Month) 18, (Day) 1989 (Year)
14. Date completed Nov (Month) 4, (Day) 19[illegible]
15. Depth to water 170 ft. (If flowing well so state)
16. Describe point from which depth measurements were made, and give sea-level elevation if available N/A
17. If flowing well, state method of flow regulation: N/A
18. Remarks:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
REG. No. 525593
File No. B(2-6)7 bAA
Entered ____ By ____
ENTERED JAN 05 1990

MICROFILMED

RECEIVED
FEB 28 1990

DWR-55-55-2/89

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	180	Gravel, clay, boulders
180	230	Brown, red clay, small gravel
230	310	Brown clay granite Quartz
310	340	Material is more tightly formed
340	390	Brown clay, more gravel
390	510	Brown clay, very small amount gravel and sand
510	1200	More brown clay very little change

I hereby certify that this well was drilled by me (or under my supervision), and that each and all statements herein contained are true to the best of my knowledge and belief.

Driller Steve Roberts
Name

P.O. Box 1027
Address

Wickenburg, Arizona 85358
City State Zip

Date December 27, 1989

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
15 South 15th Avenue
Phoenix, Arizona 85007

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner BRM Project
   Name
   4520 North Central Suite# 500 Phoenix, Arizona 85012
   Mailing Address
2. Driller Universal Drilling
   Name
   P.O. Box 1027 Wickenburg, Arizona 85358
   Mailing Address
3. Location of well: T 2N, R 6W, Sec 16 SW,SW,SE
4. Permit No. 59-525594
   (If issued)

DESCRIPTION OF WELL

5. Total depth of hole 1200 ft.
6. Type of casing Steel
7. Diameter and length of casing 8 in. from 0 to 20, 6 in from 0 to 807.
8. Method of sealing at reduction points Cement grout
9. Perforated from 200 to 800, from ____ to ____, from ____ to ____.
10. Size of cuts 3/16 X 3 Number of cuts per foot 18
11. If screen was installed: Length N/A ft. Diam ____ in. Type ____
12. Method of construction Drilled
    drilled, dug, driven, bored, jetted, etc
13. Date started October 3, 1989
    Month Day Year
14. Date completed October 31, 1989
    Month Day Year
15. Depth to water 420 ft. (If flowing well, so state)
16. Describe point from which depth measurements were made, and give sea-level elevation if available N/A
17. If flowing well, state method of flow regulation: N/A
18. Remarks:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
REG. No. 525594
File No. B(2-6)16dcc
Entered ENTERED JAN 05 1990 By

MICROFILMED

RECEIVED
2 8 1990
OPERATIONS

DWR-55-6-Rev. 2/89

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	140	Gravel, clay
140	180	Red clay
180	250	Clay mixed with gravels
250	410	Sand and clay
410	420	Gravel
420	490	Mixed volcanics and clay
490	830	Brown clay and gravel
830	1200	Gravel, quartz, volcanics, granite

I hereby certify that this well was drilled by me (or under my supervision), and that each and all statements herein contained are true to the best of my knowledge and belief.

Driller Steve Roberts
Name

P.O. Box 1027
Address

Wickenburg, Arizona 85358
City State Zip

Date December 27, 1989

STATE OF ARIZONA

DEPARTMENT OF
WATER RESOURCES

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner Butler Dairy
Name
Rt. 2, Box 320, Buckeye, Arizona 85326
Address

2. Lessee or Operator
Name
Address

3. Driller Odom Drilling
Name
327 N. 1st St. Buckeye, Arizona 85326
Address

4. Location of well: T2N, R6W, Sec. 23, NW¼ NW¼ NE¼

5. Permit No. Q-506815
(if issued)

DESCRIPTION OF WELL

6. Total depth of hole 1004 ft.

7. Type of Casing Steel

8. Diameter and length of casing 16 in. from 0 to 560, in from to .

9. Method of sealing at reduction points

10. Perforated from 424' to 984', from to , from to

11. Size of cuts 3/16" x 2½" Number of cuts per foot 40

12. If screen was installed: Length ft. Diam in. Type

13. Method of construction Drilled
drilled, dug, driven, bored, jetted, etc.

14. Date started January (Month) 23 (day) 1984 (year)

15. Date completed April (Month) 17 (day) 1984 (year)

16. Depth to water 190 ft. (If flowing well, so state.)

17. Describe point from which depth measurements were made, and give sea-level elevation if available.
GROUND

18. If flowing well, state method of flow regulation

19. REMARKS:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
Registration No. 55-506815
Received By
Entered 4-30-84 By
File No. B(2-6)23 abb

(Well log to appear on Reverse side)

RECEIVED
APR 30 1984
DEPT. OF
WATER RESOURCES

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	8	Rock and caliche
8	20	Sandy clay and gravel
20	45	Sand & gravel
45	50	Clay
50	65	Sand & gravel
65	80	Sandy clay
80	95	Clay
95	100	Sand
100	120	Sandy clay
120	125	Sand
125	135	Silty clay
135	205	Sandy clay (Poor Formation)
205	210	Quick sand (1st Water)
210	275	Yellow clay
275	285	Red clay
285	355	Clay
355	360	Slab clay
360	455	Clay
455	460	Sand
460	495	Clay
495	735	Sand & clay streaks
735	775	Quartz rock & sand
775	785	Quartz rock (hard & sharp)
785	805	Conglomerate (sand, gravel & clay
805	810	Sand
810	910	Granite conglomerate
910	950	Granite conglomerate (lots of clay)
950	970	Granite conglomerate
970	1004	Granite Conglomerate (Lots of clay)

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller ODOM'S INC.
Name

327 N. 1st St., Buckeye, Az. 85326
Address

Date 4-24-84

2-72

OF ARIZONA

ARIZONA WATER COMMISSION
WATER RIGHTS ADMINISTRATION

2

Butler Dairy

REPORT OF WELL DRILLER

NEW WELL (#2)
Active

This report should be prepared by the driller in all detail and filed with the Az. Water Commission following completion of the well.

1. OWNER K. O. Butler
Name
Address

2. Lessee or Operator
Name
Address

3. DRILLER Harder Drilling Co. INC.
Name
Address

4. Location of well: Twp. 2N Rge. 6W Section 23 NE ¼ NE ¼ NE ¼
10-acre subdivision

5. Intention to Drill File No. Permit No.

DESCRIPTION OF WELL

6. Total depth of hole 1000 ft.

7. Type of casing Steel

8. Diameter and length of casing 16 in. from 0 to 1000, in. from to, in. from to

9. Method of sealing at reduction points

10. Perforated from 400' to 1000', from to, from to, from to

11. Size of cuts 3/16" Number of cuts per foot 24

12. If screen was installed: Length ft. Diam in. Type

13. Method of construction Drilled
drilled, dug, driven, bored, jetted, etc.

14. Date started 5 (Month) 27 (Day) 80 (Year)

15. Date completed 8 (Month) 28 (Day) 80 (Year)

16. Depth to water ft.
If flowing well, so state.

17. Describe point from which depth measurements were made, and give sea-level elevation if available. Ground level

18. If flowing well, state method of flow regulation

19. REMARKS:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD

Received by
Filed 5-17-80 by Ol
File No. B(2-6)23 aaa
- 35-83325

(Well Log to Appear on Reverse Side)

WD FORM G-301
REV. 4-27-53

INDEXED

2

RECEIVED
SEP 10 1980
ARIZONA WATER
COMMISSION

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

FROM (FEET)	TO (FEET)	DESCRIPTION OF FORMATION MATERIAL
0	20	surface Sand + Gravel
20	120	Small Gravel Angular
120	160	Sand + Small Gravel
160	220	Sand
220	340	Clay with Sand streaks
340	400	Clay
400	500	Sand with streaks Sand
500	600	Clay
600	780	Clay with Sand + Gravel
780	1800	Sand.

MICROFILMED

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller F. K. Harder
Name

P.O. Box 447 Buckeye Az.
Address

DEPARTMENT OF WATER RESOURCES
99 East Virginia
Phoenix, Arizona 85004

Registration No. 506815
Owner of Well Site Butler Dairy
File No. B(2-6)23 abb

COMPLETION REPORT

1. Per A.R.S. §45-600, the Completion Report to be filed with the Department within 30 days after installation of pump equipment by the registered well owner.
2. Drawdown of the water level for a non-flowing well should be measured in feet after not less than 4 hours of continuous operation and while still in operation and for a flowing well the shut-in pressure should be measured in feet above the land or in pounds per square inch at the land surface.
3. The static groundwater level should be measured in feet from the land surface immediately prior to the well capacity test.
4. The tested pumping capacity of the well in gallons per minute for a non-flowing well should be determined by measuring the discharge of the pump after continuous operation for at least 4 hours and for a flowing well by measuring the natural flow at the land surface.

LOCATION OF THE WELL:

2N	6W	23	NW NW NE
Township	Range	Section	¼ ¼ ¼

EQUIPMENT INSTALLED:

Kind of pump TURBINE
Turbine, centrifugal, etc.

Kind of power Electric H.P. Rating of Motor 150
Electric, natural gas, gasoline, etc.

Pumping Capacity 1200 Date installed 5/11/84
Gallons per minute

WELL TEST:

Test pumping capacity 1200 Date Well Tested 4/27/84
Gallons per minute

Method of Discharge Measurement ORIFICE
Weir, orifice, current meter, etc.

Static Groundwater Level 295 ft. Drawdown 131 ft.

Total Pumping Lift 426 ft. Drawdown _____ lbs
(Flowing Well)

I HEREBY CERTIFY that the above statements are true to the best of my knowledge and belief.

February 10, 1985
DATE

Signature

4532 E. Washington
Address

Phoenix AZ
City State Zip

DWR-55-7-3/84

PHONE 273-1321

Gilbert PUMP AND EQUIPMENT COMPANY

P. O. BOX 20216
4532 EAST WASHINGTON STREET
PHOENIX, ARIZONA 85036

December 8, 1983

Butler Dairy
Buckeye, Arizona
Attention: Mr. K. O. Butler

Gentlemen:

The production efficiency of the two wells is not typical of the area. The rotary drilling samples (1/2/81) of the #2 well indicated a lot of tight clay and fine sand formations. The well has improved efficiency the more it has been pumped. The #1 well production (gallons/ft./d.d.) has dropped off probably due to perforation blockage and tight bottom fill.

Trusting this is the information you desire and if you have any questions, please call us at 273-1321.

Very truly yours,

GILBERT PUMP & EQUIPMENT CO., INC.

Gayle E. Eckleberry

GAYLE E. ECKLEBERRY
Sales Engineer

GEE:bsd

#1 (OLD) WELL APPROXIMATELY - 1800 GPM
PUMPING LEVEL - 312 Ft.
FRICTION LOSS - 16 Ft.
328 Ft. total DYNAMIC HEAD

P.L. - 312'
STATIC - 261'
51' DRAWDOWN

GPM / Ft. DRAWDOWN = 35.29

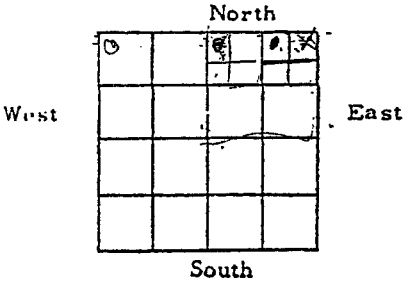
MICROFILMED

#1 westwell EXTENDED

STATE LAND DEPARTMENT
Water Division
Phoenix, Arizona

File No. (B-2-6)23 aab

Location of Well



(Indicate Well Location by a circle "o" in the above Section Plat)

REPORT OF EQUIPMENT INSTALLED

OWNER Thornton Lumber Co.

LOCATION OF WELL:

NW¼ NW¼ NE¼, Sec. 23 Twp. 2N Rge. 6W

Date Well Completed: 3-8-62 Depth 1000'

1. Well Test:

Discharge: 1600 (Gal. Per Min.) Date Well Tested: May 17, 1962

Method of Discharge Measurement: ~~Current meter~~ Orifice (weir, orifice, current meter, etc.)

Static Water Level: 192 ft. Drawdown 80 ft.

Total Pumping Lift 272 ft.

2. Equipment Installed:

Kind of Pump: ~~10" x 2½" x 1 11/16" 4-stage 14"OD FLOWAY Turbine~~ (turbine, centrifugal, etc.)

Kind of Power: Elec (Elec., Nat. Gas, Etc.) H. P. Rating of Motor 150

I HEREBY CERTIFY that all the above statements are true to the best of my knowledge and belief.

[illegible]
(Signature)

Date May 23, 1962, 19____.

4029 E. Patricia Jane Drive
Phoenix 18, Arizona
(Address)

WD Form G-306
10-57

MICROFILMED

12/12/1983

Butler Dairy
Replacement well B(2-6)23 abb

1. Pump capacity 1800 gpm
2. Actual pumping rate on a continuous basis
   days pumped 140/yr at 690 gpm

3. Transmissivity = 44,000 gpd/ft (average from 2 exist wells)
4. Specific yield = 0.10 (assumed)
5. Review period 5 years = 1825 days

Hydrologic calculations:

1. Radius of the 10 foot drawdown

$$W(u) = \frac{T\Delta s}{114.6 \times Q} = \frac{44{,}000 \times 10'}{114.6 \times 690\ gpm} = 5.5644$$

$$u = 2.2 \times 10^{-3}$$

$$r = \sqrt{\frac{44{,}000 \times 1825 \times (2.2 \times 10^{-3})}{1.87 \times 0.1}} = 971\ feet$$

2. Radius of the 25 foot drawdown

$$W(u) = \frac{44{,}000 \times 25'}{114.6 \times 690\ gpm} = 13.9 \quad u = 5.1 \times 10^{-7}$$

DR-3

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
99 EAST VIRGINIA AVENUE
PHOENIX, ARIZONA 85004

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner Douglas Land Corp.
   Name
   767 5th Ave. 7th Floor, New York NY 10153
   Mailing Address
2. Driller Western Well & Pump, Inc.
   Name
   120 North 44th Street #100 Phoenix, Arizona 85034
   Mailing Address
3. Location of well: Section 10, TWP 3N, Range 5W, Near CAP canal, powerlines
4. Permit No. (if issued) N/A

DESCRIPTION OF WELL

5. Total depth of hole ~~1000~~ 1019 ft.
6. Type of casing Steel
7. Diameter and length of casing 10 in. from 0 to 20, 6 in from 0 to 1,000'
8. Method of sealing at reduction points N/A
9. Perforated from 500 to 1,000, from - to -, from - to -.
10. Size of cuts 1/8" X 3 Number of cuts per foot 20
11. If screen was installed: Length - ft. Diam - in. Type -
12. Method of construction Drilled rotary method
    drilled, dug, driven, bored, jetted, etc.
13. Date started April (Month) 16 (Day) 1987 (Year)
14. Date completed April (Month) 20 (Day) 1987 (Year)
15. Depth to water 172 ft. (If flowing well, so state.)
16. Describe point from which depth measurements were made, and give sea-level elevation if available Top of 6" steel casing
17. If flowing well, state method of flow regulation: N. A.
18. Remarks:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
REC. NO. 55-~~516598~~ 516562
File No. B(3-5)10 aca
Entered ENTERED SEP 22 1987 By

DWR-55-6-Rev. 8/85

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	20	Caliche
20	30	Sandy gravel
30	40	Fine sand, no gravel
40	50	Some cobbles, then suddenly claye sand
50	60	Sandy clay
60	70	Sandy clay, some cobble
70	80	Sandy clay
80	90	Clay some sand
90	100	Clay, little sand
100	110	" " "
110	120	" " "
120	130	" " "
130	140	Clay
140	150	Sand
150	160	"
160	170	Sandy clay
170	180	" "
180	190	Sand
190	200	"
200	210	Gravel and clay
210	220	Sandy clay
220	230	" "
230	250	" "
250	270	" "
270	300	Gravel, some clay ...continued on separate sheet...

I hereby certify that this well was drilled by me (or under my supervision), and that each and all of the statements herein contained are true to the best of my knowledge and belief.

Driller Gary L. Fix
Name

WESTERN WELL & PUMP, INC.
120 No. 44th St. #100
Address

Phoenix, Arizona 85034
City State Zip

Date 5/18/87

LOG OF WELL

icate depth at which water was first encountered, and the depth and thickness of water aring beds. If water is artesian, indicate depth at which encountered, and depth to nich it rose in well.

From (feet)	To (feet)	Description of formation material
300	310	Gravel, some clay
310	380	Sandy clay
380	450	Sandy clay
450	490	" "
490	500	Sand
500	600	Sandy clay, and gravel
600	700	" " " "
700	710	" " "
710	770	Gravel and clay
770	870	Gravel and clay St.
870	1000	Clay and gravel

MICROFILMED

9. Groundwater to be withdrawn by means of:

A. Existing wells:

Registration No.	Location	Depth	Casing	Case Type
55-_____	_____	_____	_____	_____
55-_____	_____	_____	_____	_____

B. New wells:

Registration No. (Dept. to Complete)	Location	Depth	Casing	Case Type
55-_____	B(03-05)10aca	1200	0-1200	steel
55-_____	_____	_____	_____	_____
55-_____	_____	_____	_____	_____

10. State your plans for the well(s) after testing is completed:

Weld on tamper-proof steel cap with water level access port.

11. If new well(s) is to be drilled, complete the following information relating to the driller:

Driller's name Curt Tyler Rival Waterwell Specialties DWR License No. 455

Address 7803 Shotner Lane

Bakersfield, CA 93308

It is understood that the Permit, if granted, will be in accordance with the Groundwater Management Code (Title 45, Chapter 2). The permittee will be bound by the provisions of such law and the provisions of the Permit issued.

Signature of Applicant [signature] Date 01-18-87

MICROFILMED

DEPARTMENT OF WATER RESOURCES
99 East Virginia
Phoenix, Arizona 85004

RECEIVED AUG 27 1987 DEPT. OF WATER RESOURCES

Registration No. 55-516562

Owner of Well Site Hargis + Associates, Inc.

File No. B(3-5)10 aca

COMPLETION REPORT

1. Per A.R.S. §45-600, the Completion Report to be filed with the Department within 30 days after installation of pump equipment by the registered well owner.
2. Drawdown of the water level for a non-flowing well should be measured in feet after not less than 4 hours of continuous operation and while still in operation and for a flowing well the shut-in pressure should be measured in feet above the land or in pounds per square inch at the land surface.
3. The static groundwater level should be measured in feet from the land surface immediately prior to the well capacity test.
4. The tested pumping capacity of the well in gallons per minute for a non-flowing well should be determined by measuring the discharge of the pump after continuous operation for at least 4 hours and for a flowing well by measuring the natural flow at the land surface.

LOCATION OF THE WELL:

N3	5W	10	NE SW NE
Township	Range	Section	¼ ¼ ¼

EQUIPMENT INSTALLED:

Kind of pump Submersible (Termporary installation for testing)
Turbine, centrifugal, etc.

Kind of power Electric H.P. Rating of Motor 32
Electric, natural gas, gasoline, etc.

Pumping Capacity Temporary Date installed Tempoary
Gallons per minute

WELL TEST:

Test pumping capacity 260 Date Well Tested 05-05-87
Gallons per minute

Method of Discharge Measurement Current Meter
Weir, orifice, current meter, etc.

Static Groundwater Level 172 ft. Drawdown 119 ft.

Total Pumping Lift Tempoary ft. Drawdown N/A lbs
(Flowing Well)

I HEREBY CERTIFY that the above statements are true to the best of my knowledge and belief.

July 7, 19 87
DATE

Signature

2222 South Dobson Road, Suite 401
Address

Mesa, Arizona 85202
City State Zip

RECEIVED JUL 9 1987 DEPT. OF WATER RESOURCES

DWR-55-7-3/84

ENTERED AUG 31 1987

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
15 South 15th Avenue
Phoenix, Arizona 85007

Well No. 8

CORRECT INFORMATION IS:
Registration No.: 55-525592
Location: B(3-6)33ddd
Permit No. 59-525492

OCT - 1 1990

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner BRM Project
Name
4520 North Central Ave Suite #500 Phoenix, Arizona 85012
Mailing Address

2. Driller Universal Drilling
Name
P.O. Box 1027 Wickenburg, Arizona 85358
Mailing Address

3. Location of well: [redacted]

4. Permit No. [redacted]
(If issued)

DESCRIPTION OF WELL

5. Total depth of hole 1200 ft.
6. Type of casing 8" Steel Surface
7. Diameter and length of casing 8 in. from 0 to 20, 6 in from 0 to 888.
8. Method of sealing at reduction points Cement grout
9. Perforated from 485 to 885, from ____ to ____, from ____ to ____.
10. Size of cuts 3/16 X 3 Number of cuts per foot 18
11. If screen was installed: Length n/a ft. Diam ____ in. Type ____
12. Method of construction Drilled
drilled, dug, driven, bored, jetted, etc
13. Date started Sept (Month) 5, (Day) 1989 (Year)
14. Date completed Nov (Month) 1, (Day) 1989 (Year)
15. Depth to water 460 ft. (If flowing well, so state)
16. Describe point from which depth measurements were made and give land level elevation if available N/A
17. If flowing well, state method of flow regulation: N/A
18. Remarks:

RECEIVED
OCT 28 1990

DO NOT WRITE IN THIS SPACE
OFFICE USE
REG. No.
File No.
Entered ENTERED OCT 11 1990 By
B(3-6)33ddd
525592

DWR-55-55-2/89

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	80	Sand, Gravel, boulders, some clay
80	170	Cemented sands, some clay
170	300	Sand gravel, Some clay
300	460	Gravels, Red volcanics with boulders
460	500	Quartz to Volcanics, Schist, some boulders
500	520	Conglomerte
520	630	Sand gravel, some clay
630	720	Conglomerte, some boulders
720	740	Sand and clay
740	880	Conglomerte, gravels and clay
880	1050	Red volcanics, clay and gravel
1050	1060	Volcanics, gravel, gray and red gravel, Hard
1060	1190	Brown clay, some volcanics
1190	1200	Black volcanics

I hereby certify that this well was drilled by me (or under my supervision), and that each and all statements herein contained are true to the best of my knowledge and belief.

Driller Steve Rotarto
Name

P.O. Box 1027
Address

Wickenburg, Arizona 85358
City State Zip

Date December 27, 1989

OCT - 1 1990

STATE OF ARIZONA
DEPARTMENT OF WATER RESOURCES
15 South 15th Avenue
Phoenix, Arizona 85007

WELL DRILLER REPORT

This report should be prepared by the driller in all detail and filed with the Department within 30 days following completion of the well.

1. Owner BRM Project
   Name
   4520 North Central Ave Suite #500 Phoenix, Arizona 85012
   Mailing Address

2. Driller Universal Drilling
   Name
   P.O. Box 1027 Wickenburg, Arizona 85358
   Mailing Address

3. Location of well: [redacted]

4. Permit No. [redacted]
   (If issued)

DESCRIPTION OF WELL

5. Total depth of hole 1200 ft.
6. Type of casing 8" Steel Surface
7. Diameter and length of casing 8 in. from 0 to 20, 6 in from 0 to 888.
8. Method of sealing at reduction points Cement grout
9. Perforated from 485 to 885, from ____ to ____, from ____ to ____.
10. Size of cuts 3/16 X 3 Number of cuts per foot 18
11. If screen was installed: Length n/a ft. Diam ____ in. Type ____
12. Method of construction Drilled
    drilled, dug, driven, bored, jetted, etc
13. Date started Sept (Month) 5, (Day) 1989 (Year)
14. Date completed Nov (Month) 1, (Day) 1989 (Year)
15. Depth to water 460 ft. (If flowing well, so state)
16. Describe point from which depth measurements were made, and give sea-level elevation if available N/A
17. If flowing well, state method of flow regulation: N/A
18. Remarks:

DO NOT WRITE IN THIS SPACE
OFFICE RECORD
REG. No. 52559
File No. B(3-4)34 ccc
Entered ____ By ____

RECEIVED
DEC 28 1989
DWR

DWR-55-55-2/89

LOG OF WELL

Indicate depth at which water was first encountered, and the depth and thickness of water bearing beds. If water is artesian, indicate depth at which encountered, and depth to which it rose in well.

From (feet)	To (feet)	Description of formation material
0	80	Sand, Gravel, boulders,ssome clay
80	170	Cemented sands, some clay
170	300	Sand gravel, Some clay
300	460	Gravels, Red volcanics with boulders
460	500	Quartz to Volcanics, Schist, some boulders
500	520	Conglomerte
520	630	Sand gravel, some clay
630	720	Conglomerte, some boulders
720	740	Sand and clay
740	880	Conglomerte, gravels and clay
880	1050	Red volcanics, clay and gravel
1050	1060	Volcanics, gravel, gray and red gravel, Hard
1060	1190	Brown clay, some volcanics
1190	1200	Black volcanics

I hereby certify that this well was drilled by me (or under my supervision), and that each and all statements herein contained are true to the best of my knowledge and belief.

Driller Steve Roberts
Name

P.O. Box 1027
Address

Wickenburg, Arizona 85358
City State Zip

Date December 27, 1989

APPENDIX B

APPENDIX B

BELMONT EXPLORATORY WELL DATA

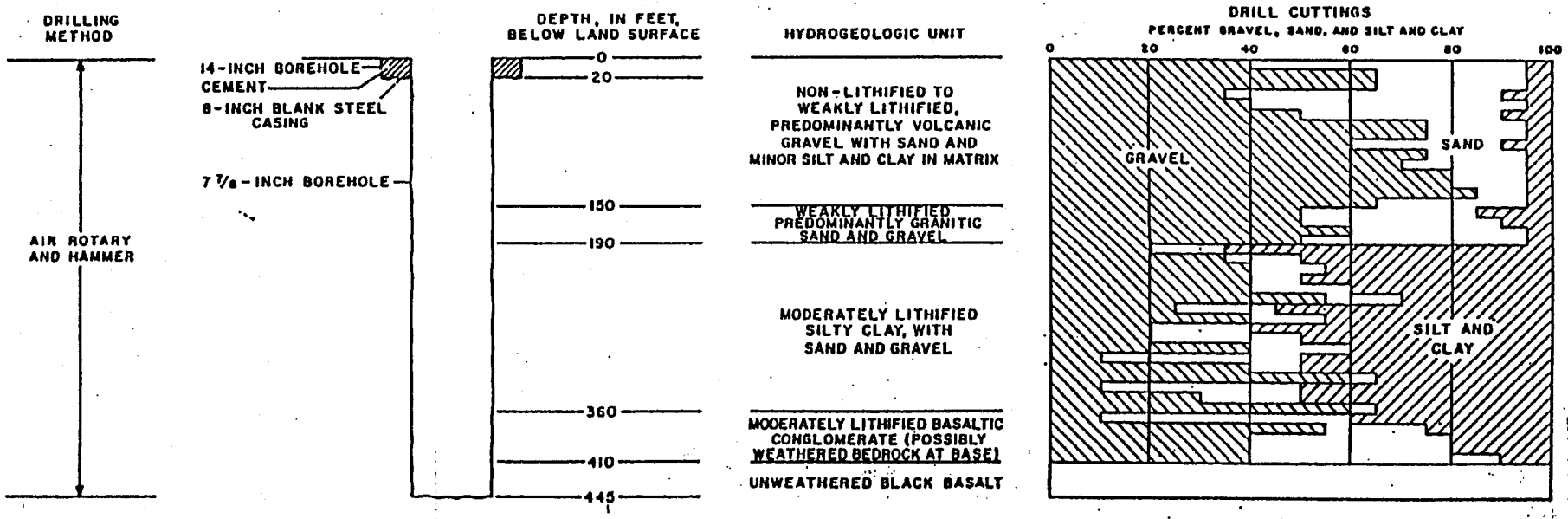
Well Construction

Borehole Lithology

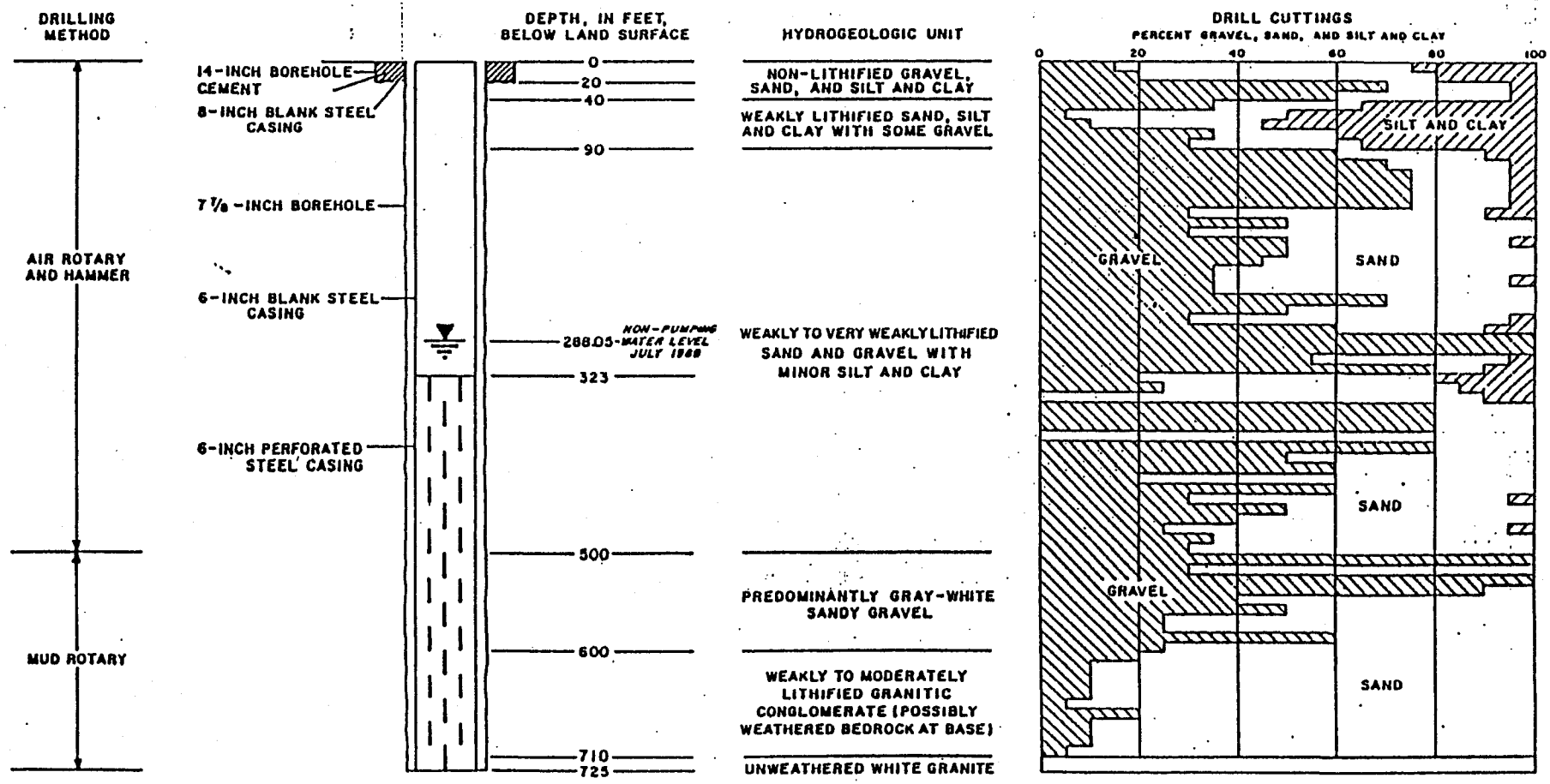
Geologic Cross Sections

Aquifer Test Data

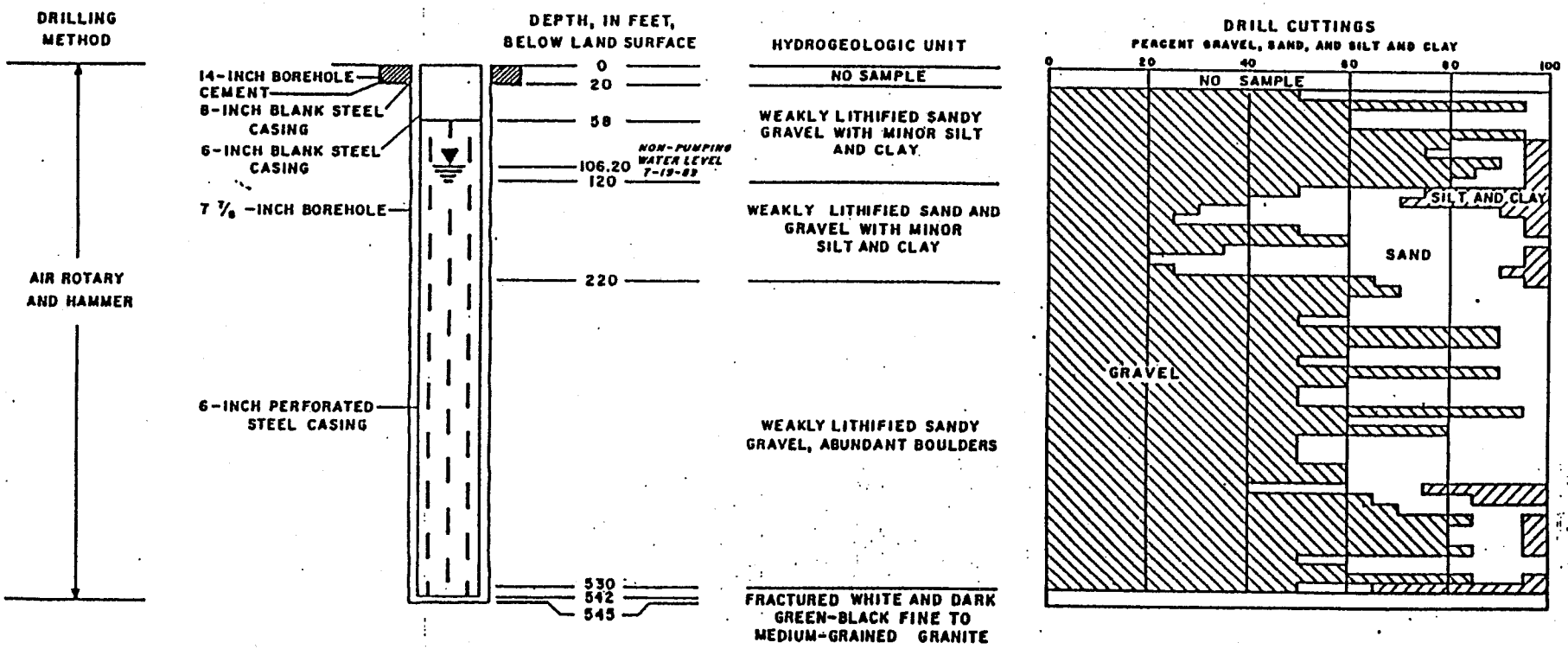
Source: Halpenny and Halpenny (1989)



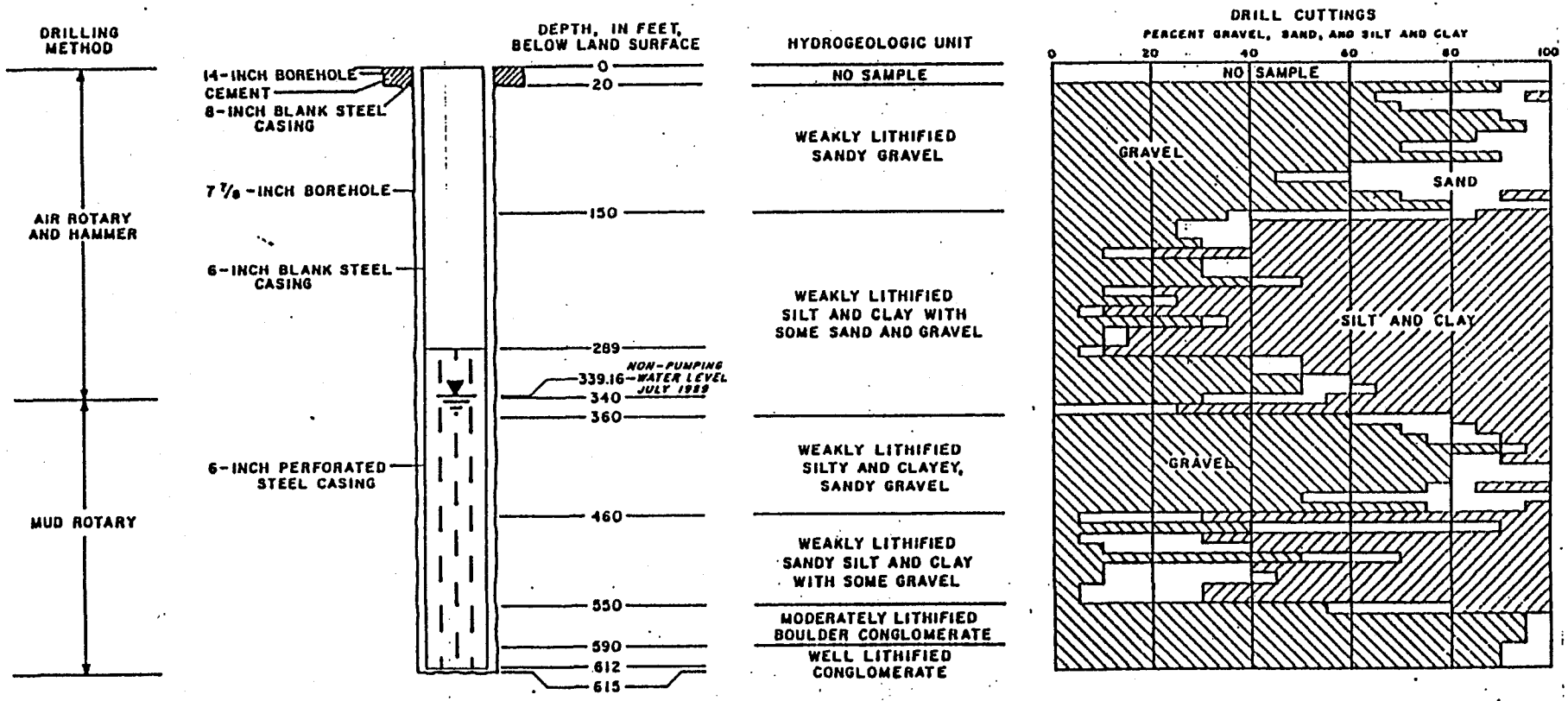
SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (B-3-6)35aaa [No. 1]



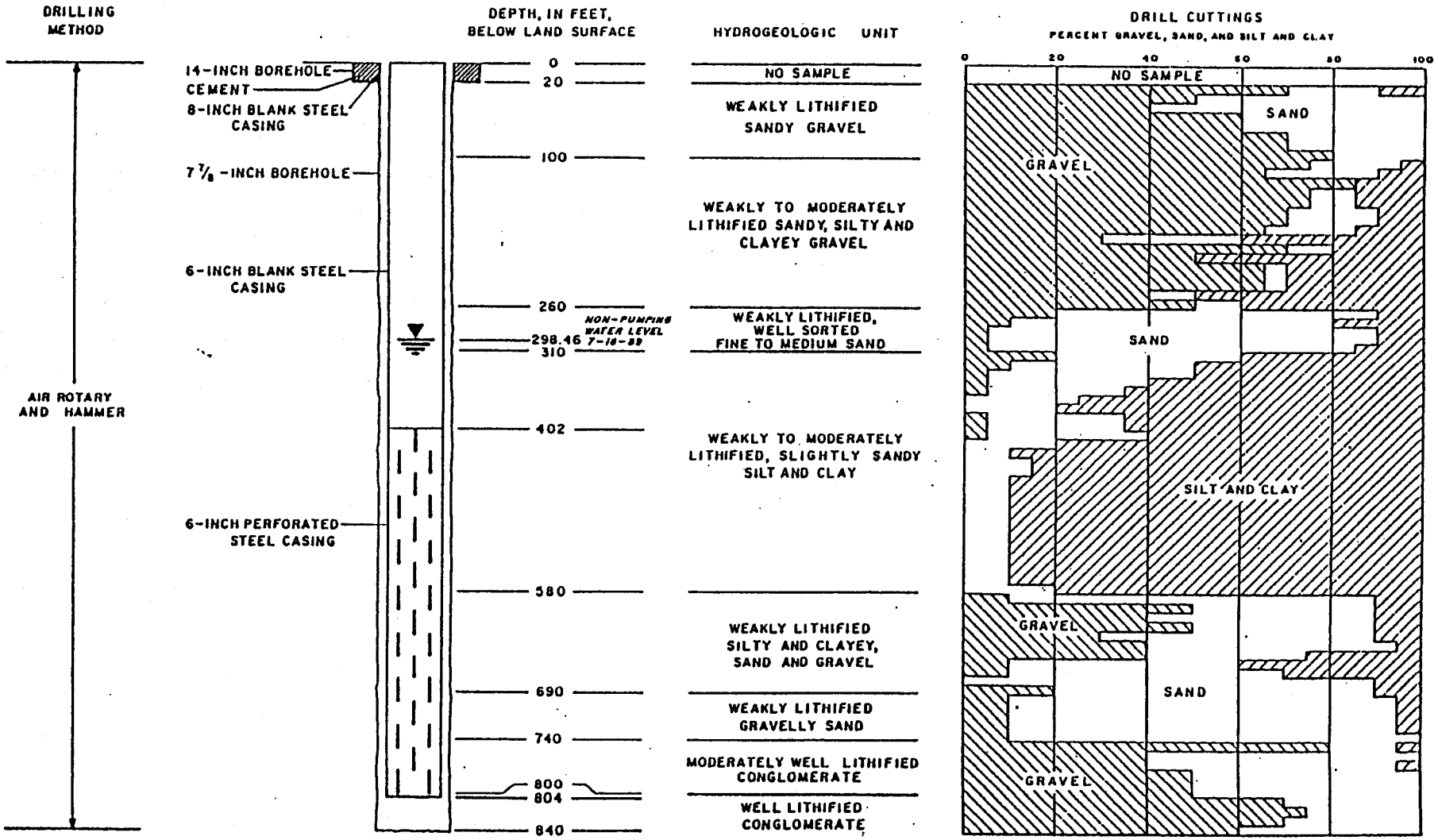
SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (8-2-5)6ddd [No. 2]



SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (8-2-5)3ddd [No. 3]



SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (B-2-6)11bbb [No. 4]



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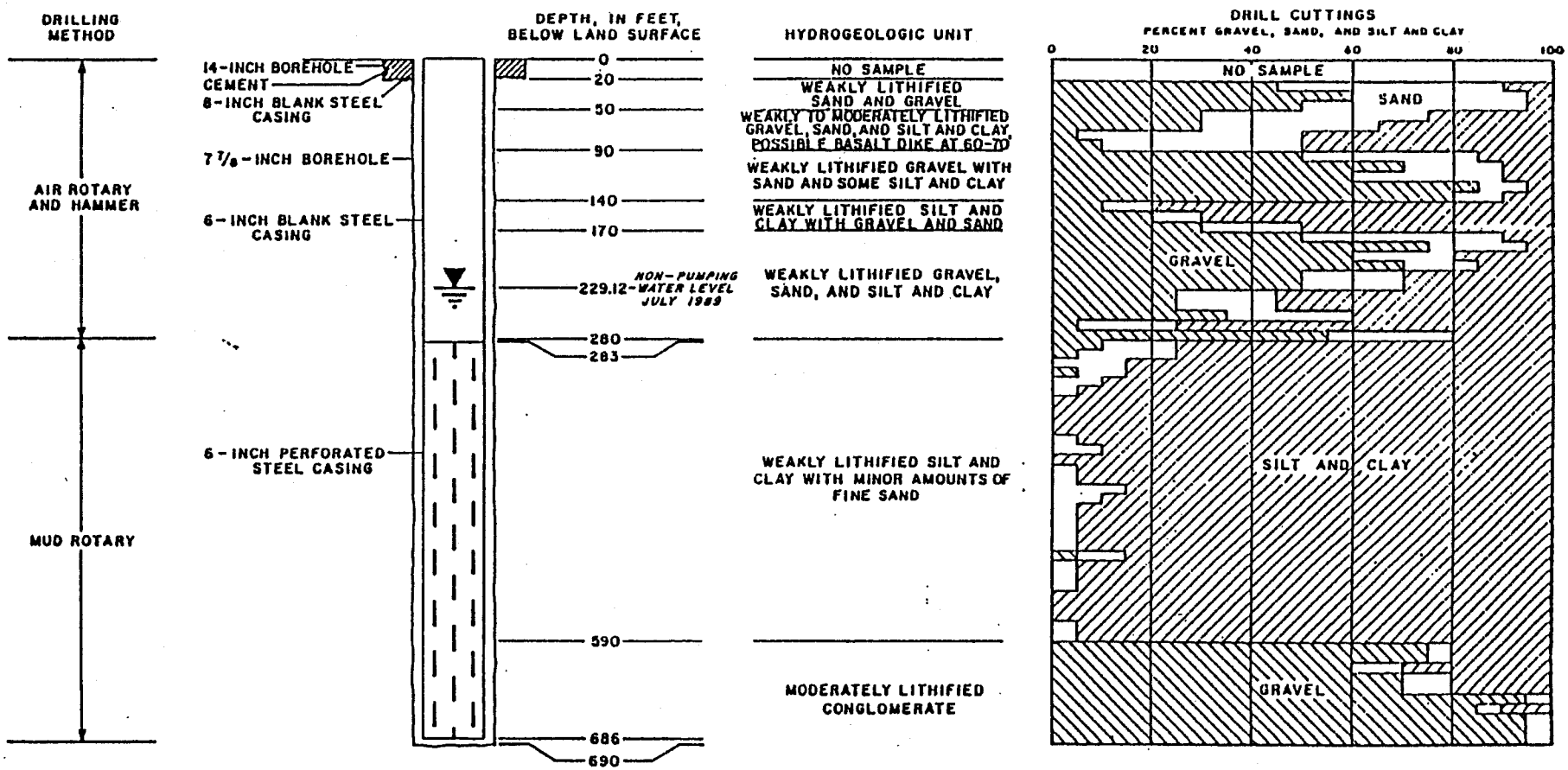
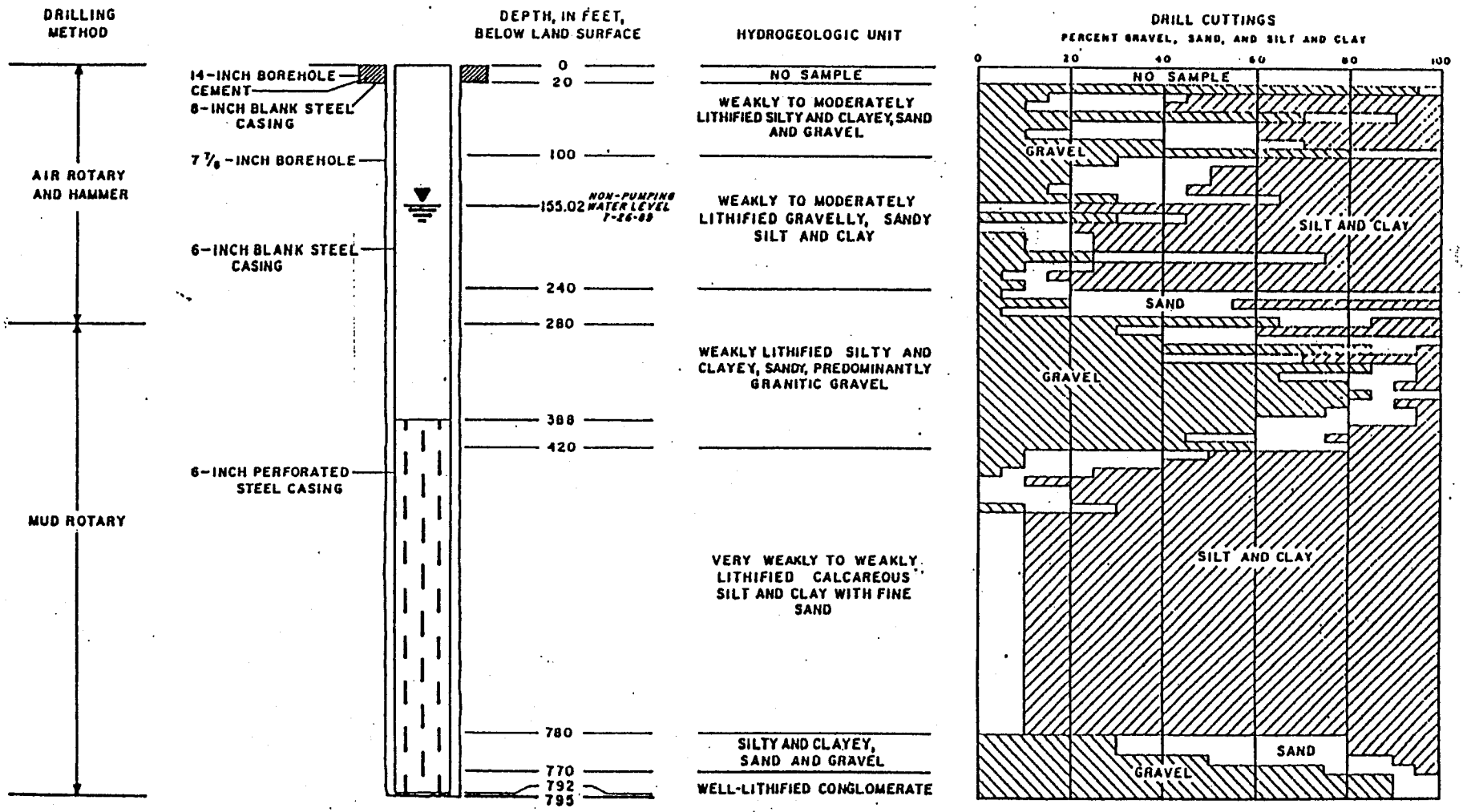


SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (8-2-6)12ddd [No. 6]



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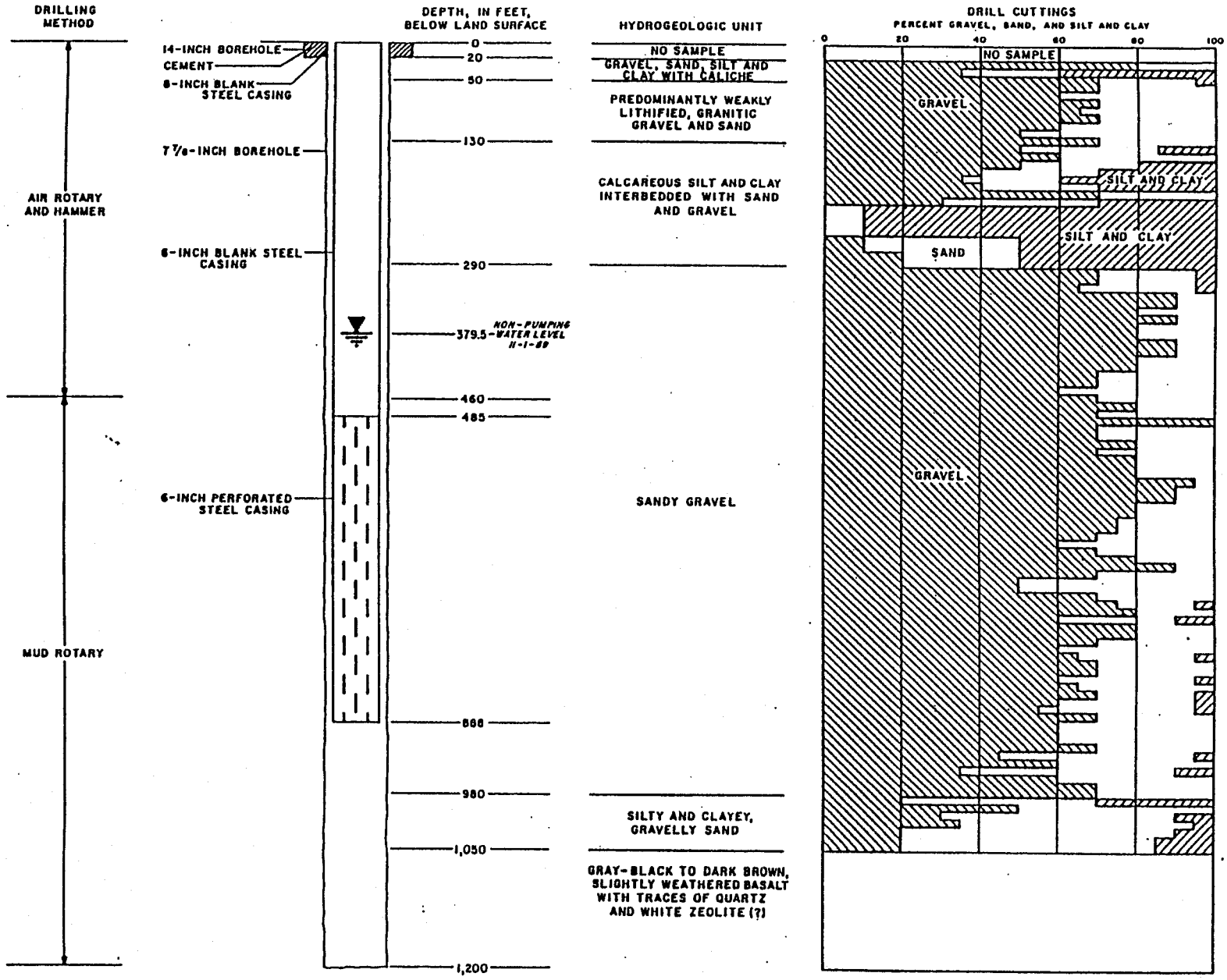

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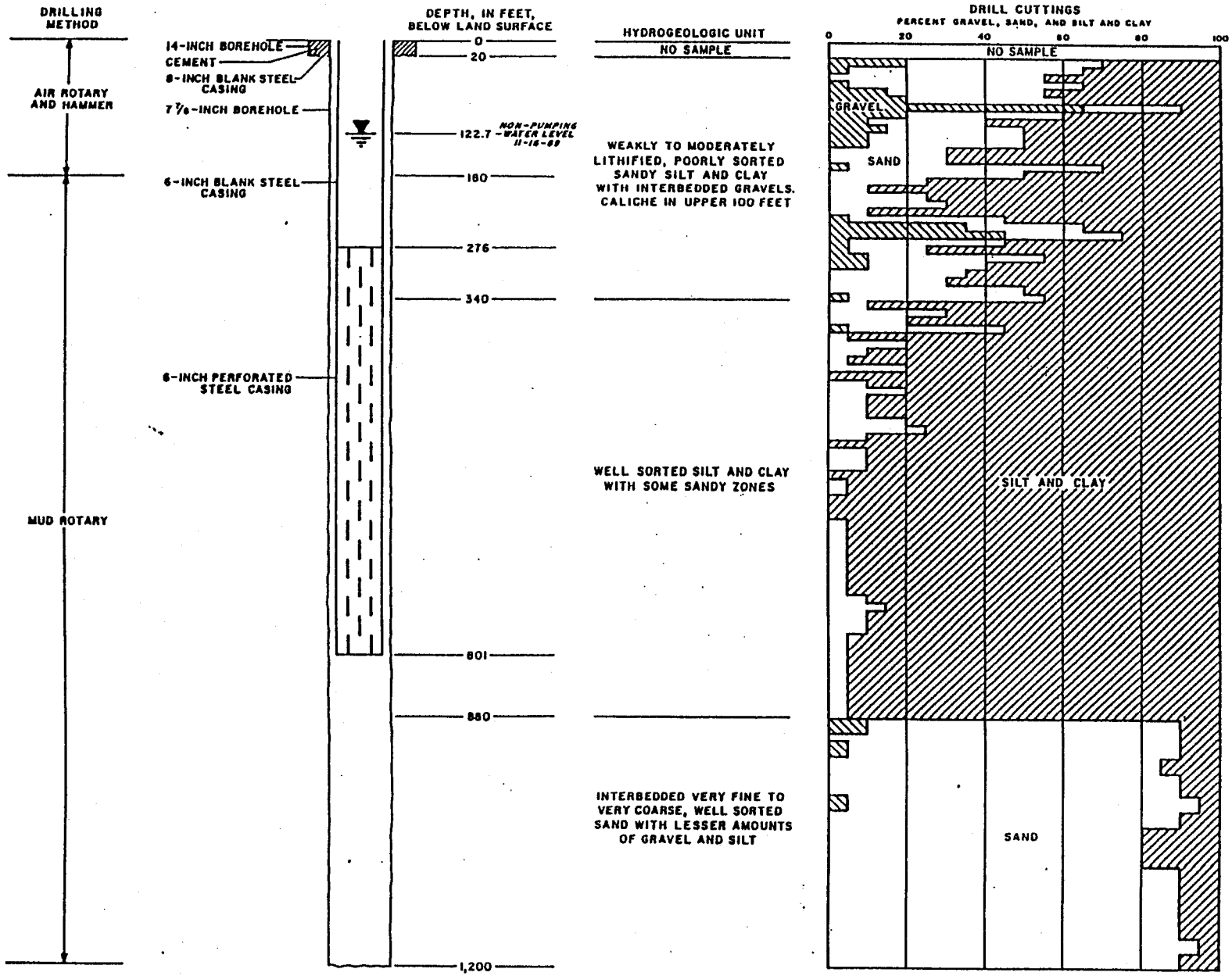

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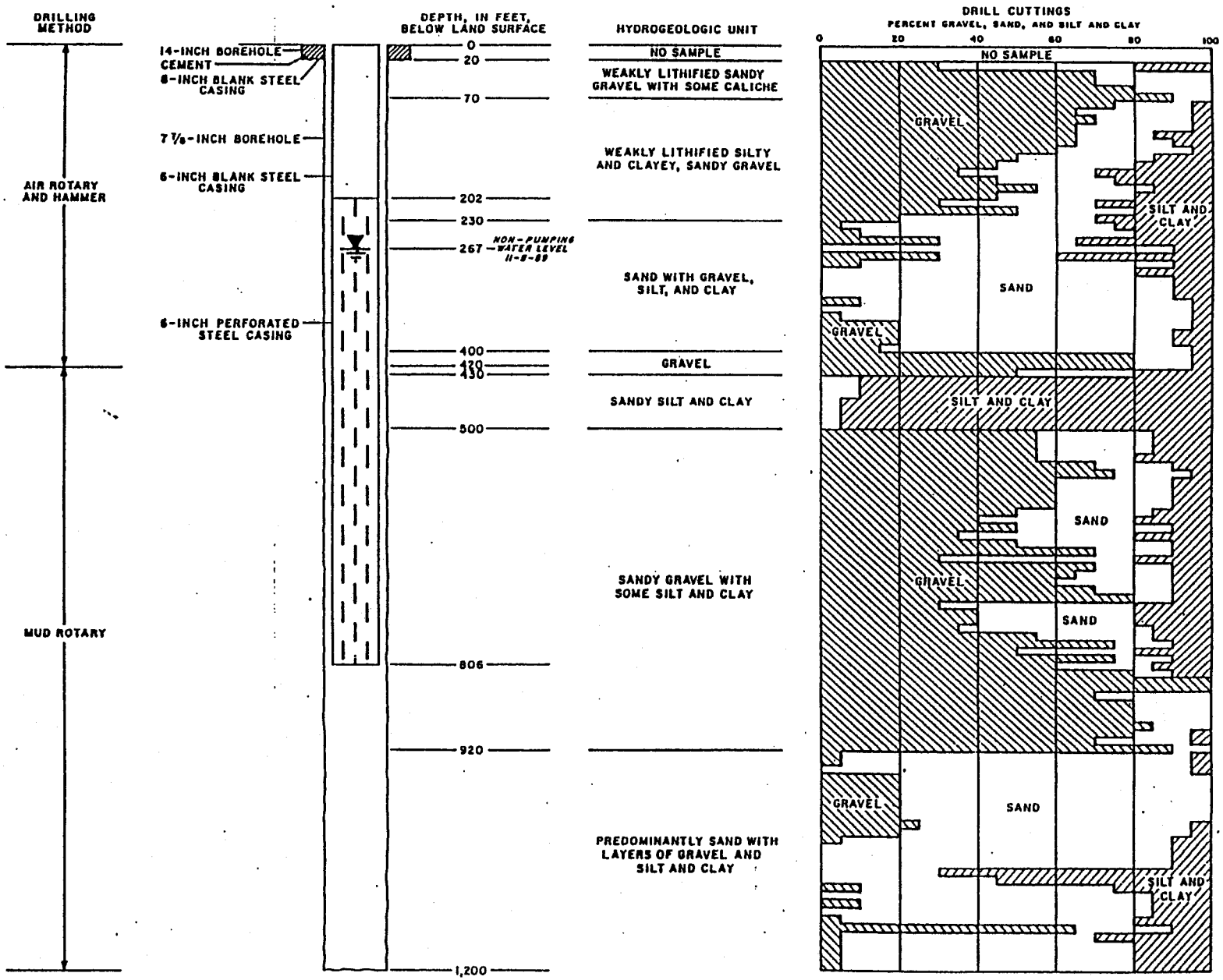


SCHEMATIC DIAGRAM OF WELL CONSTRUCTION AND PERCENT GRAVEL, SAND, AND SILT AND CLAY FOR TEST EXPLORATION HOLE (B-2-6)16dcc [No. 10]

ERROL L. MONTGOMERY & ASSOCIATES, INC.
CONSULTANTS IN HYDROGEOLOGY
1075 EAST FORT LOWELL ROAD, SUITE B
TUCSON, ARIZONA 85719 (602) 881-4912
TELEX: 165597 MONTE TUC
FAX: (602) 881-1609

ERROL L. MONTGOMERY, P.G.
JOHN W. HARSHBARGER, P.G., P.E.
DONALD K. GREENE, P.E.
WILLIAM R. VICTOR, P.G.
EDWARD W. PEACOCK, P.G.
RONALD H. DEWITT, P.G.
MARK M. CROSS, P.G.
DENNIS G. HALL, P.G.

December 15, 1989

Mr. Leonard Halpenny
WATER DEVELOPMENT CORPORATION
3938 East Santa Barbara
Tucson, Arizona 85711

RE: GEOLOGIC FINDINGS FOR THE BELMONT PROJECT

Dear Leonard:

In accordance with your request, we have prepared a summary of the geologic condition for the Belmont Project study area. The summary is based on information obtained from inspection of the drill cuttings samples for 10 test exploration holes drilled during the period May to November 1989, and review of Arizona Bureau of Geology and Mineral Technology Open-File Report 85-14 entitled Preliminary Geologic Maps of the Eastern Big Horn Mountains and Belmont Mountains, West-Central Arizona (Capps and others, 1985).

Figure 1 is a hydrogeologic map of the study area showing locations of the 10 test exploration wells and locations of three hydrogeologic sections. Figures 2, 3, and 4 are north-south, northwest-southeast, and west-east hydrogeologic sections through the study area. The Belmont Project study area bounded on the north by the Belmont Mountains, on the east by the Hassayampa River, bounded to the south by Van Buren Road, and bounded on the west by Winters Wash. Nine of the 10 test exploration holes were drilled in an alluvial valley that slopes gently south from the Belmont Mountains, west from a ridge of Late Proterozoic granite, northeast from the Palo Verde Hills, and east from the Big Horn Mountains. Test exploration hole #3 was drilled in an adjacent alluvial basin located on the east side of the Late Proterozoic granitic ridge.

The geology of the study area is typical of alluvial basins in the Basin and Range Province of Arizona. For this report, the alluvial basin deposits have been informally divided into three units: basin-fill deposits comprising poorly sorted gravel, sand, silt, and clay; fine-grained lacustrine deposits; lower coarse-grained conglomerate. Late Proterozoic granite and Tertiary basalts comprise the bedrock complex penetrated by test exploration holes #1, #2, #3, and #8.

Test exploration hole #1 is located less than 2,000 feet south from a basaltic flow of Tertiary Hot Rock Basalt (Figures 1 and 2). Hole #1 penetrated basalt at a depth of 410 feet below land surface. Because basaltic gravel overlies basalt in hole #1, and Hot Rock Basalt crops out a short distance from hole #1, it is believed that the basalt encountered at hole #1 is a different basaltic flow, or a down-faulted section of Hot Rock Basalt. Test exploration hole #8 penetrated basalt of an unknown age at a depth of 1,050 feet below land surface (Figure 3). The basalt is moderately weathered and fractured and is believed to have been aerially

exposed prior to deposition of the alluvial sediments. The basalts encountered in holes #1 and #8 are not necessarily stratigraphically continuous.

Test exploration holes #2, and #3 penetrated granite at depths of 710 and 530 feet below land surface. The granite encountered in hole #3 is fine- to medium-grained, equigranular, and biotite-rich, and is similar in lithology to the samples of Late Proterozoic granite from outcrop in section 9, Township 2 North, Range 5 West, and described by Capps and others (1985). The granite encountered in hole #2 is medium-grained and equigranular with only a trace of biotite, and similar in description to the Tertiary Belmont Granite. However, because of the proximity of holes #2 and #3 to outcrops of Late Proterozoic granite, they are believed to be completed in Late Proterozoic granite.

Test exploration holes #4, #5, #6 and #7 are completed in a moderately well-lithified coarse-grained conglomerate composed chiefly of granite and feldspar porphyry (Figures 2, 3, and 4). A coarse-grained conglomerate also overlies bedrock complex in holes #1 and #2. Coarse-grained conglomerate was not encountered in holes #9A, #10. The holes are located closer to the center of the basin, and may not have been drilled deep enough to penetrate the coarse-grained conglomerate.

Stratigraphically overlying the coarse-grained conglomerate are fine-grained lacustrine deposits and basin-fill deposits. Well sorted, moderate brown silts and clays comprise the lacustrine deposits and occur in test exploration holes #5, #6, #7, #9A and #10. The thickness of the lacustrine deposits encountered in the test exploration holes ranges from about 70 feet in hole #10 to more than 500 feet in hole #9A (Figures 4 and 2). The unit apparently thickens to the south and southwest towards the center of the basin.

The basin-fill deposits overlie the fine-grained lacustrine or the coarse-grained conglomerate deposits. The provenance of the basin-fill deposits is believed to be the Belmont Mountains, although other source areas are likely, including the Big Horn Mountains and the Palo Verde Hills. The dominant rock types in the test exploration wells are also the dominant rock types in the Belmont Mountains and comprise Late Proterozoic granite, amphibolite, and schist, Tertiary Belmont Granite, and various Tertiary volcanic flows and intrusive igneous rocks.

If you have questions or require further discussion, please contact us.

Very truly yours,

ERROL L. MONTGOMERY AND ASSOCIATES, INC.

Michael J. Rosko

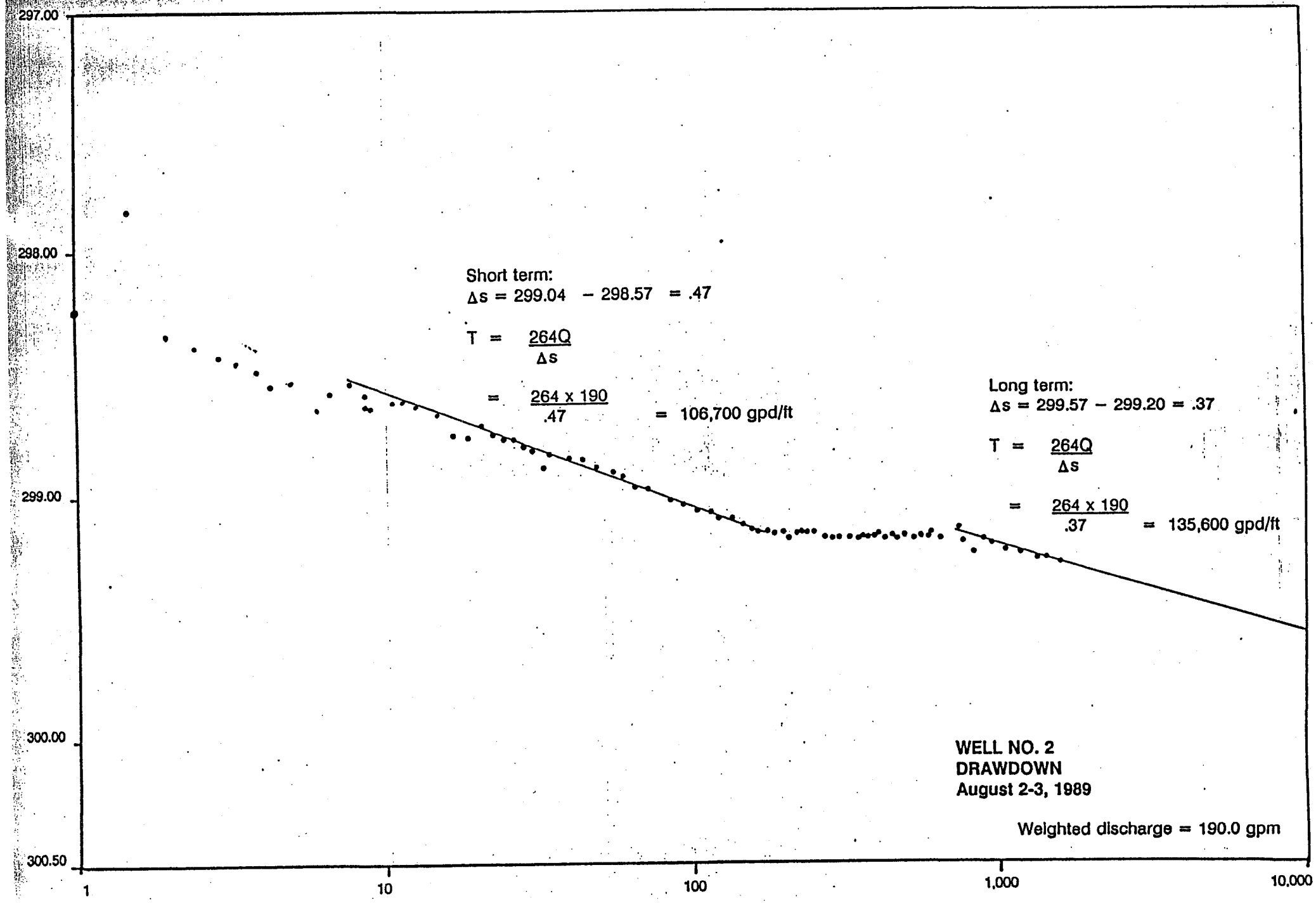
Michael J. Rosko

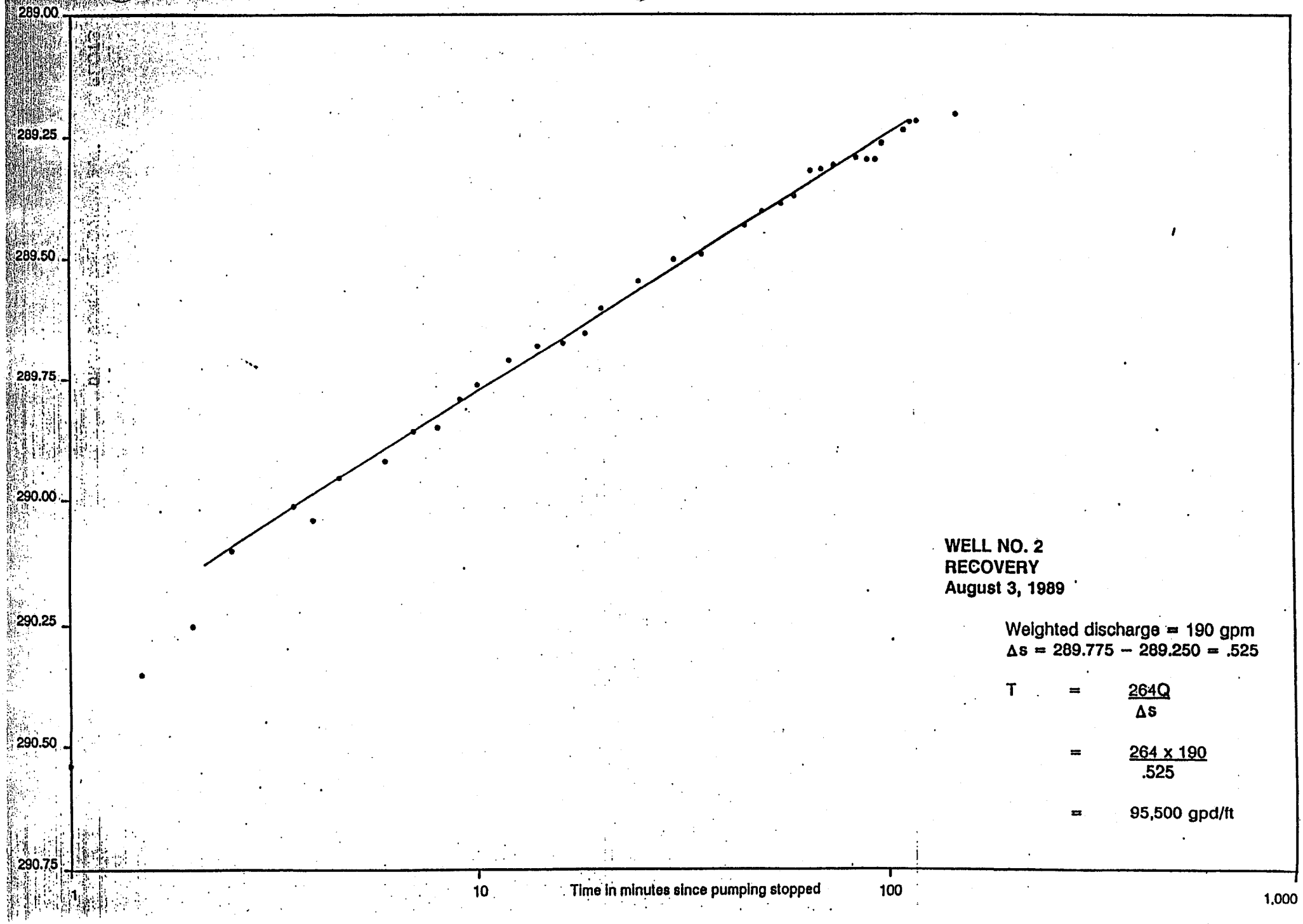
Enclosures

REFERENCES CITED

Capps, R. C., S. J. Reynolds, C. P. Kortemeier, J. A. Stimac, E. A. Scott, and G. B. Allen, 1985. Preliminary geologic maps of the Eastern Big Horn and Belmont Mountains, West-Central Arizona. Arizona Bureau of Geology and Mineral Technology: Open-File Report 85-14.

Wilson, E. D., R. T. Moore, and H. W. Pierce, 1957. Geologic map of Maricopa County, Arizona. Arizona Bureau of Mines, University of Arizona, Tucson, Arizona.

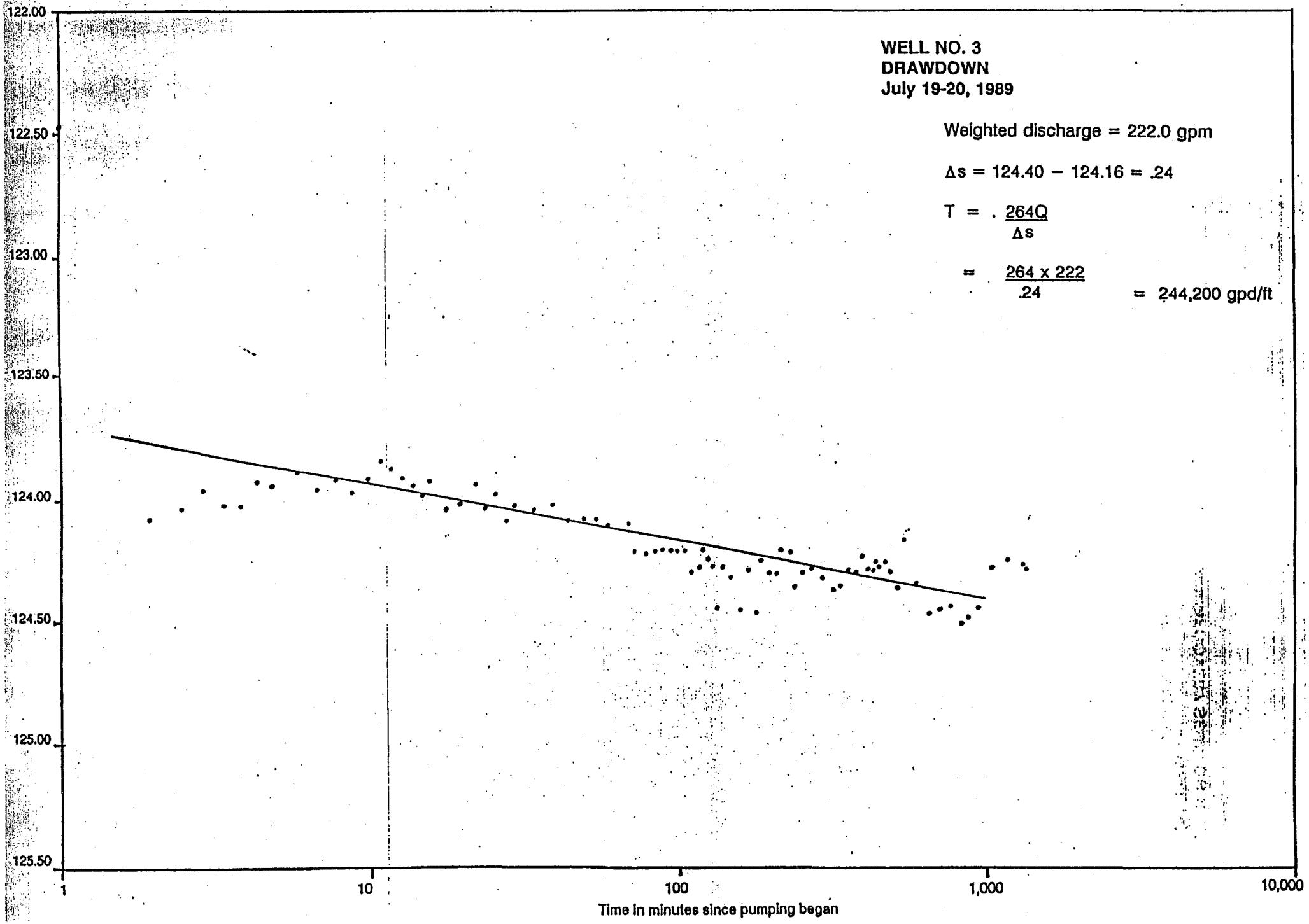

297.00
298.00
299.00
300.00
300.50
1
10
100
1,000
10,000
Short term:
Δs = 299.04 − 298.57 = .47
T = 264Q / Δs
= 264 x 190 / .47 = 106,700 gpd/ft
Long term:
Δs = 299.57 − 299.20 = .37
T = 264Q / Δs
= 264 x 190 / .37 = 135,600 gpd/ft
WELL NO. 2
DRAWDOWN
August 2-3, 1989
Weighted discharge = 190.0 gpm

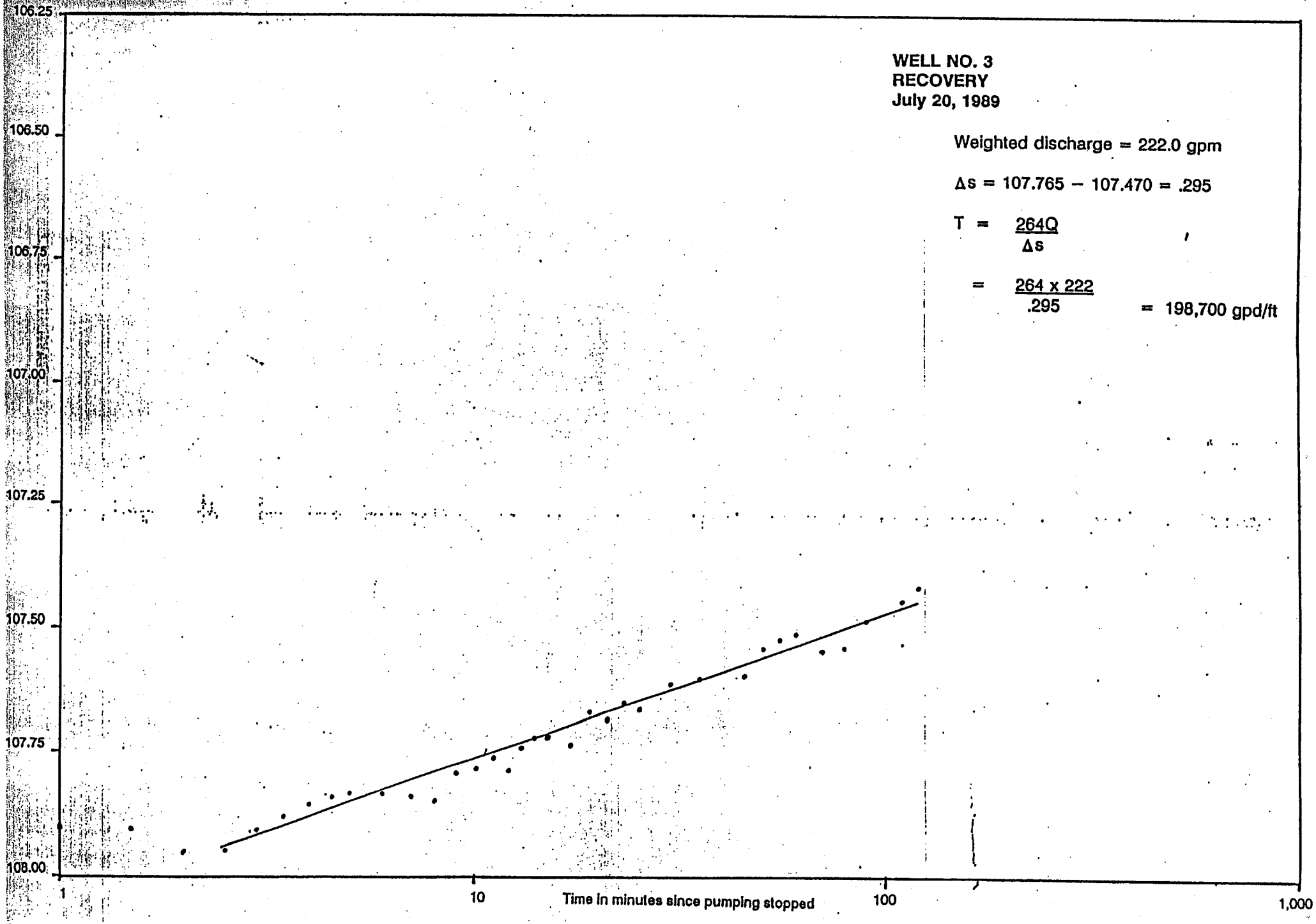


WELL NO. 2
RECOVERY
August 3, 1989

Weighted discharge = 190 gpm
$\Delta s = 289.775 - 289.250 = .525$

$$T = \frac{264Q}{\Delta s} = \frac{264 \times 190}{.525} = 95{,}500 \text{ gpd/ft}$$


WELL NO. 3
DRAWDOWN
July 19-20, 1989
Weighted discharge = 222.0 gpm
Δs = 124.40 − 124.16 = .24
T = . 264Q / Δs
= 264 x 222 / .24 = 244,200 gpd/ft
122.00
122.50
123.00
123.50
124.00
124.50
125.00
125.50
1
10
100
1,000
10,000
Time in minutes since pumping began



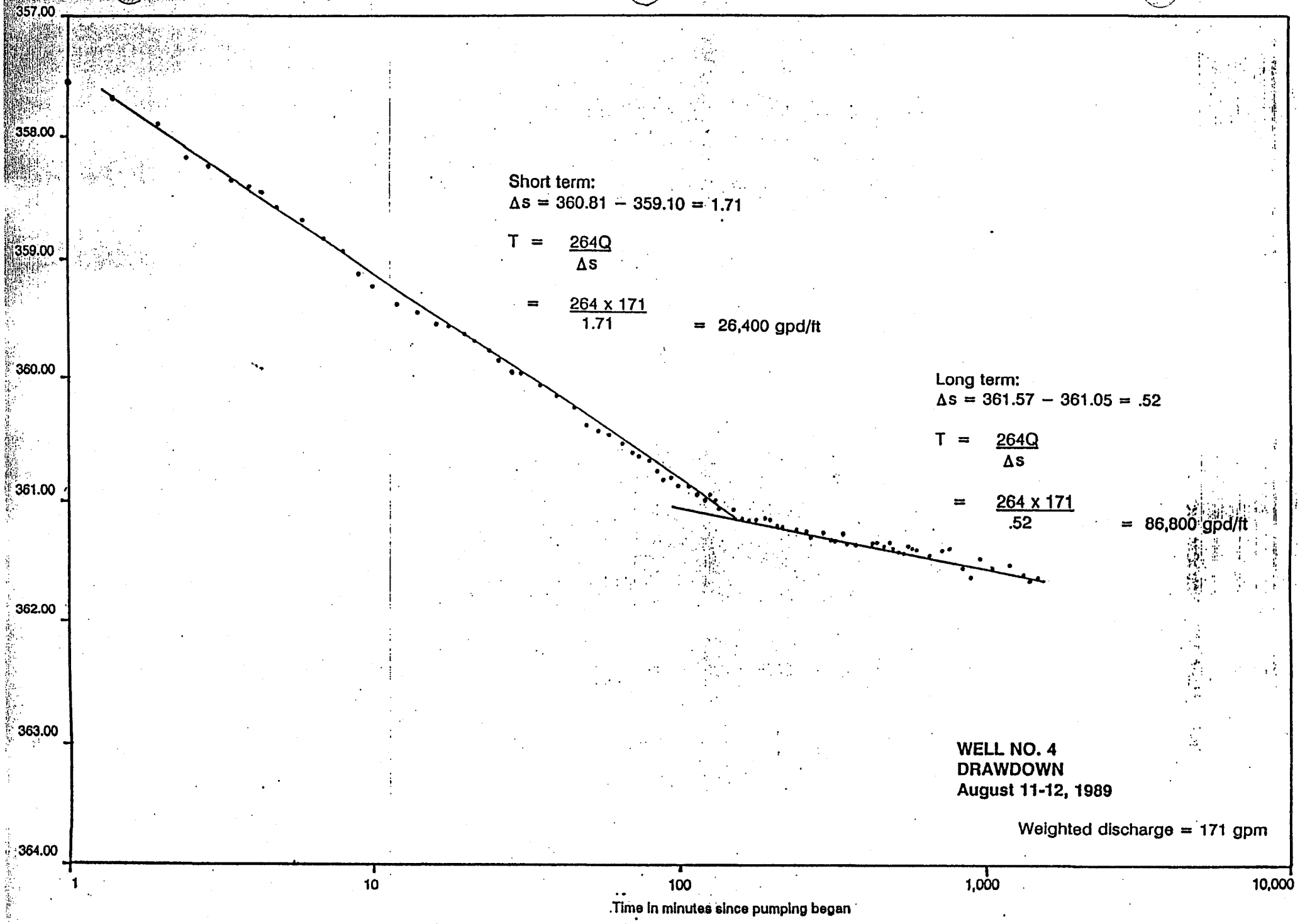
WELL NO. 3
RECOVERY
July 20, 1989

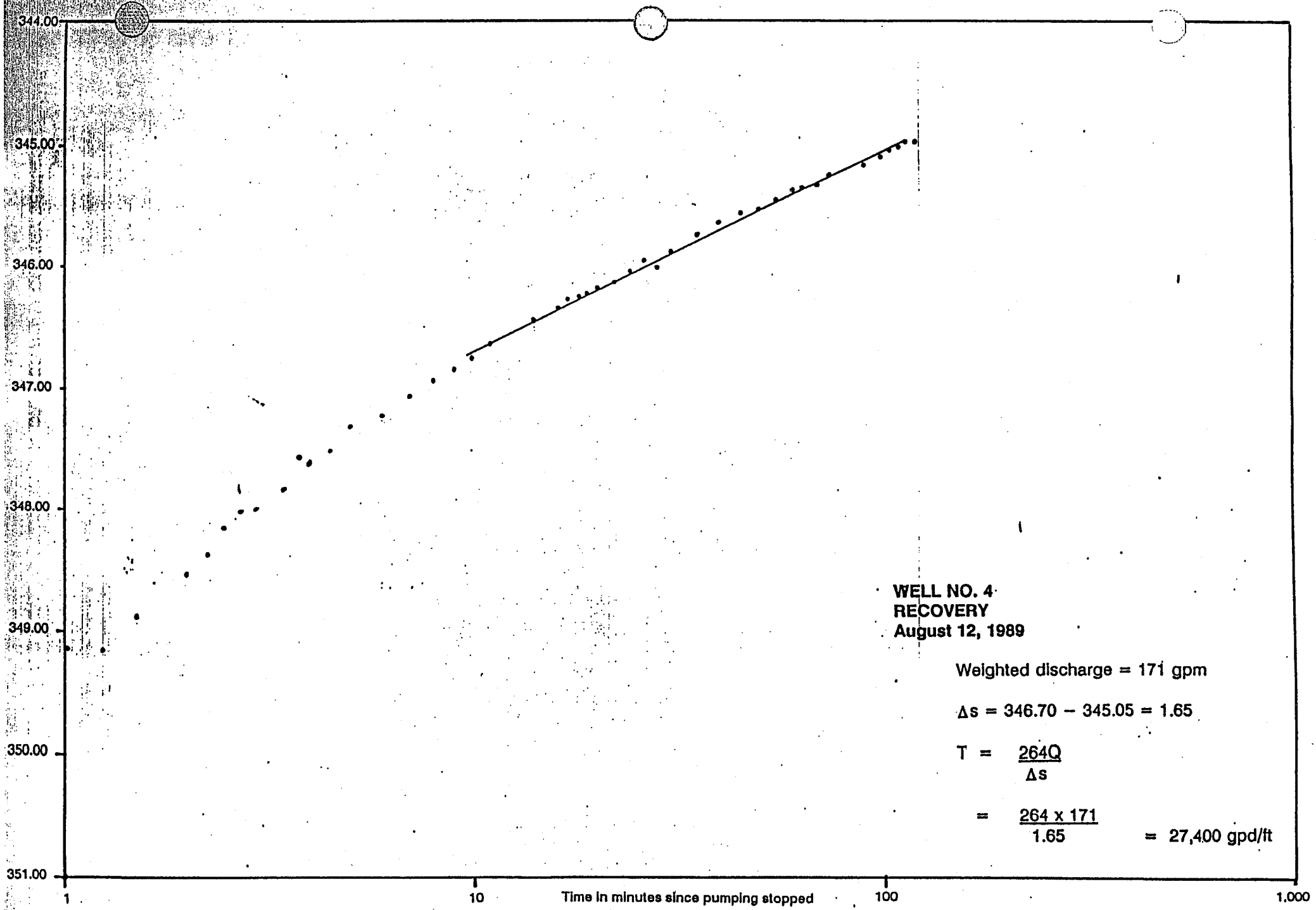
Weighted discharge = 222.0 gpm

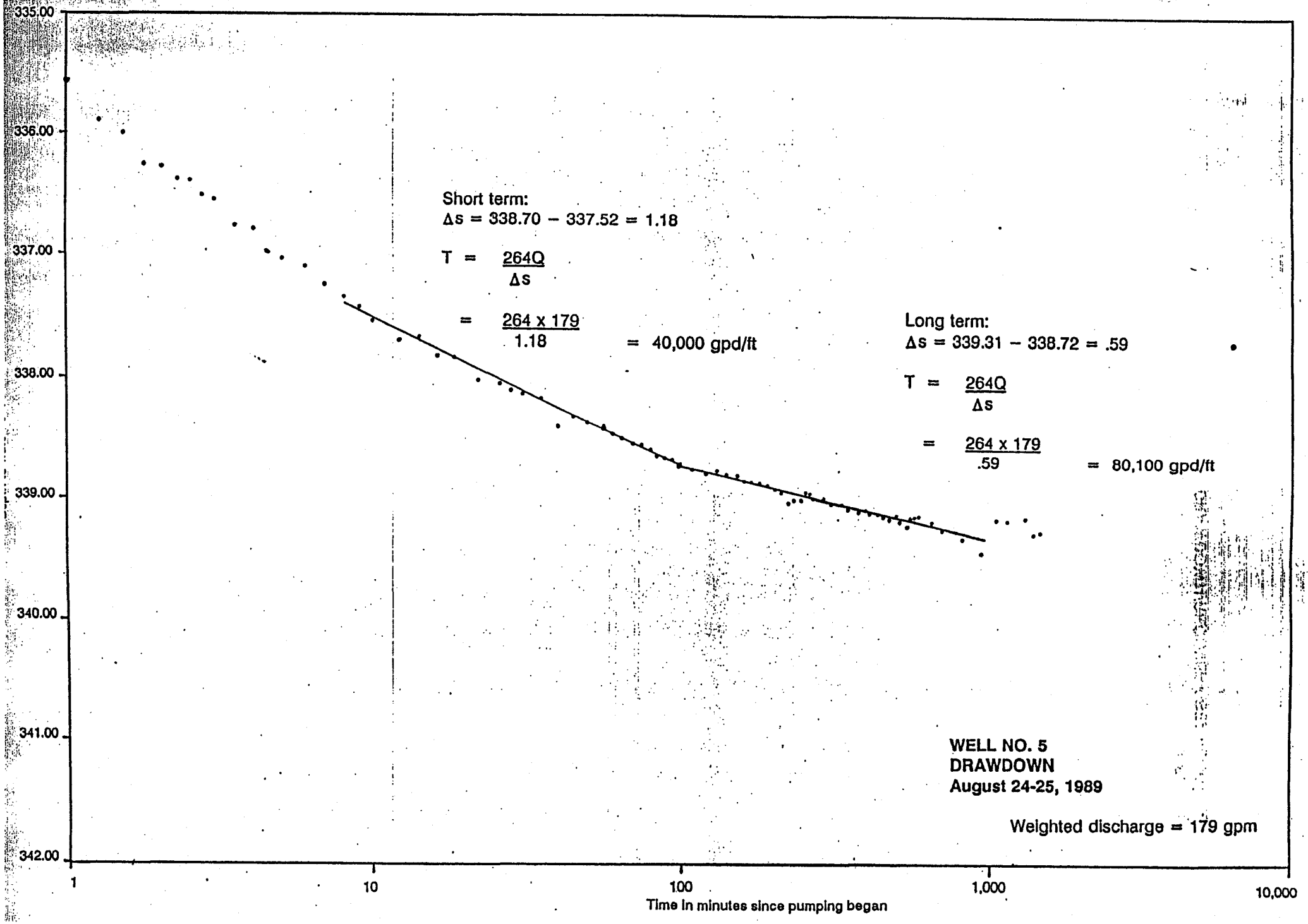
$\Delta s = 107.765 - 107.470 = .295$

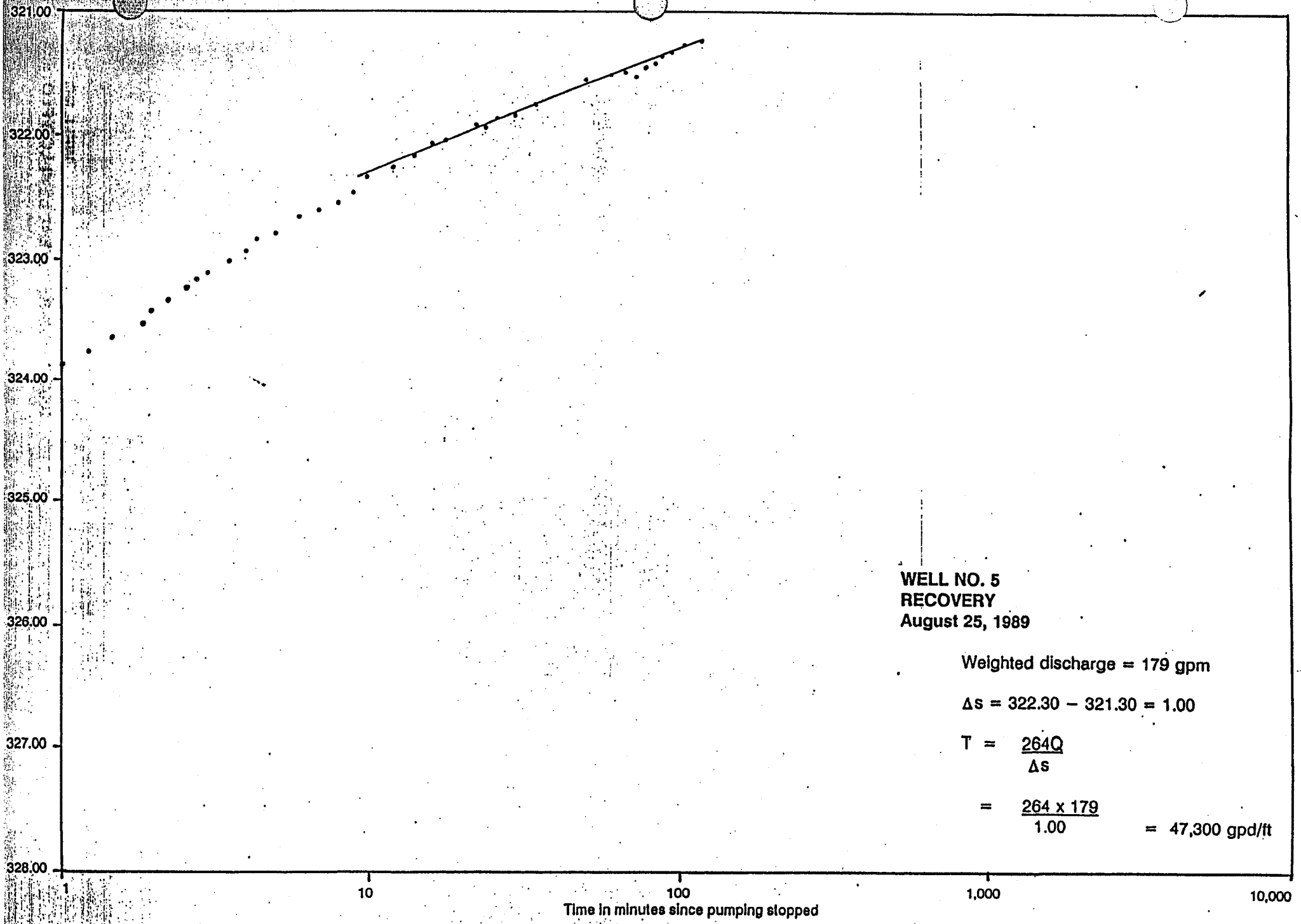
$$T = \frac{264Q}{\Delta s}$$

$$= \frac{264 \times 222}{.295} = 198{,}700 \text{ gpd/ft}$$


357.00
358.00
359.00
360.00
361.00
362.00
363.00
364.00
1
10
100
1,000
10,000
Time in minutes since pumping began
Short term:
Δs = 360.81 − 359.10 = 1.71
T = 264Q / Δs
= 264 x 171 / 1.71 = 26,400 gpd/ft
Long term:
Δs = 361.57 − 361.05 = .52
T = 264Q / Δs
= 264 x 171 / .52 = 86,800 gpd/ft
WELL NO. 4
DRAWDOWN
August 11-12, 1989
Weighted discharge = 171 gpm


344.00
345.00
346.00
347.00
348.00
349.00
350.00
351.00
1
10
100
1,000
Time in minutes since pumping stopped
WELL NO. 4
RECOVERY
August 12, 1989
Weighted discharge = 171 gpm
Δs = 346.70 − 345.05 = 1.65
T = 264Q / Δs
= 264 x 171 / 1.65 = 27,400 gpd/ft


335.00
336.00
337.00
338.00
339.00
340.00
341.00
342.00
1
10
100
1,000
10,000
Time in minutes since pumping began
Short term:
Δs = 338.70 − 337.52 = 1.18
T = 264Q / Δs
= 264 x 179 / 1.18 = 40,000 gpd/ft
Long term:
Δs = 339.31 − 338.72 = .59
T = 264Q / Δs
= 264 x 179 / .59 = 80,100 gpd/ft
WELL NO. 5
DRAWDOWN
August 24-25, 1989
Weighted discharge = 179 gpm



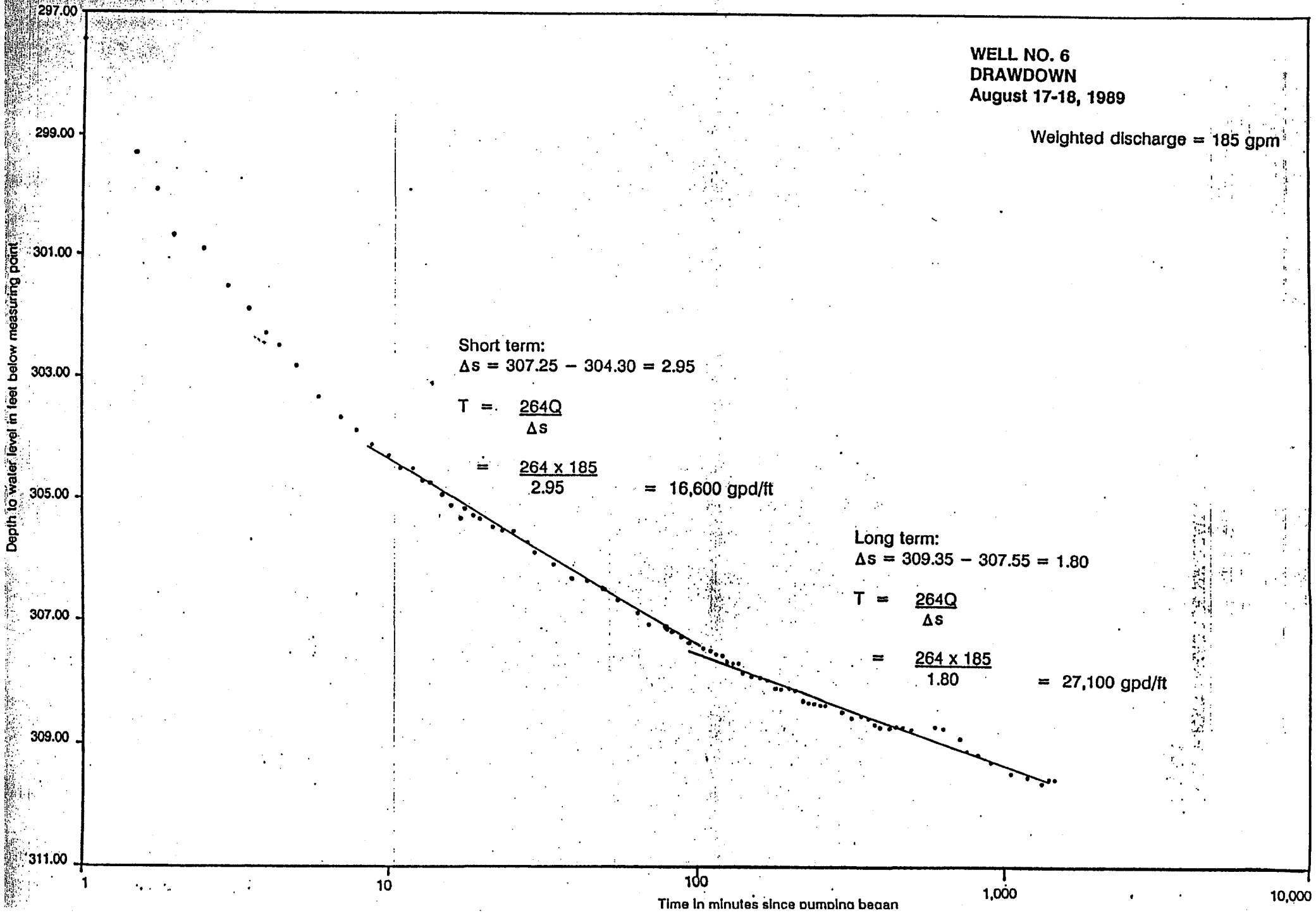
WELL NO. 5
RECOVERY
August 25, 1989

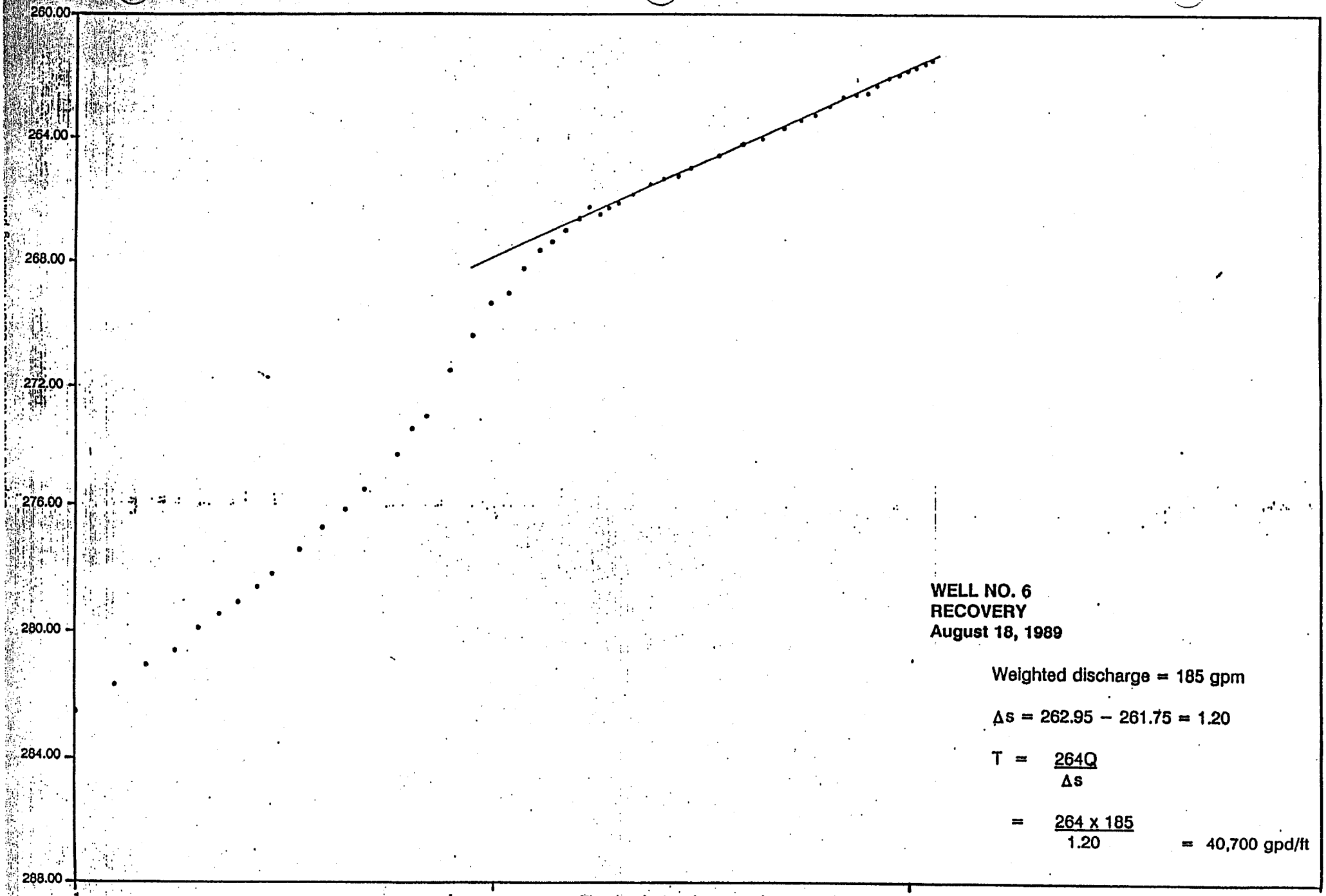
Weighted discharge = 179 gpm

$\Delta s = 322.30 - 321.30 = 1.00$

$$T = \frac{264Q}{\Delta s}$$

$$= \frac{264 \times 179}{1.00} = 47{,}300 \text{ gpd/ft}$$


WELL NO. 6
DRAWDOWN
August 17-18, 1989
Weighted discharge = 185 gpm
Short term:
Δs = 307.25 − 304.30 = 2.95
T = 264Q / Δs
= 264 x 185 / 2.95 = 16,600 gpd/ft
Long term:
Δs = 309.35 − 307.55 = 1.80
T = 264Q / Δs
= 264 x 185 / 1.80 = 27,100 gpd/ft
Depth to water level in feet below measuring point
297.00
299.00
301.00
303.00
305.00
307.00
309.00
311.00
1
10
100
1,000
10,000
Time in minutes since pumping began



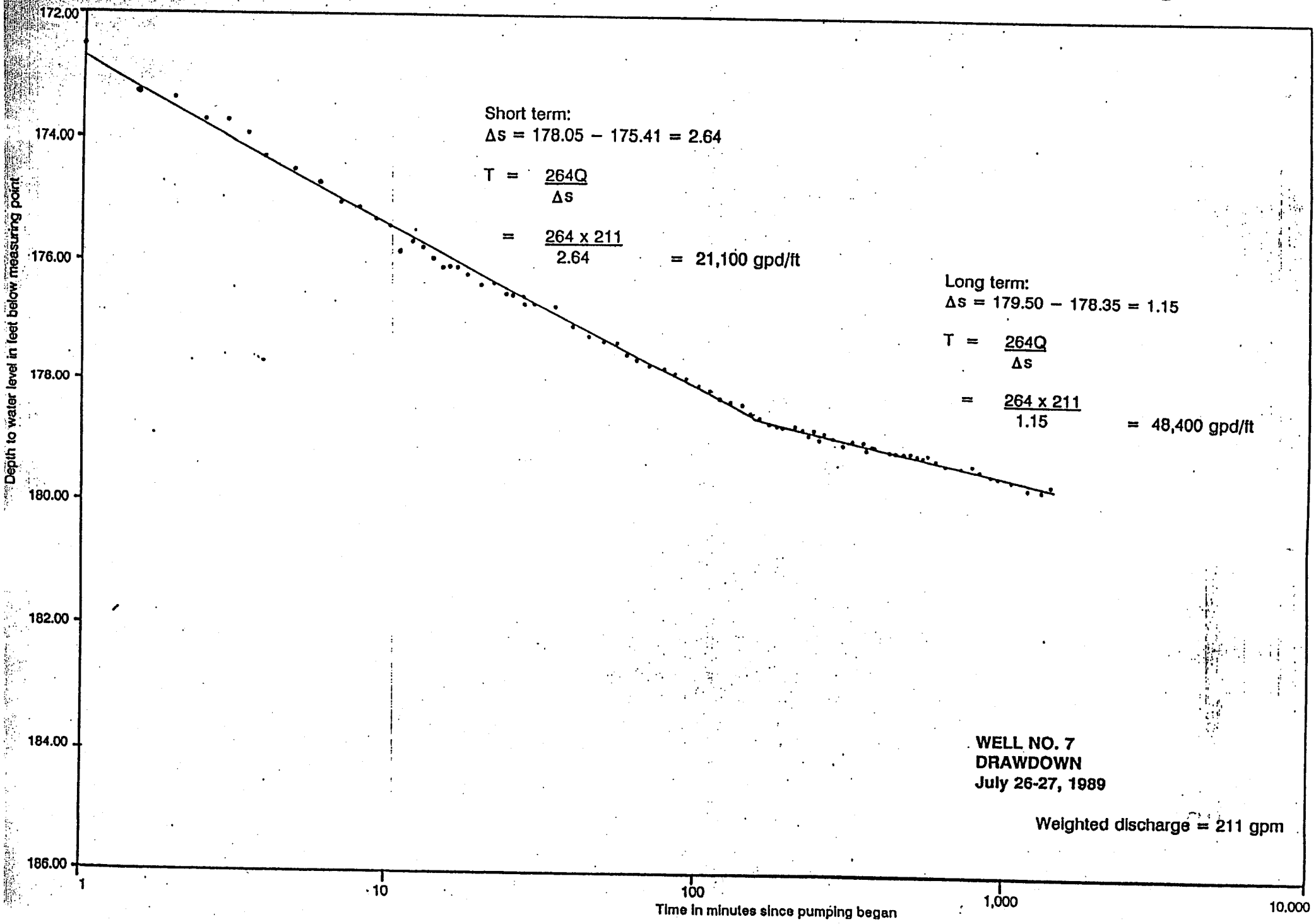
WELL NO. 6
RECOVERY
August 18, 1989

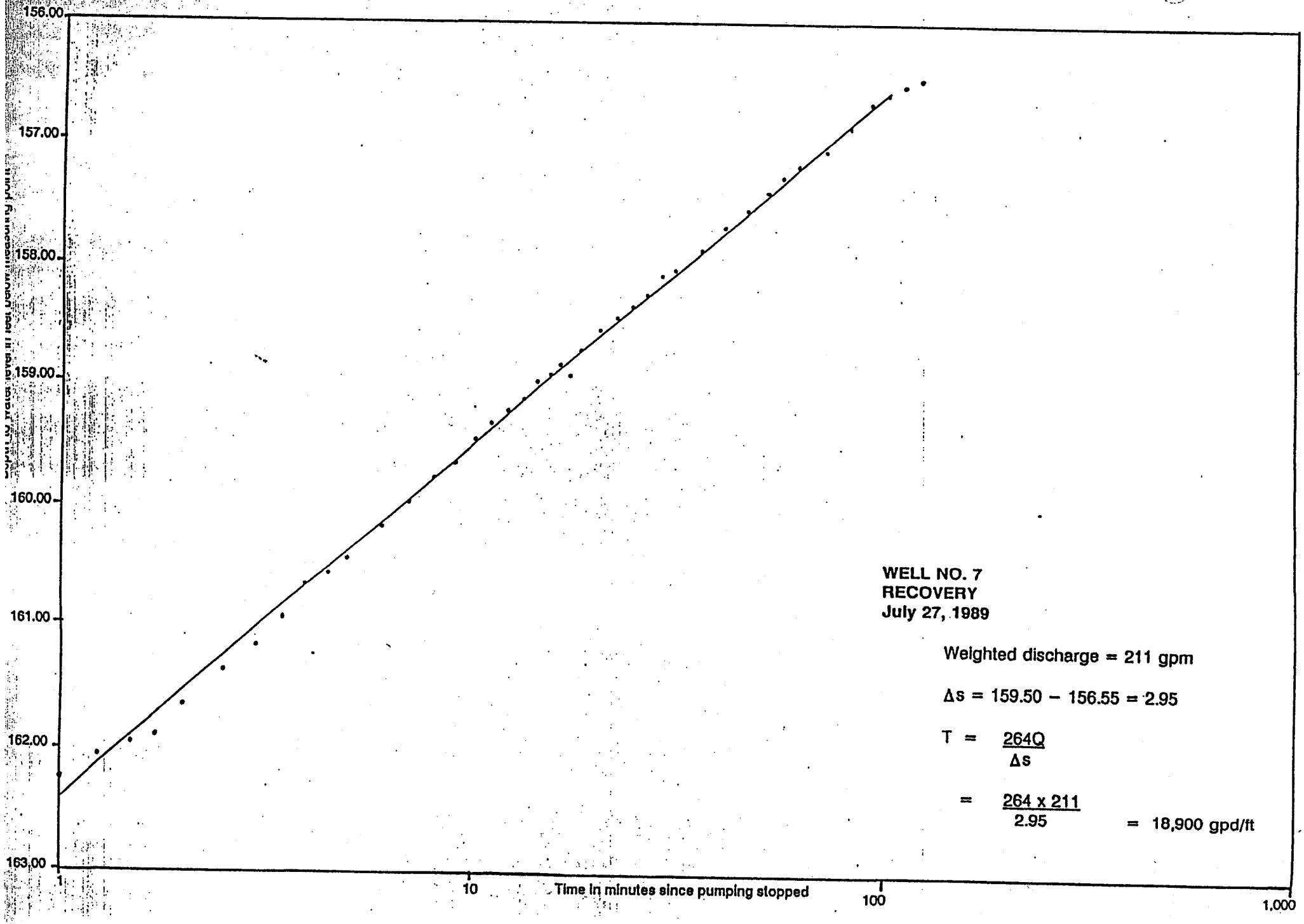
Weighted discharge = 185 gpm

$\Delta s = 262.95 - 261.75 = 1.20$

$$T = \frac{264Q}{\Delta s}$$

$$= \frac{264 \times 185}{1.20} = 40{,}700 \text{ gpd/ft}$$


172.00
174.00
176.00
178.00
180.00
182.00
184.00
186.00
Depth to water level in feet below measuring point
1
10
100
1,000
10,000
Time in minutes since pumping began
Short term:
Δs = 178.05 − 175.41 = 2.64
T = 264Q / Δs
= 264 x 211 / 2.64 = 21,100 gpd/ft
Long term:
Δs = 179.50 − 178.35 = 1.15
T = 264Q / Δs
= 264 x 211 / 1.15 = 48,400 gpd/ft
WELL NO. 7
DRAWDOWN
July 26-27, 1989
Weighted discharge = 211 gpm



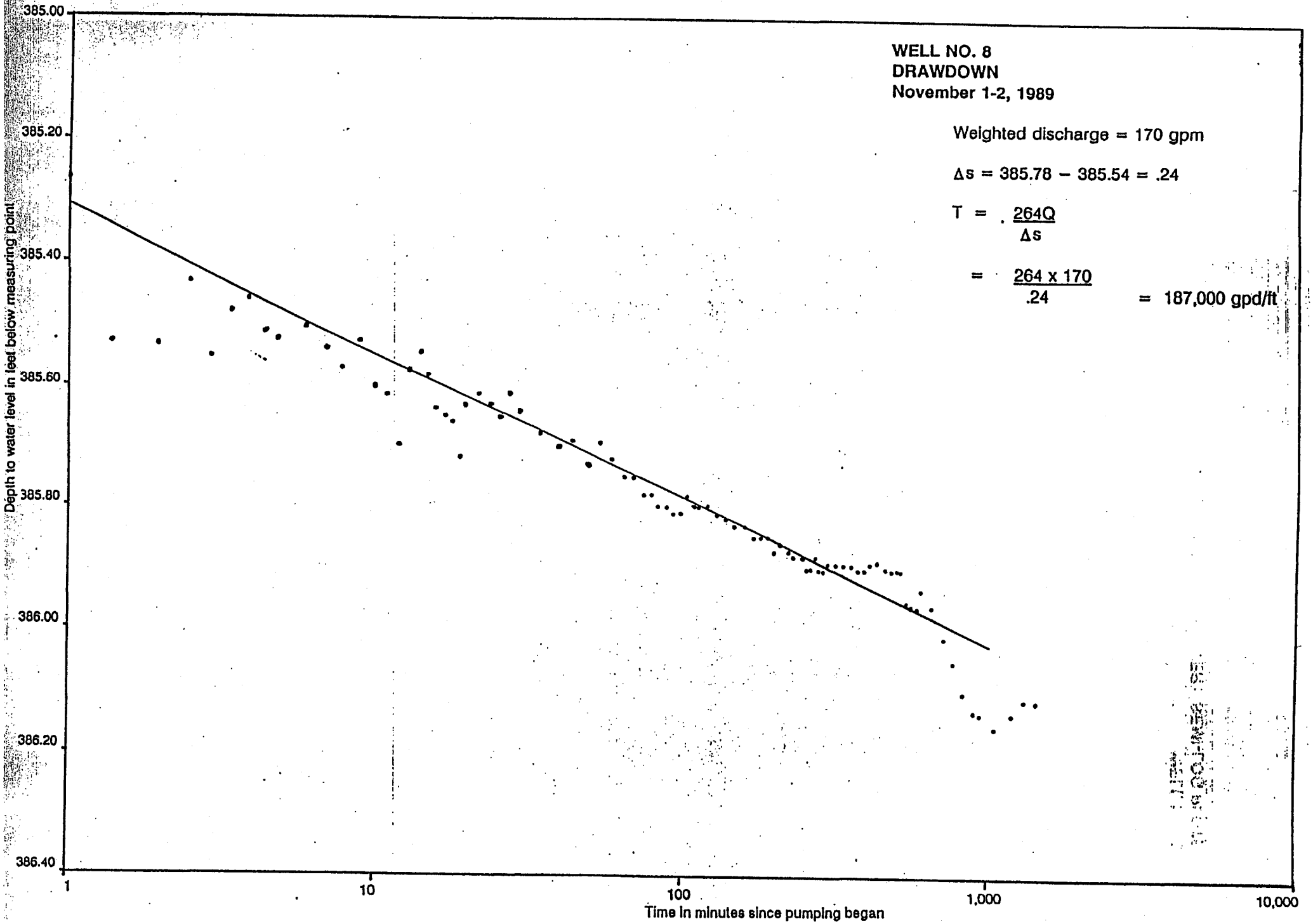
WELL NO. 7
RECOVERY
July 27, 1989

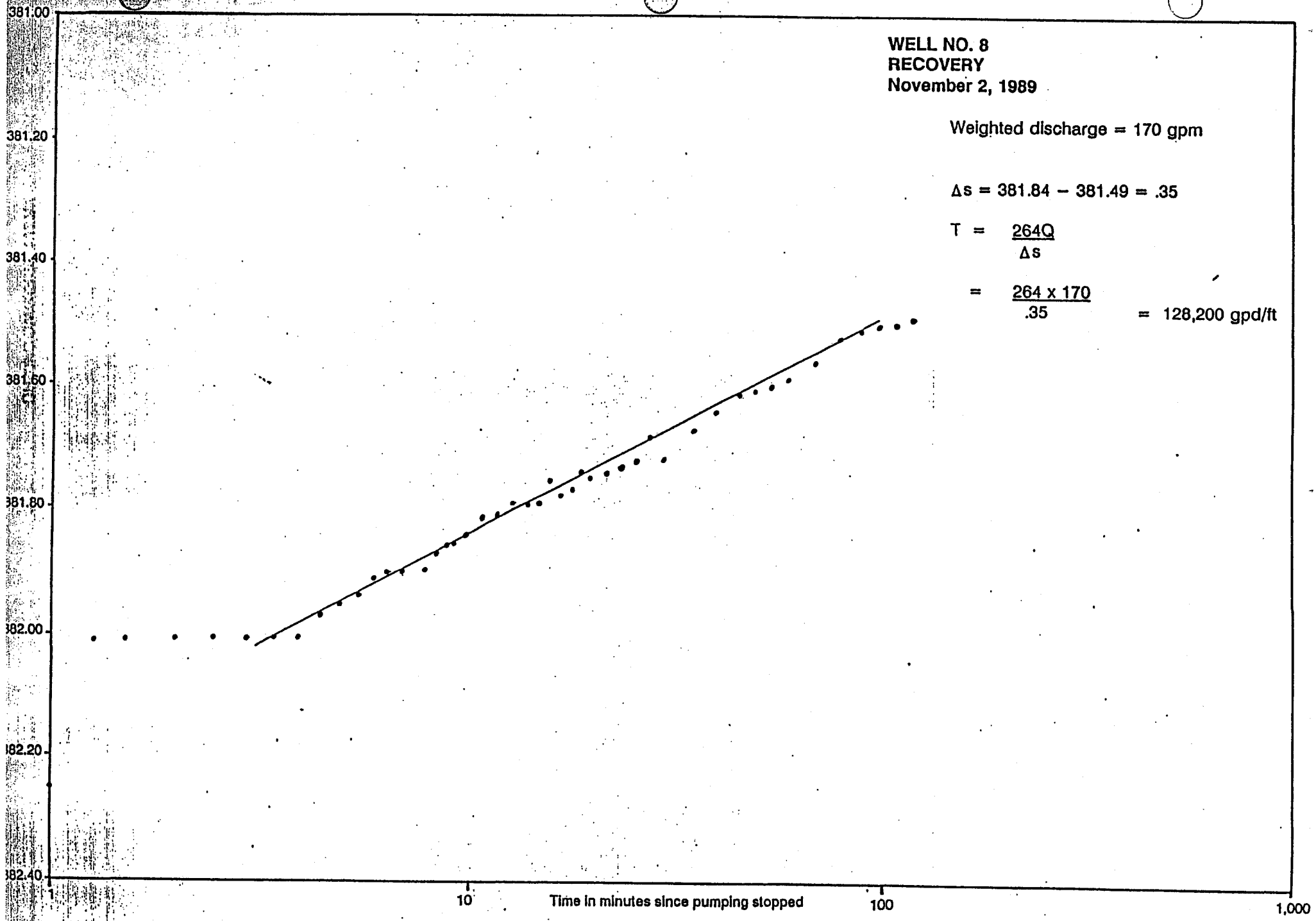
Weighted discharge = 211 gpm

$\Delta s = 159.50 - 156.55 = 2.95$

$$T = \frac{264Q}{\Delta s}$$

$$= \frac{264 \times 211}{2.95} = 18{,}900 \text{ gpd/ft}$$


WELL NO. 8
DRAWDOWN
November 1-2, 1989
Weighted discharge = 170 gpm
Δs = 385.78 − 385.54 = .24
T = 264Q / Δs
= 264 x 170 / .24 = 187,000 gpd/ft
Depth to water level in feet below measuring point
385.00
385.20
385.40
385.60
385.80
386.00
386.20
386.40
1
10
100
1,000
10,000
Time in minutes since pumping began



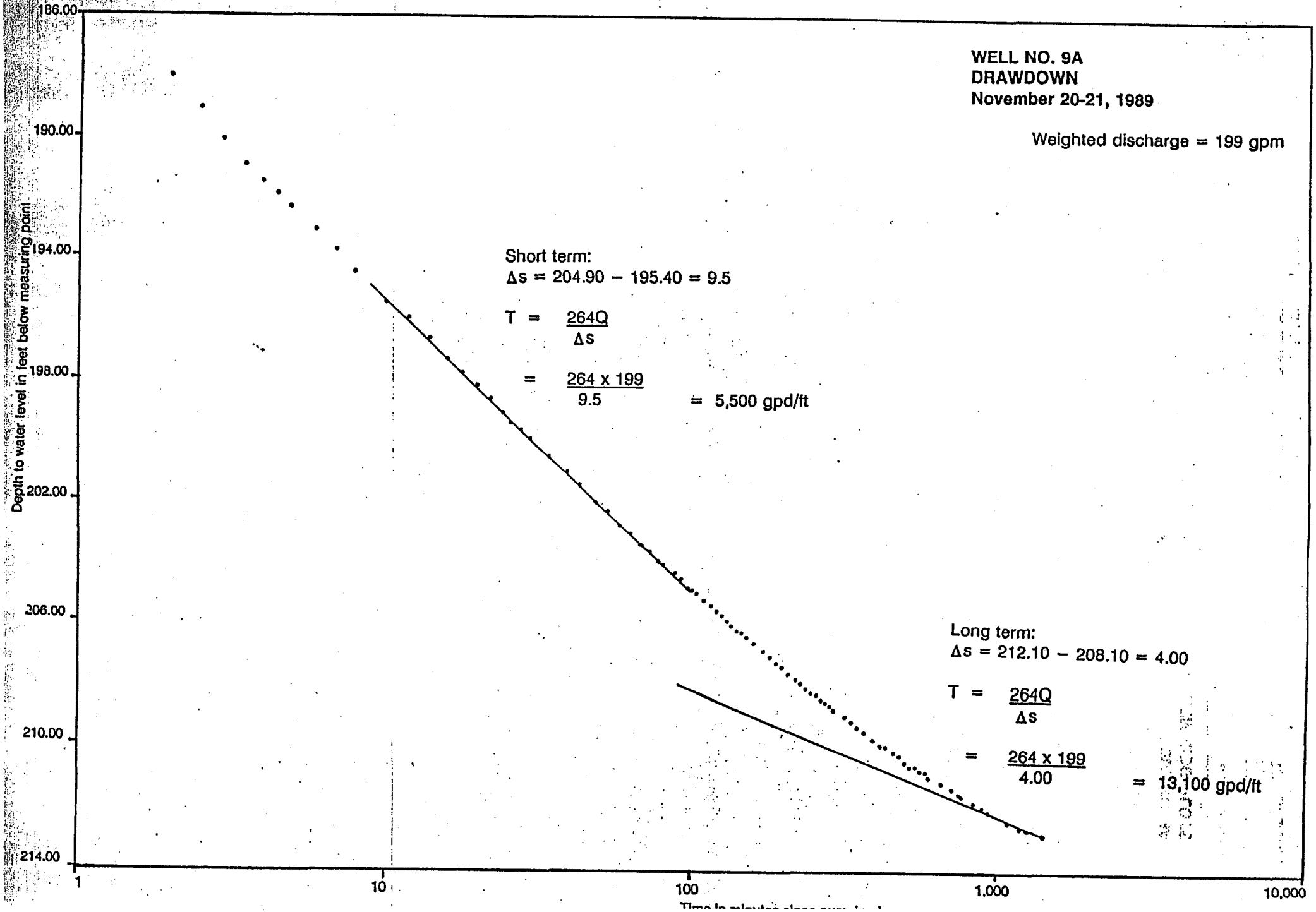
WELL NO. 8
RECOVERY
November 2, 1989

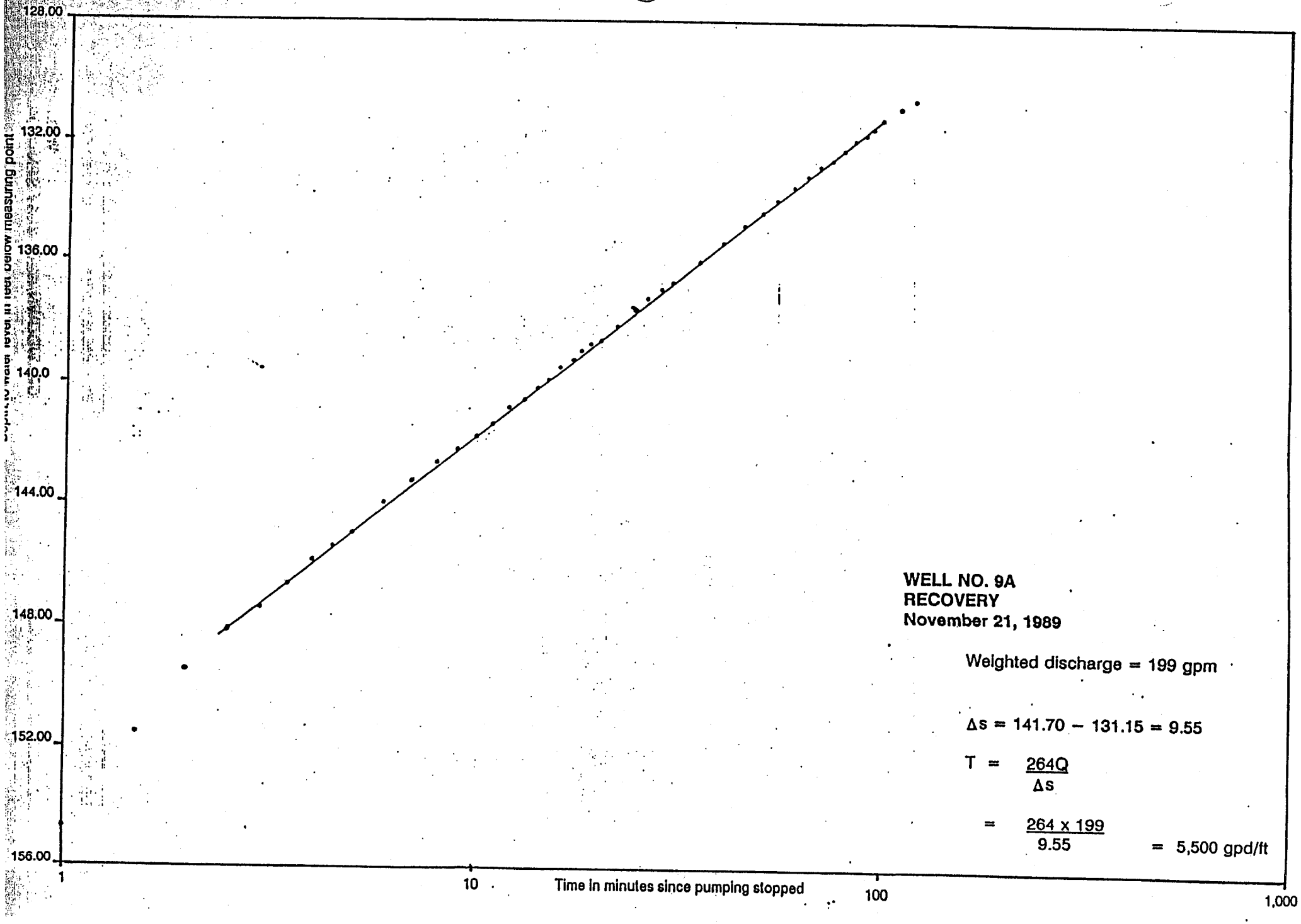
Weighted discharge = 170 gpm

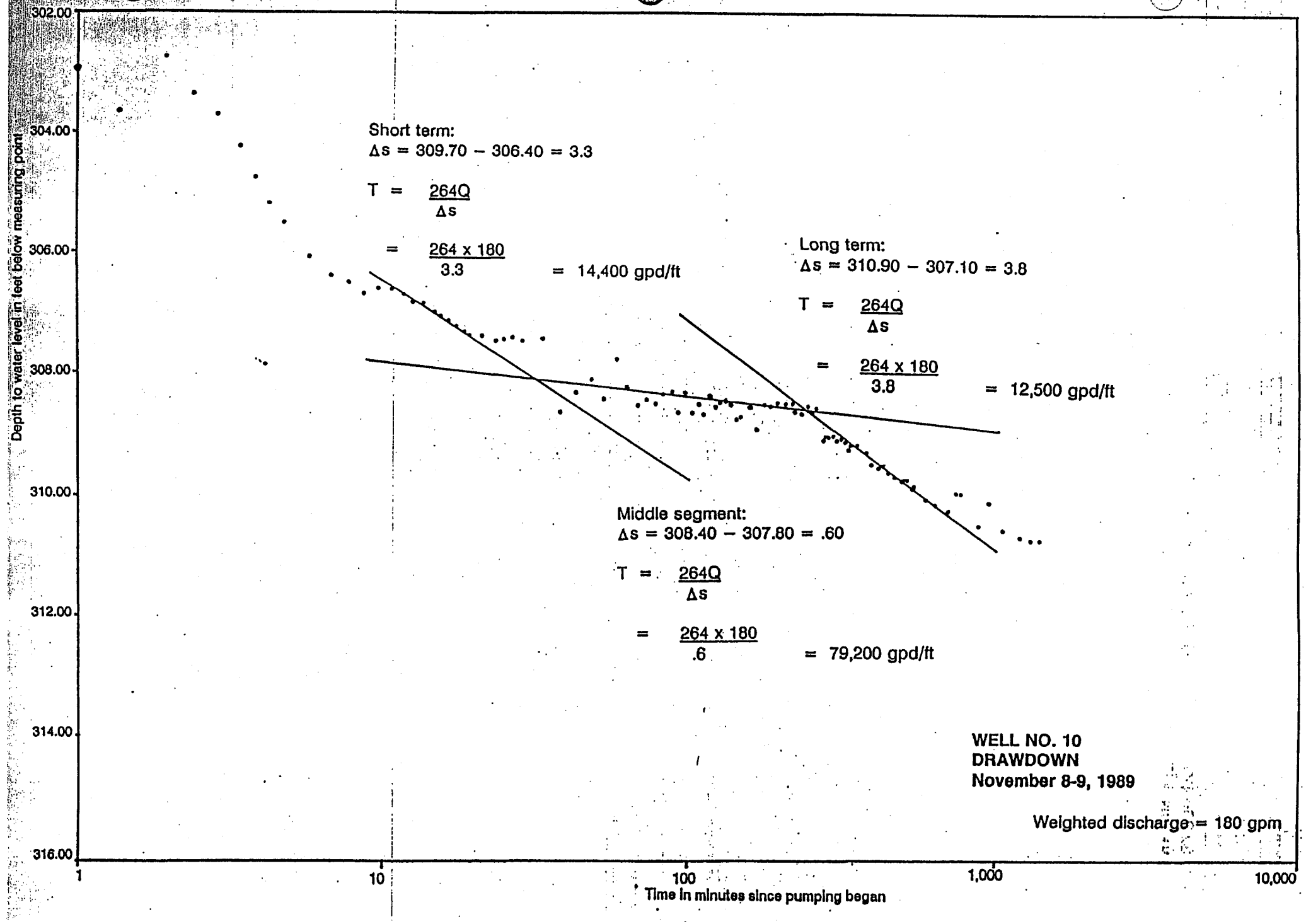
$\Delta s = 381.84 - 381.49 = .35$

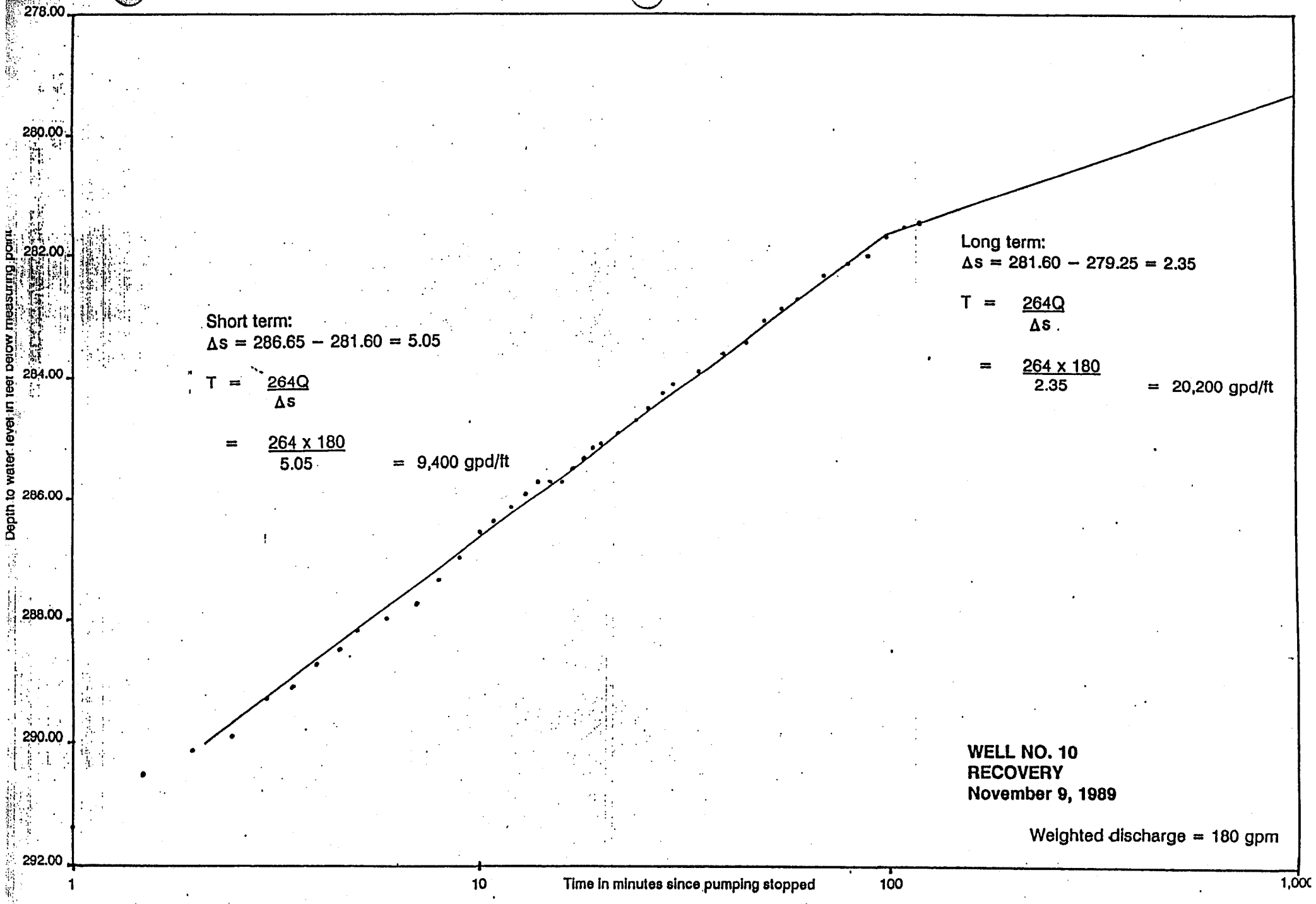
$$T = \frac{264Q}{\Delta s}$$

$$= \frac{264 \times 170}{.35} = 128{,}200 \text{ gpd/ft}$$


WELL NO. 9A
DRAWDOWN
November 20-21, 1989
Weighted discharge = 199 gpm
Short term:
Δs = 204.90 − 195.40 = 9.5
T = 264Q / Δs
= 264 x 199 / 9.5 = 5,500 gpd/ft
Long term:
Δs = 212.10 − 208.10 = 4.00
T = 264Q / Δs
= 264 x 199 / 4.00 = 13,100 gpd/ft
Depth to water level in feet below measuring point
186.00
190.00
194.00
198.00
202.00
206.00
210.00
214.00
1
10
100
1,000
10,000


128.00
132.00
136.00
140.0
144.00
148.00
152.00
156.00
Depth to water level in feet below measuring point
1
10
100
1,000
Time in minutes since pumping stopped
WELL NO. 9A
RECOVERY
November 21, 1989
Weighted discharge = 199 gpm
Δs = 141.70 − 131.15 = 9.55
T = 264Q / Δs
= 264 x 199 / 9.55
= 5,500 gpd/ft


Depth to water level in feet below measuring point
302.00
304.00
306.00
308.00
310.00
312.00
314.00
316.00
1
10
100
1,000
10,000
Time in minutes since pumping began
Short term:
Δs = 309.70 − 306.40 = 3.3
T = 264Q / Δs
= 264 x 180 / 3.3 = 14,400 gpd/ft
Long term:
Δs = 310.90 − 307.10 = 3.8
T = 264Q / Δs
= 264 x 180 / 3.8 = 12,500 gpd/ft
Middle segment:
Δs = 308.40 − 307.80 = .60
T = 264Q / Δs
= 264 x 180 / .6 = 79,200 gpd/ft
WELL NO. 10
DRAWDOWN
November 8-9, 1989
Weighted discharge = 180 gpm


278.00
280.00
282.00
284.00
286.00
288.00
290.00
292.00
Depth to water level in feet below measuring point
1
10
100
1,000
Time in minutes since pumping stopped
Short term:
Δs = 286.65 − 281.60 = 5.05
T = 264Q / Δs
= 264 x 180 / 5.05 = 9,400 gpd/ft
Long term:
Δs = 281.60 − 279.25 = 2.35
T = 264Q / Δs
= 264 x 180 / 2.35 = 20,200 gpd/ft
WELL NO. 10
RECOVERY
November 9, 1989
Weighted discharge = 180 gpm

APPENDIX C

APPENDIX C

GROUND-WATER SURFACE MEASUREMENTS

ADWR GWSI Water Levels

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-05 03DDD	20-Nov-91	104.55	1050	A	S	*
B-02-05 03DDD	28-Oct-97	102.6	1052	A	V	
B-02-05 06DDD	19-Nov-91	290.2	935	A	V	*
B-02-05 06DDD	28-Oct-97	288.2	937	A	V	
B-02-05 06DDD	29-Oct-98	286.3	939	A	V	
B-02-05 10AAB	28-Oct-97	111.9	1048	A	V	
B-02-05 10AAB	20-Nov-91	112.5	1048	A	V	*
B-02-05 10DAB	15-Jul-81	97.9	1052	A	S	*
B-02-05 10DAB	20-Nov-91	122.05	1028	A	S	*
B-02-05 10DAB	28-Oct-97	121.7	1028	A	V	
B-02-05 10DDC	15-Jul-81	93	1059	*	S	*
B-02-05 15BBC	23-Mar-81	122	1038	A	V	*
B-02-05 15BBC	14-Jan-82	124	1036	A	V	*
B-02-05 15BBC	19-Jan-70	125	1035	U	S	*
B-02-05 15BBC	08-May-69	123.05	1037	U	S	*
B-02-05 15BBC	08-May-67	123.05	1037	U	*	*
B-02-05 15BBC	28-Oct-97	129	1031	A	V	
B-02-05 15BBC	20-Nov-91	129.5	1031	A	V	*
B-02-05 15BBC	08-Jan-87	127.1	1033	A	V	*
B-02-05 25BAB	21-Dec-82	146.6	1002	A	S	*
B-02-05 25BAB	10-Dec-86	148.3	1001	A	V	*
B-02-05 25BAB	25-Nov-91	149.6	999	A	V	*
B-02-05 25BAB	27-Oct-98	149.9	999	A	V	
B-02-05 25BAB	20-Nov-97	149.7	999	A	V	
B-02-05 25CAA	10-Dec-86	142.7	996	A	V	*
B-02-05 25CAC	10-Dec-86	139.9	990	A	V	*
B-02-05 25CAC	27-Nov-91	141.2	989	A	V	*
B-02-05 25CDB	25-Nov-91	140.4	994	A	V	*
B-02-05 25CDB	21-Jan-82	148.8	985	A	S	*
B-02-05 25CDB	10-Dec-86	139.1	995	A	V	*
B-02-05 25CDB	20-Nov-97	140.4	994	A	V	
B-02-05 29AAC	01-Mar-60	139.15	994	*	S	*
B-02-05 29AAC	01-Mar-63	145.64	987	*	S	*
B-02-05 29AAC	14-Mar-62	137.24	996	*	S	*
B-02-05 29AAC	03-Jan-58	136.02	997	*	S	*
B-02-05 29AAC	08-Jan-87	145.1	988	A	V	*
B-02-05 29AAC	14-Jan-82	144.8	988	*	S	*
B-02-05 29AAC	19-Jan-70	140.6	993	*	S	*
B-02-05 29AAC	19-Nov-56	135.74	997	*	S	*
B-02-05 29AAC	27-Jan-81	141.7	991	*	V	*
B-02-05 29DAC	19-Jan-70	136.4	991	U	V	*
B-02-05 29DAC	12-Mar-69	136.2	991	U	S	*
B-02-05 29DAC	26-Jan-68	135.94	991	U	S	*
B-02-05 29DAC	24-Jan-68	135.94	991	U	S	*
B-02-05 29DAC	24-Feb-67	135.78	991	U	S	*
B-02-05 29DAC	15-Mar-66	136.54	990	U	S	*
B-02-05 29DAC	31-Dec-63	136.75	990	U	S	*
B-02-05 29DAC	15-Mar-62	134.19	993	U	S	*
B-02-05 29DAC	16-Feb-65	137.14	990	U	S	*

ADWR GWSI Water Levels

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-05 29DAC	07-Jun-88	141.5	986	A	V	*
B-02-05 29DAC	18-Nov-92	142.75	984	A	V	*
B-02-05 29DAC	05-Feb-71	136.8	990	U	V	*
B-02-05 29DAC	15-Jan-75	137.2	990	U	S	*
B-02-05 29DAC	07-Jun-85	140.8	986	A	V	*
B-02-05 29DAC	27-Feb-78	138.4	989	U	S	*
B-02-05 29DAC	19-Feb-71	136.8	990	U	*	*
B-02-05 29DAC	22-Dec-76	138.3	989	U	S	*
B-02-05 29DAC	12-Dec-94	142.2	985	A	V	*
B-02-05 29DAC	31-Dec-86	140.6	986	A	V	*
B-02-05 29DAC	14-Jan-85	140.4	987	A	V	*
B-02-05 29DAC	03-Dec-85	141	986	A	V	*
B-02-05 29DAC	06-Jan-83	140.9	986	A	V	*
B-02-05 29DAC	05-Dec-83	140	987	A	V	
B-02-05 29DAC	29-Nov-89	141.9	985	A	V	*
B-02-05 29DAC	07-Jan-82	139.2	988	A	V	*
B-02-05 29DAC	19-Jan-81	138.2	989	A	V	*
B-02-05 29DAC	23-Jan-80	138.6	988	U	S	*
B-02-05 29DAC	20-Feb-79	140.1	987	U	V	*
B-02-05 29DAC	09-Jun-86	140.7	986	A	V	*
B-02-05 29DAC	06-Dec-93	141.8	985	A	V	*
B-02-05 29DAC	06-Nov-97	143	984	A	V	
B-02-05 29DAC	09-Jan-76	137.8	989	U	S	*
B-02-05 29DAC	17-Jan-91	142.4	985	A	V	*
B-02-05 29DAC	02-Dec-91	142.5	985	A	V	*
B-02-05 29DAC	15-Nov-95	142.5	985	A	V	*
B-02-05 29DAC	27-Oct-98	143.3	984	A	V	
B-02-05 29DAC	11-Jun-87	140.9	986	A	V	*
B-02-05 29DAC	28-Dec-71	136.7	990	U	S	*
B-02-05 29DAC	18-Dec-87	141.1	986	A	V	*
B-02-05 29DAC	07-Dec-88	141.5	986	A	V	*
B-02-05 29DAC	13-Nov-96	143	984	A	V	*
B-02-05 29DAC	01-Mar-63	136.78	990	U	S	*
B-02-05 29DAC	18-Jan-74	137	990	U	S	*
B-02-05 29DAC	07-Feb-73	136.8	990	U	S	*
B-02-05 30BCC	03-Dec-91	144.3	976	A	V	*
B-02-05 30BCC	08-Jan-87	142.4	978	A	V	*
B-02-05 31BCA1	01-Mar-60	110.55	987	*	R	*
B-02-05 31BCA1	30-Dec-57	110.1	988	*	S	*
B-02-05 31BCA1	30-Jan-72	114	984	*	*	*
B-02-05 31BCA1	14-Mar-62	111.66	986	*	*	*
B-02-05 31BCA2	08-Jan-87	113.1	985	A	V	*
B-02-05 31BCA2	03-Dec-91	111.6	986	A	V	*
B-02-05 31BCA2	06-Nov-97	130	968	A	V	
B-02-05 32ABA	15-Mar-62	128.66	991	U	S	*
B-02-05 32ABA	06-Nov-97	137.5	983	A	V	*
B-02-06 03DCD	29-Oct-97	329.3	876	A	V	
B-02-06 03DCD	19-Nov-91	351.2	854	A	V	*
B-02-06 04CAA	19-Nov-91	365.6	842	A	V	*

ADWR GWSI Water Levels

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 04CAA	30-Oct-97	341.1	867	A	V	
B-02-06 04CAA	08-Dec-86	350.6	857	A	V	*
B-02-06 04CAA	22-Jan-82	357.9	850	A	V	*
B-02-06 04CAA	13-Jan-70	283.8	924	U	*	*
B-02-06 04CDA	01-Dec-88	357.7	840	A	V	*
B-02-06 04CDA	08-Dec-86	357.4	841	A	V	*
B-02-06 04CDA	22-Jan-82	347.8	850	*	V	*
B-02-06 04CDA	29-Jan-81	344.4	854	*	V	*
B-02-06 05DAA	30-Dec-71	285	916	U	S	*
B-02-06 05DAA	28-Mar-62	232.46	969	U	S	*
B-02-06 05DAA	15-Mar-66	253.72	947	U	S	*
B-02-06 05DAA	11-Nov-96	363.1	838	A	V	*
B-02-06 05DAA	08-Mar-63	239.52	961	U	S	*
B-02-06 05DAA	20-Nov-92	346.1	855	A	V	*
B-02-06 05DAA	14-Jan-85	351.3	850	A	V	*
B-02-06 05DAA	05-Mar-69	277.9	923	U	V	*
B-02-06 05DAA	24-Mar-61	228.16	973	U	S	*
B-02-06 05DAA	08-Dec-86	345.2	856	A	V	*
B-02-06 05DAA	04-Dec-85	356.6	844	A	V	*
B-02-06 05DAA	06-Jan-83	350.6	850	A	V	*
B-02-06 05DAA	11-Feb-65	248.15	953	U	S	*
B-02-06 05DAA	29-Nov-89	357	844	A	V	*
B-02-06 05DAA	07-Dec-88	350.2	851	A	V	*
B-02-06 05DAA	18-Dec-87	343.2	858	A	V	*
B-02-06 05DAA	11-Jun-87	346.7	854	A	V	*
B-02-06 05DAA	13-Jan-70	289.2	912	U	S	*
B-02-06 05DAA	08-Dec-86	344.2	857	A	V	*
B-02-06 05DAA	05-Feb-71	286.4	915	U	V	*
B-02-06 05DAA	11-Jun-86	356.7	844	A	V	*
B-02-06 05DAA	02-Dec-93	336.9	864	A	V	*
B-02-06 05DAA	23-Nov-94	352.1	849	A	V	*
B-02-06 05DAA	23-Jan-80	336.5	865	U	V	*
B-02-06 05DAA	24-Feb-78	319.4	882	U	V	*
B-02-06 05DAA	22-Dec-76	320.2	881	U	V	*
B-02-06 05DAA	09-Jan-76	321.6	879	U	*	*
B-02-06 05DAA	30-Jan-75	318.9	882	U	S	*
B-02-06 05DAA	31-Dec-86	342.5	859	A	V	*
B-02-06 05DAA	05-Dec-83	351.6	849	A	V	
B-02-06 05DBB	18-Nov-91	372.5	826	A	V	*
B-02-06 05DBB	08-Dec-86	352.6	845	A	V	*
B-02-06 05DBB	30-Oct-97	327.2	871	A	V	
B-02-06 06CBB	08-Mar-63	243.32	973	*	S	*
B-02-06 06CBB	12-Mar-62	239.39	977	*	S	*
B-02-06 06CBB	11-Feb-65	247.24	969	*	S	*
B-02-06 06CBB	15-Mar-66	250.76	965	*	S	*
B-02-06 06CBB	24-Feb-67	263.34	953	*	S	*
B-02-06 06CBB	26-Jan-68	267.38	949	*	S	*
B-02-06 06CBB	13-Jan-70	286.6	929	*	S	*
B-02-06 06CBB	05-Feb-71	281.3	935	*	S	*

ADWR GWSI Water Levels

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 06CBB	30-Dec-71	288.3	928	*	S	*
B-02-06 06CBB	18-Jan-74	297.1	919	*	S	*
B-02-06 06CBB	31-Dec-63	247.8	968	*	S	*
B-02-06 06DAA	13-Jan-70	282.1	916	U	S	*
B-02-06 06DAA	30-Oct-97	331.5	867	A	V	
B-02-06 06DAA	19-Nov-91	355.1	843	A	V	*
B-02-06 06DAA	08-Dec-86	341.1	857	A	V	*
B-02-06 06DAA	30-Dec-71	288	910	U	*	*
B-02-06 06DAA	01-Jan-69	273	925	U	E	*
B-02-06 06DAA	22-Jan-82	346.6	851	A	S	*
B-02-06 08AAA	18-Nov-91	343.7	846	A	V	
B-02-06 08AAA	30-Oct-97	318.7	871	A	V	
B-02-06 08AAA	08-Dec-86	329.7	860	A	V	*
B-02-06 08AAA	26-Jan-81	336.7	853	A	V	*
B-02-06 08AAA	01-Mar-63	232.38	958	U	S	*
B-02-06 08AAA	14-Mar-62	221.19	969	U	S	*
B-02-06 08AAA	22-Jan-82	335.6	854	A	V	*
B-02-06 08AAA	13-Jan-70	265.4	925	U	S	*
B-02-06 08CAA	13-Jan-70	241.5	929	U	S	*
B-02-06 08CAA	08-Dec-86	307.4	863	A	V	*
B-02-06 08CAA	19-Nov-91	319.6	850	A	V	*
B-02-06 08CAA	30-Oct-97	294.2	876	A	V	
B-02-06 08CAA	26-Jan-81	307	863	A	V	*
B-02-06 08CAA	22-Jan-82	308.87	861	A	S	*
B-02-06 09ABA	29-Jan-81	335.9	861	*	V	*
B-02-06 09ABA	30-Dec-71	282	915	*	*	*
B-02-06 09ABA	18-Nov-91	346.7	850	A	V	*
B-02-06 09ABA	30-Jan-75	300.8	896	*	S	*
B-02-06 09ABA	22-Jan-82	340.3	857	*	V	*
B-02-06 09ABA	08-Dec-86	334.3	863	A	V	*
B-02-06 09BBA	08-Dec-86	331.3	863	A	V	*
B-02-06 09BBA	30-Oct-97	320.5	874	A	V	
B-02-06 09BBA	18-Nov-91	345.1	849	A	V	*
B-02-06 09CBB	22-Jan-82	335.8	839	A	V	*
B-02-06 09CBB	04-Dec-85	324.8	850	A	V	*
B-02-06 09CBB	25-Jan-84	315.7	859	A	V	*
B-02-06 09CBB	09-Jan-85	319.3	856	A	V	*
B-02-06 09CBB	06-Jun-85	342.6	832	A	V	*
B-02-06 09CBB	07-Dec-88	313	862	A	V	*
B-02-06 09CBB	23-Nov-94	303.6	871	A	V	*
B-02-06 09CBB	29-Oct-98	300	875	A	V	
B-02-06 09CBB	30-Oct-97	300.8	874	A	V	
B-02-06 09CBB	11-Nov-96	303	872	A	V	*
B-02-06 09CBB	01-Dec-88	313.8	861	A	V	*
B-02-06 09CBB	08-Dec-86	297.1	878	A	V	*
B-02-06 09CBB	02-Dec-93	298.8	876	A	V	*
B-02-06 09CBB	20-Nov-92	307.7	867	A	V	*
B-02-06 09CBB	19-Nov-91	318.7	856	A	V	*
B-02-06 09CBB	15-Jan-91	316.7	858	A	V	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 09CBB	29-Nov-89	322.2	853	A	V	*
B-02-06 09CBB	18-Dec-87	309.7	865	A	V	*
B-02-06 09CBB	08-Jan-87	311.2	864	A	V	*
B-02-06 09CBB	31-Dec-86	310.8	864	A	V	*
B-02-06 09CBB	14-Nov-95	305.4	870	A	V	*
B-02-06 11BBB	19-Nov-91	345.6	867	A	V	*
B-02-06 12AAA	28-Oct-97	269	964	A	V	
B-02-06 12AAA	19-Nov-91	266.1	967	A	V	*
B-02-06 12AAA	08-Jan-87	260.8	972	A	V	*
B-02-06 12DDD	28-Oct-97	236.3	962	A	V	
B-02-06 12DDD	19-Nov-91	231.6	966	A	V	*
B-02-06 14BCC	28-Oct-97	278.9	886	A	V	
B-02-06 14BCC	19-Nov-91	304.6	860	A	V	*
B-02-06 16CAA1	28-Mar-62	205.43	952	U	*	*
B-02-06 16CAA1	08-Dec-86	338.4	819	A	V	*
B-02-06 16CAA1	19-Nov-56	171.02	986	U	S	*
B-02-06 16CAA1	19-Nov-91	295	862	A	V	*
B-02-06 16CAA1	22-Jan-82	299.6	857	A	V	*
B-02-06 16CAA1	05-Mar-69	231.3	926	U	*	*
B-02-06 16CAA1	03-Jan-58	173.44	984	U	*	*
B-02-06 16CAA1	13-Jan-70	228.4	929	U	*	*
B-02-06 16DCC	17-Jan-92	152.4	988	A	V	*
B-02-06 16DCC	30-Oct-97	148.5	992	A	V	
B-02-06 17AAA	30-Oct-97	282.6	877	A	V	
B-02-06 17AAA	01-Jan-69	229	931	U	E	*
B-02-06 17AAA	26-Jan-81	296.4	864	A	V	*
B-02-06 17AAA	22-Jan-82	299.72	860	A	S	*
B-02-06 17AAA	08-Dec-86	296.8	863	A	V	*
B-02-06 17AAA	19-Nov-91	306.9	853	A	V	*
B-02-06 17AAA	30-Dec-71	247	913	U	*	*
B-02-06 17AAA	13-Jan-70	233.1	927	U	S	*
B-02-06 17BDB	18-Dec-53	164.75	977	*	S	*
B-02-06 17BDB	19-Nov-56	167.7	974	*	S	*
B-02-06 17BDB	17-Dec-58	161.76	980	*	S	*
B-02-06 17BDB	03-Jan-58	169.87	972	*	S	*
B-02-06 17BDB	01-Mar-60	160.01	982	*	S	*
B-02-06 17BDB	22-Mar-61	190.72	951	*	S	*
B-02-06 17CCD	19-Nov-91	272.8	854	A	V	*
B-02-06 17DAA	13-Jan-70	214.7	929	U	S	*
B-02-06 17DAA	01-Jan-69	211	933	U	E	*
B-02-06 17DAA	22-Jan-82	279.58	864	A	S	*
B-02-06 17DAA	08-Dec-86	277.8	866	A	V	*
B-02-06 17DAA	19-Nov-91	285	859	A	V	*
B-02-06 17DAA	30-Oct-97	262	882	A	V	
B-02-06 17DAA	26-Jan-81	274.2	870	A	V	*
B-02-06 19BBB	25-Jan-82	247.1	883	*	S	*
B-02-06 19BBB	08-Dec-86	267.4	863	A	V	*
B-02-06 19BBB	19-Nov-91	272	858	A	V	*
B-02-06 19BBB	25-Jan-81	233	897	*	*	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 19CDB	26-Nov-91	251.7	849	A	V	*
B-02-06 19CDB	31-Oct-97	236.8	864	A	V	
B-02-06 19DAA	13-Jan-70	193.2	921	U	*	*
B-02-06 19DAA	19-Nov-56	140.2	974	U	S	*
B-02-06 19DAA	08-Dec-86	250.1	864	A	V	*
B-02-06 19DAA	25-Jan-82	250.7	863	A	V	*
B-02-06 19DAA	17-Dec-58	152.69	961	U	*	*
B-02-06 19DAA	25-Jan-81	242.1	872	A	V	*
B-02-06 19DAA	19-Nov-91	254	860	A	V	*
B-02-06 19DAA	12-Mar-62	176.99	937	U	*	*
B-02-06 19DAA	21-Mar-61	158.8	955	U	*	*
B-02-06 19DAA	05-Mar-69	196	918	U	*	*
B-02-06 19DAA	29-Oct-97	240.4	874	A	V	
B-02-06 20ABA	19-Nov-91	272.7	857	A	V	*
B-02-06 20ABA	08-Dec-86	266.2	864	A	V	*
B-02-06 20ABA	29-Oct-97	260.6	869	A	V	
B-02-06 20ABA	01-Dec-88	264.5	866	A	V	*
B-02-06 20BBA	29-Oct-97	256.3	868	A	V	
B-02-06 20BBA	01-Mar-63	183.31	941	U	S	*
B-02-06 20BBA	05-Mar-69	206.9	917	U	S	*
B-02-06 20BBA	22-Mar-61	170.6	953	U	S	*
B-02-06 20BBA	19-Nov-91	269	855	A	V	*
B-02-06 20BBA	30-Dec-71	224	900	U	*	*
B-02-06 20BBA	13-Jan-70	205.5	919	U	S	*
B-02-06 20BBA	08-Dec-86	265.1	859	A	V	*
B-02-06 20CDD1	31-Jan-52	120.8	981	*	S	*
B-02-06 20CDD1	26-Jan-51	120.75	981	*	S	*
B-02-06 20CDD1	26-Jan-81	69.8	1032	*	V	*
B-02-06 20CDD1	29-Mar-54	123.19	979	*	S	*
B-02-06 20CDD1	23-Mar-50	123.15	979	*	S	*
B-02-06 20CDD1	09-Dec-53	125.95	976	*	S	*
B-02-06 20CDD1	04-Mar-49	120.79	981	*	S	*
B-02-06 20CDD1	13-May-48	120.77	981	*	S	*
B-02-06 20CDD1	02-May-46	89.03	1013	*	S	*
B-02-06 20CDD1	13-Oct-48	120.78	981	*	S	*
B-02-06 20DAA	19-Nov-91	255.4	863	A	V	*
B-02-06 20DAA	29-Oct-97	243.8	874	A	V	
B-02-06 20DAA	24-Mar-61	172.01	946	U	S	*
B-02-06 20DAA	30-Dec-71	226	892	U	*	*
B-02-06 20DAA	26-Jan-81	246.1	872	A	V	*
B-02-06 20DAA	25-Jan-82	251.6	866	A	V	*
B-02-06 21BBA	11-Jun-87	265.4	871	A	V	*
B-02-06 21BBA	30-Dec-71	241	895	U	*	*
B-02-06 21BBA	15-Jan-91	258.1	878	A	V	*
B-02-06 21BBA	02-Dec-93	245.4	891	A	V	*
B-02-06 21BBA	19-Jan-81	230.2	906	A	V	*
B-02-06 21BBA	24-Mar-61	183.64	952	U	S	*
B-02-06 21BBA	14-Mar-62	185.07	951	U	*	*
B-02-06 21BBA	14-Jan-85	259.6	876	A	V	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 21BBA	11-Feb-65	186.35	950	U	*	*
B-02-06 21BBA	27-Feb-78	227.6	908	U	V	*
B-02-06 21BBA	15-Mar-66	199.52	936	U	*	*
B-02-06 21BBA	24-Mar-67	214.35	922	U	*	*
B-02-06 21BBA	19-Nov-91	263.6	872	A	V	*
B-02-06 21BBA	09-Jan-76	227.8	908	U	V	*
B-02-06 21BBA	01-Mar-63	193.59	942	U	*	*
B-02-06 21BBA	20-Feb-79	260.5	876	U	V	*
B-02-06 21BBA	08-Dec-86	254.6	881	A	V	*
B-02-06 21BBA	22-Jan-82	257.9	878	U	V	*
B-02-06 21BBA	06-Jan-83	258.5	878	A	V	*
B-02-06 21BBA	05-Dec-83	259.4	877	A	V	
B-02-06 21BBA	29-Nov-89	262.7	873	A	V	*
B-02-06 21BBA	06-Jun-85	293.4	843	A	V	*
B-02-06 21BBA	07-Dec-88	248.9	887	A	V	*
B-02-06 21BBA	13-Jan-70	209	927	U	V	*
B-02-06 21BBA	27-Oct-98	244.3	892	A	V	
B-02-06 21BBA	30-Oct-97	243.5	893	A	V	
B-02-06 21BBA	11-Nov-96	245	891	A	V	*
B-02-06 21BBA	14-Nov-95	251.1	885	A	V	*
B-02-06 21BBA	23-Nov-94	249.3	887	A	V	*
B-02-06 21BBA	20-Nov-92	252.7	883	A	V	*
B-02-06 21BBA	22-Dec-76	229	907	U	V	*
B-02-06 21BBB	30-Oct-97	254.8	879	A	V	
B-02-06 21BBB	19-Nov-91	271.7	862	A	V	*
B-02-06 21BBB	08-Dec-86	266.8	867	A	V	*
B-02-06 21DBB	08-Dec-86	131.8	995	A	V	*
B-02-06 21DBB	13-Jan-70	200	927	U	S	*
B-02-06 21DBB	06-Mar-69	219	908	U	S	*
B-02-06 21DBB	01-Mar-63	195.43	932	U	S	*
B-02-06 21DBB	30-Oct-97	106.2	1021	A	V	
B-02-06 21DBB	19-Nov-91	114.6	1012	A	V	*
B-02-06 21DBB	08-Jan-75	228.8	898	U	S	*
B-02-06 21DBB	30-Dec-71	235	892	U	S	*
B-02-06 21DBB	14-Mar-62	195.48	932	U	S	*
B-02-06 23AAA	28-Oct-97	263.9	900	A	V	
B-02-06 23AAA	20-Nov-91	317.7	846	A	V	*
B-02-06 23AAA	01-Dec-88	303.2	861	A	V	*
B-02-06 23AAA	04-Dec-86	278.4	886	A	V	*
B-02-06 23AAB	28-Oct-97	206.9	953	A	V	
B-02-06 23AAB	17-Jan-92	213.4	947	A	V	*
B-02-06 23AAB	04-Dec-86	276.8	883	A	V	*
B-02-06 23AAB	14-Mar-62	176.85	983	U	S	*
B-02-06 23AAB	01-Mar-63	182.76	977	U	*	*
B-02-06 23AAB	30-Dec-71	191	969	U	*	*
B-02-06 23AAB	15-Jan-75	191.9	968	U	*	*
B-02-06 23AAB	25-Jan-82	270.3	890	A	V	*
B-02-06 23AAB	26-Jan-81	266.8	893	A	V	*
B-02-06 23ABA	17-Dec-58	192.68	969	U	S	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 23ABA	03-Jan-58	183.2	979	U	S	*
B-02-06 23ABA	11-Feb-65	187.3	975	U	S	*
B-02-06 23ABA	20-Nov-91	222.5	940	A	V	*
B-02-06 23ABA	26-Jan-81	271.8	890	A	V	*
B-02-06 23ABA	28-Oct-97	206.3	956	A	V	
B-02-06 23ABA	01-Mar-60	174.03	988	U	S	*
B-02-06 23ABA	14-Mar-62	176.33	986	U	S	*
B-02-06 23ABA	31-Dec-63	181.86	980	U	S	*
B-02-06 23ABA	15-Mar-66	181.05	981	U	S	*
B-02-06 23ABA	30-Dec-71	191	971	U	S	*
B-02-06 23ABA	15-Jan-75	190.92	971	U	S	*
B-02-06 23ABA	06-Dec-56	178.51	983	U	S	*
B-02-06 23ABA	25-Jan-82	278.7	883	A	S	*
B-02-06 23ABB	28-Oct-97	248	910	A	V	
B-02-06 23ABB	20-Nov-91	262.2	896	A	V	*
B-02-06 23DDC	17-Dec-58	146.48	992	*	S	*
B-02-06 23DDC	24-Mar-61	147.7	990	*	S	*
B-02-06 23DDC	14-Mar-61	147.7	990	*	S	*
B-02-06 23DDC	01-Mar-63	147.15	991	*	S	*
B-02-06 23DDC	26-Jan-81	122.2	1016	*	V	*
B-02-06 23DDC	03-Jan-58	147.08	991	*	S	*
B-02-06 23DDC	17-Dec-56	147.1	991	*	S	*
B-02-06 23DDC	14-Mar-62	151.87	986	*	S	*
B-02-06 24BDD	28-Oct-97	181.2	974	A	V	
B-02-06 24BDD	20-Nov-91	184.1	971	A	V	*
B-02-06 24CBA	04-Dec-86	176	974	A	V	*
B-02-06 24CBA	01-Mar-63	169.41	981	*	S	*
B-02-06 24CBA	12-Mar-69	16.41	1134	*	S	*
B-02-06 24CBA	12-Jan-70	164.5	986	*	S	*
B-02-06 24CBA	12-Mar-70	164.1	986	*	*	*
B-02-06 24CBA	30-Dec-71	165	985	*	*	*
B-02-06 24CBA	09-Sep-92	179.5	971	A	V	*
B-02-06 24CBA	24-Mar-61	161.78	988	*	S	*
B-02-06 24CBA	14-Mar-62	166.5	984	*	S	*
B-02-06 24DAB	22-Jan-82	240.42	915	*	S	*
B-02-06 24DAD	04-Dec-86	165.9	984	A	V	*
B-02-06 24DCB2	27-Jan-81	168.7	953	*	V	*
B-02-06 24DCB2	25-Jan-82	167.3	955	*	S	*
B-02-06 24DCB2	04-Dec-86	165.4	957	A	V	*
B-02-06 25BAA	03-Jan-58	152.14	987	*	S	*
B-02-06 25BAA	06-Dec-56	146.17	993	*	S	*
B-02-06 25BAA	09-Dec-53	157.7	982	*	S	*
B-02-06 27ADA	15-Jan-75	136.85	981	*	S	*
B-02-06 27ADA	30-Dec-71	136	982	*	S	*
B-02-06 27ADA	06-Mar-69	135.1	983	*	S	*
B-02-06 27ADA	06-Nov-97	143.5	975	A	V	
B-02-06 27ADA	14-Mar-62	133.24	985	*	S	*
B-02-06 27ADA	04-Dec-86	139.9	978	A	V	*
B-02-06 27ADA	12-Jan-70	135.3	983	*	S	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 27ADA	25-Jan-82	143.8	974	A	S	*
B-02-06 27ADA	26-Jan-81	137.1	981	A	V	*
B-02-06 27ADA	01-Mar-63	135.56	982	*	S	*
B-02-06 27BAB	14-Mar-62	144.77	977	*	*	*
B-02-06 27BAB	22-Mar-61	154.75	967	*	S	*
B-02-06 27BAB	30-Dec-71	196	926	*	*	*
B-02-06 27DBA	16-Apr-81	133.1	977	*	V	*
B-02-06 27DBB	16-Apr-81	131.8	978	*	V	*
B-02-06 28AAC	03-Dec-91	196.1	915	A	V	*
B-02-06 28BAB	25-Jan-82	193.7	917	*	S	*
B-02-06 28BAB	12-Jan-70	182.8	928	*	S	*
B-02-06 28BAB	25-Jan-81	184.8	926	*	V	*
B-02-06 28BAB	04-Dec-86	235	876	A	V	*
B-02-06 28BAB	12-Mar-69	194.1	917	*	S	*
B-02-06 28BAB	14-Mar-62	166.29	945	*	S	*
B-02-06 28BAB	01-Mar-60	159.16	952	*	S	*
B-02-06 28BAB	17-Dec-58	150.1	961	*	S	*
B-02-06 28BAB	03-Jan-58	144.6	966	*	S	*
B-02-06 28BAB	06-Dec-56	140.5	971	*	S	*
B-02-06 28BAB	31-Oct-97	223	888	A	V	
B-02-06 28BAB	26-Nov-91	228.6	882	A	V	*
B-02-06 29BAB	26-Nov-91	248	852	A	V	*
B-02-06 29BAB	31-Oct-97	238.2	862	A	V	
B-02-06 29DCC	06-Nov-97	196.3	877	A	V	
B-02-06 30AAA	31-Oct-97	237	869	A	V	
B-02-06 30AAA	26-Nov-91	250.3	856	A	V	*
B-02-06 30AAA	08-Dec-86	247.2	859	A	V	*
B-02-06 30BBB	27-Nov-91	249.4	846	A	V	*
B-02-06 31AAA	04-Dec-86	233.3	846	A	V	*
B-02-06 31AAA	26-Nov-91	235.2	844	A	V	*
B-02-06 31AAA	27-Jan-82	239.6	839	*	S	*
B-02-06 31AAA	31-Oct-97	229.5	850	A	V	
B-02-06 31DAA	01-Mar-63	145.54	919	*	S	*
B-02-06 31DAA	01-Mar-60	120.78	944	*	S	*
B-02-06 31DAA	07-Nov-56	108.45	957	*	S	*
B-02-06 31DAA	08-Jan-75	184.2	881	*	S	*
B-02-06 31DAA	26-Nov-91	206.7	858	A	V	*
B-02-06 31DAA	31-Dec-63	131.67	933	*	S	*
B-02-06 31DAA	11-Feb-65	136.05	929	*	S	*
B-02-06 31DAA	13-Mar-69	158	907	*	S	*
B-02-06 31DDD	08-Jan-75	179.9	878	*	S	*
B-02-06 31DDD	26-Nov-91	209.3	849	A	V	*
B-02-06 32BAB	08-Jan-75	200.4	871	U	S	*
B-02-06 32BAB	26-Nov-91	226.3	845	A	V	*
B-02-06 32BAB	04-Nov-97	215	856	A	V	
B-02-06 33CAA	17-Jan-91	210.3	865	A	V	*
B-02-06 33CAA	26-May-55	111.36	964	*	S	*
B-02-06 33CAA	31-Oct-97	200.1	875	A	V	
B-02-06 33CAA	23-Nov-94	202.3	873	A	V	*

LOCAL_ID	WL_DATE	WL_DEPTH	WL_ELEV	SOURCE	METHOD	REMARK
B-02-06 27ADA	25-Jan-82	143.8	974	A	S	*
B-02-06 27ADA	26-Jan-81	137.1	981	A	V	*
B-02-06 27ADA	01-Mar-63	135.56	982	*	S	*
B-02-06 27BAB	14-Mar-62	144.77	977	*	*	*
B-02-06 27BAB	22-Mar-61	154.75	967	*	S	*
B-02-06 27BAB	30-Dec-71	196	926	*	*	*
B-02-06 27DBA	16-Apr-81	133.1	977	*	V	*
B-02-06 27DBB	16-Apr-81	131.8	978	*	V	*
B-02-06 28AAC	03-Dec-91	196.1	915	A	V	*
B-02-06 28BAB	25-Jan-82	193.7	917	*	S	*
B-02-06 28BAB	12-Jan-70	182.8	928	*	S	*
B-02-06 28BAB	25-Jan-81	184.8	926	*	V	*
B-02-06 28BAB	04-Dec-86	235	876	A	V	*
B-02-06 28BAB	12-Mar-69	194.1	917	*	S	*
B-02-06 28BAB	14-Mar-62	166.29	945	*	S	*
B-02-06 28BAB	01-Mar-60	159.16	952	*	S	*
B-02-06 28BAB	17-Dec-58	150.1	961	*	S	*
B-02-06 28BAB	03-Jan-58	144.6	966	*	S	*
B-02-06 28BAB	06-Dec-56	140.5	971	*	S	*
B-02-06 28BAB	31-Oct-97	223	888	A	V	
B-02-06 28BAB	26-Nov-91	228.6	882	A	V	*
B-02-06 29BAB	26-Nov-91	248	852	A	V	*
B-02-06 29BAB	31-Oct-97	238.2	862	A	V	
B-02-06 29DCC	06-Nov-97	196.3	877	A	V	
B-02-06 30AAA	31-Oct-97	237	869	A	V	
B-02-06 30AAA	26-Nov-91	250.3	856	A	V	*
B-02-06 30AAA	08-Dec-86	247.2	859	A	V	*
B-02-06 30BBB	27-Nov-91	249.4	846	A	V	*
B-02-06 31AAA	04-Dec-86	233.3	846	A	V	*
B-02-06 31AAA	26-Nov-91	235.2	844	A	V	*
B-02-06 31AAA	27-Jan-82	239.6	839	*	S	*
B-02-06 31AAA	31-Oct-97	229.5	850	A	V	
B-02-06 31DAA	01-Mar-63	145.54	919	*	S	*
B-02-06 31DAA	01-Mar-60	120.78	944	*	S	*
B-02-06 31DAA	07-Nov-56	108.45	957	*	S	*
B-02-06 31DAA	08-Jan-75	184.2	881	*	S	*
B-02-06 31DAA	26-Nov-91	206.7	858	A	V	*
B-02-06 31DAA	31-Dec-63	131.67	933	*	S	*
B-02-06 31DAA	11-Feb-65	136.05	929	*	S	*
B-02-06 31DAA	13-Mar-69	158	907	*	S	*
B-02-06 31DDD	08-Jan-75	179.9	878	*	S	*
B-02-06 31DDD	26-Nov-91	209.3	849	A	V	*
B-02-06 32BAB	08-Jan-75	200.4	871	U	S	*
B-02-06 32BAB	26-Nov-91	226.3	845	A	V	*
B-02-06 32BAB	04-Nov-97	215	856	A	V	
B-02-06 33CAA	17-Jan-91	210.3	865	A	V	*
B-02-06 33CAA	26-May-55	111.36	964	*	S	*
B-02-06 33CAA	31-Oct-97	200.1	875	A	V	
B-02-06 33CAA	23-Nov-94	202.3	873	A	V	*

APPENDIX D

APPENDIX D

GROUND-WATER QUALITY DATA

TABLE 4-3

CHEMICAL AND RADIOLOGICAL QUALITY
OF WATER SAMPLES FROM TEST WELLS

(Abbreviations: mg/l = milligrams per liter; μmhos/cm = micromhos per centimeter; pCi/l = picocuries per liter. Trace metals are reported in micrograms per liter; have been converted to mg/l. N.D. = None Detected.)

Constituent	Unit	Well Numbers 2	3	4	5	6	7
Calcium	mg/l	25	29	13	17	18	13
Magnesium	mg/l	4.8	7.3	2.6	3.1	3.8	3.0
Sodium	mg/l	49	47	106	94	68	76
Potassium	mg/l	3.0	2.2	2.4	2.4	2.3	1.9
Carbonate	mg/l	N.D.	N.D.	N.D.	N.D.	3.4	9.4
Bicarbonate	mg/l	169	152	146	187	176	168
Chloride	mg/l	16.6	25.8	59.8	41.8	18.8	16.6
Sulfate	mg/l	22	19	50	44	21	23
Nitrate	mg/l	8.0	27.5	14.2	11.1	8.4	9.8
Fluoride	mg/l	1.4	.95	5.2	2.8	2.7	3.2
pH	pH units	7.8	8.1	8.1	8.1	8.2	8.4
Elec. Conductivity	μmhos	350	400	570	530	400	410
Total Dissolved Solids	mg/l	240	270	370	340	280	250
Arsenic	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	.011
Barium	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Cadmium	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Copper	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Iron	mg/l	N.D.	.076	.096	N.D.	.054	N.D.
Lead	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Manganese	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Mercury	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Selenium	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Silver	mg/l	N.D.	N.D.	N.D.	N.D.	N.D.	N.D.
Zinc	mg/l	.070	.095	.058	.082	.071	.067
Total Chromium	mg/l	.018	N.D.	.033	.028	.022	.023
Gross Alpha	pCi/l	<2	<2	<2	6±3	4±3	2±1

APPENDIX E

APPENDIX E

THWELLS MODEL OUTPUT FOR HASSAYAMPA RANCH 100-YEAR AQUIFER IMPACT ANALYSIS

********** THWELLS - version 4.01 **********
PAGE 1

CALCULATION OF DRAWDOWN IN A HOMOGENEOUS, ISOTROPIC, CONFINED, LEAKY CONFINED OR UNCONFINED AQUIFER WITH MULTIPLE PRODUCTION AND INJECTION WELLS AND UNIFORM REGIONAL FLOW

Belmont 100-yr Aquifer Impact Analysis

********** INPUT DATA
****

UNCONFINED AQUIFER - THEIS EQUATION WITH JACOB'S CORRECTION

WATER TABLE CORRECTION APPLIED; DRAWDOWNS EXCEED 10% OF SATURATED THICKNESS

AQUIFER THICKNESS = 650 [ft]
TRANSMISSIVITY = 54000 [gpd/ft]

STORAGE COEFFICIENT = .13

REGIONAL FLOW GRADIENT
(positive--downwards--in flow direction) = 0

REGIONAL FLOW DIRECTION
(horizontal angle in degrees
counter-clockwise from positive x-axis) = 0

REGIONAL FLOW OFFSET AT ORIGIN
(positive in downwards direction) = 0 [ft]

WATER TABLE CORRECTION APPLIED; DRAWDOWNS EXCEED 10% OF SATURATED THICKNESS

AQUIFER THICKNESS = 650 [ft]

PUMPING/INJECTION WELL DATA

WELL NO. 1

X-COORDINATE	=	1091074 [ft]
Y-COORDINATE	=	1.215577E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 2

X-COORDINATE	=	1092214 [ft]
Y-COORDINATE	=	1.216371E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 3

X-COORDINATE	=	1091758 [ft]
Y-COORDINATE	=	1.216904E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 4

X-COORDINATE	=	1091097 [ft]
Y-COORDINATE	=	1.217121E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 5

X-COORDINATE	=	1087266 [ft]
Y-COORDINATE	=	1.217401E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 6

X-COORDINATE	=	1077028 [ft]
Y-COORDINATE	=	1.217178E+07 [ft]
PUMPING/INJECTION RATE	=	1049760 [gpd]
TIME SINCE START PUMPING/INJECTION	=	36500 [day]

WELL NO. 7

X-COORDINATE = 1082021 [ft]
Y-COORDINATE = 1.217451E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 8

X-COORDINATE = 1079946 [ft]
Y-COORDINATE = 1.217707E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 9

X-COORDINATE = 1077187 [ft]
Y-COORDINATE = 1.217939E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 10

X-COORDINATE = 1087312 [ft]
Y-COORDINATE = 1.217673E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 11

X-COORDINATE = 1082592 [ft]
Y-COORDINATE = 1.217976E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 12

X-COORDINATE = 1084538 [ft]
Y-COORDINATE = 1.217125E+07 [ft]
PUMPING/INJECTION RATE = 1049760 [gpd]
TIME SINCE START PUMPING/INJECTION = 36500 [day]

WELL NO. 13

```
                    X-COORDINATE  =  1077255 [ft]
                    Y-COORDINATE  =  1.218508E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 14

```
                    X-COORDINATE  =  1072026 [ft]
                    Y-COORDINATE  =  1.218741E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 15

```
                    X-COORDINATE  =  1082574 [ft]
                    Y-COORDINATE  =  1.218456E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 16

```
                    X-COORDINATE  =  1092629 [ft]
                    Y-COORDINATE  =  1.216066E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 17

```
                    X-COORDINATE  =  1089640 [ft]
                    Y-COORDINATE  =  1.216564E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 18

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 19

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 20

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 21

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 22

```
                    X-COORDINATE  =  1095140 [ft]
                    Y-COORDINATE  =  1.220231E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 23

```
                    X-COORDINATE  =  1087528 [ft]
                    Y-COORDINATE  =  1.220951E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 24

```
                    X-COORDINATE  =  1090391 [ft]
                    Y-COORDINATE  =  1.220459E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 25

```
                    X-COORDINATE  =  1087295 [ft]
                    Y-COORDINATE  =  1.220347E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 26

```
                    X-COORDINATE  =  1083731 [ft]
                    Y-COORDINATE  =  1.220291E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 27

```
                    X-COORDINATE  =  1093778 [ft]
                    Y-COORDINATE  =  1.219996E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 28

```
                    X-COORDINATE  =  1088170 [ft]
                    Y-COORDINATE  =  1.21998E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 29

```
                    X-COORDINATE  =  1094230 [ft]
                    Y-COORDINATE  =  1.220608E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 30

```
                    X-COORDINATE  =  1080854 [ft]
                    Y-COORDINATE  =  1.219801E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 31

```
                    X-COORDINATE  =  1075170 [ft]
                    Y-COORDINATE  =  1.219871E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 32

```
                    X-COORDINATE  =  1085675 [ft]
                    Y-COORDINATE  =  1.21957E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 33

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 34

```
                    X-COORDINATE  =  0 [ft]
                    Y-COORDINATE  =  0 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 35

```
                    X-COORDINATE  =  1114889 [ft]
                    Y-COORDINATE  =  1.216949E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 36

```
                    X-COORDINATE  =  1107453 [ft]
                    Y-COORDINATE  =  1.217248E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 37

```
                    X-COORDINATE  =  1103067 [ft]
                    Y-COORDINATE  =  1.217555E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 38

```
                    X-COORDINATE  =  1101525 [ft]
                    Y-COORDINATE  =  1.217721E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 39

```
                    X-COORDINATE  =  1101021 [ft]
                    Y-COORDINATE  =  1.218193E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 40

```
                    X-COORDINATE  =  1108092 [ft]
                    Y-COORDINATE  =  1.218967E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 41

```
                    X-COORDINATE  =  1103219 [ft]
                    Y-COORDINATE  =  1.218672E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 42

```
                    X-COORDINATE  =  1102051 [ft]
                    Y-COORDINATE  =  1.21898E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 43

```
                    X-COORDINATE  =  1101424 [ft]
                    Y-COORDINATE  =  1.219335E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 44

```
                    X-COORDINATE  =  1098651 [ft]
                    Y-COORDINATE  =  1.218326E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 45

```
                    X-COORDINATE  =  1098397 [ft]
                    Y-COORDINATE  =  1.218886E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 46

```
                    X-COORDINATE  =  1104776 [ft]
                    Y-COORDINATE  =  1.218291E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 47

```
                    X-COORDINATE  =  1096474 [ft]
                    Y-COORDINATE  =  1.219615E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 48

```
                    X-COORDINATE  =  1097080 [ft]
                    Y-COORDINATE  =  1.220184E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 49

```
                    X-COORDINATE  =  1094252 [ft]
                    Y-COORDINATE  =  1.219129E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 50

```
                    X-COORDINATE  =  1109881 [ft]
                    Y-COORDINATE  =  1.217059E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 51

```
                    X-COORDINATE  =  1107071 [ft]
                    Y-COORDINATE  =  1.217568E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 52

```
                    X-COORDINATE  =  1084995 [ft]
                    Y-COORDINATE  =  1.214846E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 53

```
                    X-COORDINATE  =  1077403 [ft]
                    Y-COORDINATE  =  1.214588E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 54

```
                    X-COORDINATE  =  1072074 [ft]
                    Y-COORDINATE  =  1.214536E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 55

```
                    X-COORDINATE  =  1069823 [ft]
                    Y-COORDINATE  =  1.214561E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 56

```
                    X-COORDINATE  =  1066365 [ft]
                    Y-COORDINATE  =  1.214886E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 57

```
                    X-COORDINATE  =  1066689 [ft]
                    Y-COORDINATE  =  1.215934E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 58

```
                    X-COORDINATE  =  1064913 [ft]
                    Y-COORDINATE  =  1.215393E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 59

```
                    X-COORDINATE  =  1062022 [ft]
                    Y-COORDINATE  =  1.21555E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 60

```
                    X-COORDINATE  =  1059231 [ft]
                    Y-COORDINATE  =  1.215779E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```


WELL NO. 61

```
                    X-COORDINATE  =  1063706 [ft]
                    Y-COORDINATE  =  1.214832E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 62

```
                    X-COORDINATE  =  1059861 [ft]
                    Y-COORDINATE  =  1.215241E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 63

```
                    X-COORDINATE  =  1068578 [ft]
                    Y-COORDINATE  =  1.215205E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 64

```
                    X-COORDINATE  =  1053656 [ft]
                    Y-COORDINATE  =  1.215668E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 65

```
                    X-COORDINATE  =  1050405 [ft]
                    Y-COORDINATE  =  1.21614E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 66

```
                    X-COORDINATE  =  1055137 [ft]
                    Y-COORDINATE  =  1.215155E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 67

```
                    X-COORDINATE  =  1080475 [ft]
                    Y-COORDINATE  =  1.214603E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 68

```
                    X-COORDINATE  =  1075029 [ft]
                    Y-COORDINATE  =  1.214806E+07 [ft]
          PUMPING/INJECTION RATE  =  1049760 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 69

```
                    X-COORDINATE  =  1095112 [ft]
                    Y-COORDINATE  =  1.217124E+07 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 70

```
                    X-COORDINATE  =  1095112 [ft]
                    Y-COORDINATE  =  1.217256E+07 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 71

```
                    X-COORDINATE  =**1095060** [ft]
                    Y-COORDINATE  =  1.217133E+07 [ft]
          PUMPING/INJECTION RATE  =  0 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

Well identified as having the greatest impact

---------- Drawdown in [ft]

Y [ft]	<- X [ft] ->				
	1045072	1045732	1046392	1047052	1047712
%12153625.00	128.360	131.659	135.072	138.607	142.268
%12154285.00	129.216	132.560	136.022	139.608	143.324
%12154945.00	130.001	133.387	136.894	140.526	144.292
%12155605.00	130.713	134.138	137.685	141.360	145.169
%12156265.00	131.351	134.810	138.394	142.108	145.957
%12156925.00	131.910	135.400	139.019	142.770	146.656
%12157585.00	132.388	135.907	139.559	143.347	147.271
%12158245.00	132.781	136.326	140.009	143.836	147.806
%12158905.00	133.085	136.650	140.363	144.232	148.259
%12159565.00	133.294	136.872	140.609	144.519	148.614
%12160225.00	133.401	136.982	140.730	144.671	148.833
%12160885.00	133.403	136.970	140.710	144.654	148.850
%12161545.00	133.298	136.833	140.537	144.444	148.604
%12162205.00	133.090	136.574	140.214	144.037	148.082
%12162865.00	132.787	136.203	139.757	143.465	147.341
%12163525.00	132.400	135.739	139.195	142.771	146.469
%12164185.00	131.944	135.202	138.556	142.003	145.535
%12164845.00	131.433	134.609	137.865	141.194	144.584
%12165505.00	130.880	133.978	137.142	140.366	143.637
%12166165.00	130.293	133.319	136.401	139.533	142.703
%12166825.00	129.683	132.641	135.650	138.702	141.788
%12167485.00	129.054	131.952	134.894	137.876	140.890
%12168145.00	128.412	131.254	134.138	137.058	140.008
%12168805.00	127.760	130.551	133.382	136.247	139.143

%12169465.00	127.100	129.845	132.627	135.444	138.291
141.164					
%12170125.00	126.434	129.136	131.875	134.648	137.451
140.281					
%12170785.00	125.763	128.426	131.125	133.858	136.622
139.413					
%12171445.00	125.087	127.714	130.377	133.073	135.801
138.557					
%12172105.00	124.408	127.002	129.631	132.293	134.988
137.712					
%12172765.00	123.725	126.288	128.885	131.517	134.181
136.875					
%12173425.00	123.038	125.572	128.141	130.743	133.378
136.045					
%12174085.00	122.348	124.854	127.396	129.971	132.580
135.221					
%12174745.00	121.655	124.135	126.650	129.200	131.784
134.400					
%12175405.00	120.957	123.413	125.904	128.429	130.989
133.583					
%12176065.00	120.255	122.688	125.155	127.658	130.195
132.767					
%12176725.00	119.549	121.959	124.404	126.885	129.401
131.952					
%12177385.00	118.839	121.227	123.651	126.110	128.605
131.136					
%12178045.00	118.123	120.490	122.893	125.332	127.807
130.319					
%12178705.00	117.403	119.749	122.132	124.551	127.007
129.499					

Y [ft]	<- X [ft] ->				
	1045072	1045732	1046392	1047052	1047712
1048372					
%12179365.00	116.677	119.003	121.367	123.766	126.203
128.676					
%12180025.00	115.945	118.252	120.596	122.977	125.394
127.850					
%12180685.00	115.207	117.495	119.820	122.182	124.581
127.018					
%12181345.00	114.462	116.732	119.038	121.382	123.763
126.182					
%12182005.00	113.711	115.962	118.250	120.575	122.938
125.339					
%12182665.00	112.953	115.186	117.455	119.762	122.107
124.490					
%12183325.00	112.189	114.403	116.654	118.942	121.269
123.634					
%12183985.00	111.417	113.612	115.845	118.115	120.424
122.771					
%12184645.00	110.637	112.814	115.029	117.281	119.571
121.900					
%12185305.00	109.850	112.009	114.205	116.438	118.710
121.021					
%12185965.00	109.055	111.196	113.373	115.588	117.841
120.133					
%12186625.00	108.253	110.374	112.533	114.729	116.963
119.236					
%12187285.00	107.442	109.545	111.685	113.862	116.077
118.331					
%12187945.00	106.624	108.708	110.829	112.986	115.182
117.416					
%12188605.00	105.798	107.863	109.964	112.102	114.278
116.493					
%12189265.00	104.964	107.009	109.091	111.209	113.365
115.560					
%12189925.00	104.122	106.148	108.209	110.308	112.444
114.618					
%12190585.00	103.272	105.278	107.320	109.398	111.513
113.666					
%12191245.00	102.414	104.400	106.422	108.479	110.574
112.705					
%12191905.00	101.549	103.515	105.516	107.552	109.625
111.736					
%12192565.00	100.676	102.621	104.602	106.617	108.668
110.757					
%12193225.00	99.795	101.720	103.679	105.673	107.703
109.769					
%12193885.00	98.908	100.812	102.750	104.722	106.729
108.773					
%12194545.00	98.013	99.896	101.812	103.762	105.747
107.768					
%12195205.00	97.112	98.973	100.868	102.795	104.757
106.755					
%12195865.00	96.204	98.044	99.916	101.821	103.760

105.734					
%12196525.00	95.289	97.108	98.957	100.840	102.755
104.705					
%12197185.00	94.369	96.165	97.992	99.851	101.743
103.669					
%12197845.00	93.442	95.216	97.021	98.857	100.725
102.626					
%12198505.00	92.511	94.262	96.043	97.856	99.700
101.576					

Y [ft] <- X [ft] ->

	1049032	1049692	1050352	1051012	1051672
1052332					
%12153625.00	150.008	154.103	158.360	162.782	167.363
172.079					
%12154285.00	151.183	155.346	159.676	164.180	168.848
173.637					
%12154945.00	152.257	156.479	160.881	165.478	170.276
175.238					
%12155605.00	153.224	157.494	161.955	166.641	171.598
176.867					
%12156265.00	154.083	158.382	162.872	167.604	172.675
178.282					
%12156925.00	154.839	159.146	163.620	168.313	173.333
178.911					
%12157585.00	155.510	159.807	164.222	168.784	173.558
178.639					
%12158245.00	156.124	160.415	164.749	169.117	173.545
178.049					
%12158905.00	156.720	161.045	165.310	169.454	173.501
177.499					
%12159565.00	157.332	161.801	166.068	169.952	173.549
177.053					

Y [ft]	<- X [ft] ->				
	1049032	1049692	1050352	1051012	1051672
%12160225.00	157.950	162.824	167.334	170.804	173.709
%12160885.00	158.389	164.154	170.130	172.173	173.789
%12161545.00	158.173	164.383	174.557	172.420	173.188
%12162205.00	157.093	162.183	166.934	169.626	171.619
%12162865.00	155.621	159.870	163.767	166.958	169.683
%12163525.00	154.135	157.946	161.540	164.807	167.807
%12164185.00	152.742	156.303	159.734	162.989	166.085
%12164845.00	151.449	154.848	158.168	161.385	164.505
%12165505.00	150.240	153.522	156.757	159.931	163.043
%12166165.00	149.101	152.292	155.457	158.586	161.677
%12166825.00	148.016	151.134	154.239	157.324	160.389
%12167485.00	146.977	150.032	153.085	156.130	159.164
%12168145.00	145.975	148.977	151.983	154.989	157.994
%12168805.00	145.004	147.958	150.922	153.893	156.869
%12169465.00	144.058	146.971	149.897	152.835	155.783
%12170125.00	143.135	146.009	148.901	151.809	154.731
%12170785.00	142.230	145.070	147.930	150.810	153.706
%12171445.00	141.341	144.149	146.980	149.833	152.707
%12172105.00	140.465	143.244	146.048	148.877	151.728
%12172765.00	139.599	142.351	145.131	147.936	150.767
%12173425.00	138.743	141.470	144.226	147.010	149.821
%12174085.00	137.893	140.597	143.331	146.095	148.888
%12174745.00	137.050	139.731	142.444	145.189	147.964
%12175405.00	136.210	138.870	141.564	144.290	147.048
%12176065.00	135.373	138.013	140.688	143.396	146.138
%12176725.00	134.538	137.158	139.814	142.506	145.232

147.995					
%12177385.00	133.702	136.305	138.943	141.617	144.329
147.077					
%12178045.00	132.866	135.450	138.071	140.730	143.426
146.160					
%12178705.00	132.028	134.594	137.199	139.841	142.522
145.243					
%12179365.00	131.187	133.736	136.324	138.950	141.616
144.323					
%12180025.00	130.343	132.875	135.445	138.056	140.707
143.400					
%12180685.00	129.494	132.009	134.563	137.158	139.794
142.472					
%12181345.00	128.640	131.137	133.675	136.254	138.875
141.539					
%12182005.00	127.780	130.260	132.781	135.344	137.949
140.598					
%12182665.00	126.913	129.376	131.880	134.427	137.016
139.650					
%12183325.00	126.040	128.485	130.972	133.502	136.075
138.693					
%12183985.00	125.158	127.586	130.056	132.569	135.125
137.727					
%12184645.00	124.269	126.679	129.131	131.626	134.166
136.750					
%12185305.00	123.371	125.763	128.197	130.674	133.196
135.763					
%12185965.00	122.465	124.838	127.254	129.713	132.216
134.765					

Y [ft]	<- X [ft] ->				
	1049032	1049692	1050352	1051012	1051672
%12186625.00	121.550	123.904	126.301	128.740	131.225
%12187285.00	120.625	122.960	125.337	127.758	130.223
%12187945.00	119.691	122.006	124.364	126.764	129.209
%12188605.00	118.747	121.042	123.379	125.760	128.184
%12189265.00	117.794	120.068	122.385	124.744	127.147
%12189925.00	116.831	119.084	121.379	123.717	126.098
%12190585.00	115.858	118.090	120.364	122.679	125.038
%12191245.00	114.876	117.086	119.337	121.630	123.966
%12191905.00	113.884	116.072	118.300	120.570	122.882
%12192565.00	112.883	115.048	117.253	119.499	121.787
%12193225.00	111.872	114.014	116.196	118.417	120.681
%12193885.00	110.853	112.971	115.128	117.326	119.564
%12194545.00	109.825	111.919	114.051	116.224	118.436
%12195205.00	108.788	110.857	112.965	115.112	117.298
%12195865.00	107.742	109.788	111.870	113.991	116.150
%12196525.00	106.689	108.709	110.766	112.860	114.993
%12197185.00	105.628	107.623	109.654	111.721	113.827
%12197845.00	104.560	106.529	108.533	110.574	112.651
%12198505.00	103.485	105.428	107.406	109.419	111.468

Y [ft]	<- X [ft] ->				
	1052992	1053652	1054312	1054972	1055632
%12153625.00	176.880	181.686	186.384	190.839	194.980
%12154285.00	178.448	183.139	187.592	191.795	195.825
%12154945.00	180.219	184.924	189.134	192.995	196.778

%12155605.00	182.352	187.369	191.102	194.304	197.682
201.374					
%12156265.00	184.851	191.859	193.468	195.398	198.312
201.839					
%12156925.00	185.680	194.459	194.095	195.622	198.411
201.905					
%12157585.00	184.029	188.937	192.122	194.814	197.902
201.491					
%12158245.00	182.534	186.688	190.274	193.562	196.943
200.622					
%12158905.00	181.431	185.207	188.775	192.226	195.725
199.407					
%12159565.00	180.548	184.023	187.459	190.887	194.371
197.977					
%12160225.00	179.736	182.939	186.212	189.544	192.947
196.439					
%12160885.00	178.859	181.838	184.961	188.182	191.485
194.859					
%12161545.00	177.801	180.648	183.664	186.792	190.003
193.275					
%12162205.00	176.523	179.341	182.306	185.372	188.512
191.703					
%12162865.00	175.081	177.938	180.894	183.928	187.020
190.153					
%12163525.00	173.565	176.482	179.453	182.475	185.538
188.631					
%12164185.00	172.047	175.015	178.007	181.027	184.074
187.142					
%12164845.00	170.567	173.569	176.577	179.600	182.638
185.690					
%12165505.00	169.141	172.160	175.179	178.203	181.236
184.278					
%12166165.00	167.774	170.799	173.820	176.844	179.874
182.909					
%12166825.00	166.464	169.486	172.505	175.526	178.552
181.582					

Y [ft]	<- X [ft] ->				
	1052992	1053652	1054312	1054972	1055632
1056292					
%12167485.00	165.206	168.220	171.234	174.250	177.271
180.298					
%12168145.00	163.998	167.000	170.005	173.015	176.032
179.055					
%12168805.00	162.832	165.821	168.816	171.819	174.831
177.851					
%12169465.00	161.705	164.680	167.664	170.659	173.666
176.684					
%12170125.00	160.612	163.572	166.546	169.533	172.534
175.550					
%12170785.00	159.549	162.495	165.458	168.437	171.433
174.447					
%12171445.00	158.513	161.445	164.396	167.367	170.359
173.371					
%12172105.00	157.499	160.417	163.358	166.322	169.308
172.319					
%12172765.00	156.504	159.410	162.340	165.296	168.278
171.287					
%12173425.00	155.526	158.419	161.340	164.289	167.266
170.273					
%12174085.00	154.562	157.443	160.354	163.296	166.268
169.273					
%12174745.00	153.609	156.478	159.380	162.315	165.283
168.285					
%12175405.00	152.665	155.523	158.415	161.343	164.306
167.306					
%12176065.00	151.727	154.574	157.457	160.378	163.336
166.333					
%12176725.00	150.794	153.630	156.504	159.417	162.370
165.364					
%12177385.00	149.864	152.689	155.553	158.459	161.406
164.396					
%12178045.00	148.934	151.748	154.603	157.500	160.441
163.427					
%12178705.00	148.004	150.807	153.652	156.541	159.475
162.456					
%12179365.00	147.072	149.863	152.698	155.578	158.504
161.479					
%12180025.00	146.136	148.915	151.739	154.609	157.528
160.496					
%12180685.00	145.194	147.961	150.774	153.634	156.544
159.505					
%12181345.00	144.247	147.001	149.802	152.651	155.551
158.503					
%12182005.00	143.292	146.033	148.821	151.659	154.548
157.491					
%12182665.00	142.329	145.056	147.831	150.656	153.534
156.465					
%12183325.00	141.357	144.069	146.830	149.642	152.507
155.426					
%12183985.00	140.375	143.071	145.817	148.615	151.466

154.373					
%12184645.00	139.382	142.062	144.792	147.575	150.411
153.303					
%12185305.00	138.378	141.041	143.755	146.521	149.341
152.218					
%12185965.00	137.362	140.007	142.703	145.452	148.255
151.115					
%12186625.00	136.333	138.960	141.638	144.368	147.153
149.995					
%12187285.00	135.292	137.900	140.558	143.269	146.034
148.856					
%12187945.00	134.238	136.826	139.463	142.154	144.899
147.700					
%12188605.00	133.172	135.738	138.354	141.023	143.746
146.526					
%12189265.00	132.091	134.636	137.230	139.876	142.577
145.333					
%12189925.00	130.998	133.520	136.091	138.714	141.390
144.122					
%12190585.00	129.892	132.390	134.937	137.536	140.187
142.893					
%12191245.00	128.773	131.246	133.769	136.342	138.967
141.647					
%12191905.00	127.640	130.089	132.586	135.133	137.731
140.384					
%12192565.00	126.496	128.918	131.389	133.909	136.480
139.103					
%12193225.00	125.338	127.735	130.178	132.670	135.212
137.807					

```
  Y [ft]                                <- X [ft] ->
-------------------------------------------------------------------------
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                1052992     1053652     1054312     1054972     1055632
1056292
%12193885.00    124.169     126.538     128.954     131.417     133.930
136.494
%12194545.00    122.988     125.330     127.717     130.151     132.634
135.167
%12195205.00    121.796     124.109     126.467     128.871     131.323
133.824
%12195865.00    120.592     122.877     125.205     127.579     129.999
132.468
%12196525.00    119.379     121.634     123.932     126.275     128.663
131.098
%12197185.00    118.155     120.380     122.648     124.959     127.314
129.716
%12197845.00    116.922     119.117     121.353     123.632     125.954
128.322
%12198505.00    115.679     117.844     120.048     122.294     124.583
126.916

  Y [ft]                                <- X [ft] ->
-------------------------------------------------------------------------
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                1056952     1057612     1058272     1058932     1059592
1060252
%12153625.00    202.933     207.187     211.796     216.735     221.615
225.615
%12154285.00    203.885     208.147     212.619     217.223     221.761
226.036
%12154945.00    204.703     208.951     213.362     217.843     222.300
226.764
%12155605.00    205.376     209.650     214.104     218.580     222.951
227.326
%12156265.00    205.834     210.224     214.895     219.541     223.733
227.548
%12156925.00    205.957     210.558     215.740     221.145     225.058
227.596
%12157585.00    205.606     210.366     216.155     224.470     227.663
227.221
%12158245.00    204.711     209.346     214.800     221.414     224.742
225.335
%12158905.00    203.361     207.641     212.223     216.714     220.105
222.417
%12159565.00    201.744     205.666     209.648     213.446     216.757
219.562
%12160225.00    200.024     203.673     207.308     210.803     214.039
216.998
%12160885.00    198.291     201.747     205.175     208.505     211.681
214.688
%12161545.00    196.586     199.908     203.203     206.430     209.558
212.576
%12162205.00    194.924     198.151     201.357     204.515     207.607
210.622
```

%12162865.00	193.309	196.469	199.614	202.725	205.789	208.798
%12163525.00	191.742	194.855	197.958	201.037	204.081	207.084
%12164185.00	190.222	193.304	196.378	199.435	202.467	205.467
%12164845.00	188.750	191.812	194.868	197.911	200.936	203.938
%12165505.00	187.325	190.374	193.419	196.456	199.480	202.486
%12166165.00	185.948	188.989	192.029	195.064	198.091	201.105
%12166825.00	184.617	187.655	190.693	193.730	196.763	199.789
%12167485.00	183.330	186.367	189.408	192.450	195.492	198.532
%12168145.00	182.086	185.124	188.168	191.218	194.271	197.327
%12168805.00	180.882	183.922	186.972	190.030	193.097	196.170
%12169465.00	179.715	182.758	185.814	188.883	191.963	195.056
%12170125.00	178.582	181.629	184.692	187.771	190.867	193.978
%12170785.00	177.480	180.531	183.601	186.692	189.802	192.933
%12171445.00	176.405	179.460	182.538	185.640	188.765	191.916
%12172105.00	175.353	178.413	181.499	184.612	187.752	190.922
%12172765.00	174.323	177.387	180.480	183.604	186.759	189.947
%12173425.00	173.310	176.378	179.478	182.612	185.781	188.987
%12174085.00	172.311	175.383	178.490	181.634	184.816	188.039

Y [ft]	<- X [ft] ->				
	1056952	1057612	1058272	1058932	1059592
1060252					
%12174745.00	171.323	174.398	177.511	180.665	183.859
187.097					
%12175405.00	170.344	173.422	176.540	179.702	182.908
186.161					
%12176065.00	169.371	172.450	175.574	178.742	181.959
185.225					
%12176725.00	168.400	171.481	174.608	177.783	181.009
184.286					
%12177385.00	167.431	170.512	173.642	176.822	180.055
183.343					
%12178045.00	166.460	169.541	172.672	175.856	179.096
182.393					
%12178705.00	165.485	168.564	171.697	174.883	178.128
181.432					
%12179365.00	164.504	167.581	170.713	173.901	177.149
180.459					
%12180025.00	163.516	166.590	169.719	172.908	176.157
179.471					
%12180685.00	162.518	165.587	168.714	171.900	175.150
178.466					
%12181345.00	161.509	164.572	167.694	170.878	174.126
177.442					
%12182005.00	160.488	163.544	166.660	169.839	173.084
176.398					
%12182665.00	159.453	162.500	165.609	168.781	172.021
175.332					
%12183325.00	158.403	161.440	164.539	167.703	170.936
174.241					
%12183985.00	157.337	160.362	163.450	166.605	169.828
173.125					
%12184645.00	156.254	159.266	162.341	165.484	168.696
171.982					
%12185305.00	155.153	158.150	161.211	164.340	167.539
170.812					
%12185965.00	154.034	157.014	160.059	163.172	166.355
169.613					
%12186625.00	152.895	155.858	158.885	161.980	165.145
168.386					
%12187285.00	151.738	154.681	157.688	160.763	163.909
167.129					
%12187945.00	150.560	153.482	156.468	159.522	162.645
165.842					
%12188605.00	149.364	152.263	155.226	158.255	161.354
164.527					
%12189265.00	148.147	151.022	153.960	156.965	160.038
163.183					
%12189925.00	146.912	149.761	152.673	155.650	158.695
161.811					
%12190585.00	145.657	148.479	151.364	154.312	157.327
160.413					
%12191245.00	144.383	147.178	150.033	152.951	155.935

158.988
%12191905.00 143.091 145.856 148.681 151.569 154.520
157.539
%12192565.00 141.782 144.516 147.310 150.165 153.082
156.066
%12193225.00 140.455 143.158 145.919 148.740 151.623
154.570
%12193885.00 139.111 141.782 144.510 147.296 150.143
153.053
%12194545.00 137.751 140.389 143.083 145.834 148.644
151.516
%12195205.00 136.376 138.980 141.639 144.354 147.126
149.958
%12195865.00 134.986 137.556 140.179 142.856 145.590
148.383
%12196525.00 133.583 136.117 138.703 141.343 144.038
146.790
%12197185.00 132.165 134.664 137.213 139.814 142.469
145.180
%12197845.00 130.736 133.197 135.709 138.271 140.885
143.554
%12198505.00 129.294 131.719 134.191 136.714 139.287
141.914

Y [ft] <- X [ft] ->

1060912 1061572 1062232 1062892 1063552
1064212
%12153625.00 228.778 231.735 234.593 237.419 240.619
244.967
%12154285.00 230.089 233.955 237.117 239.498 242.128
245.980
%12154945.00 231.517 236.973 240.805 241.269 242.537
244.671

Y [ft]	<- X [ft] ->				
	1060912	1061572	1062232	1062892	1063552
1064212					
%12155605.00	232.212	239.142	245.272	241.716	242.038
243.314					
%12156265.00	231.540	235.922	239.008	239.858	240.741
241.987					
%12156925.00	230.312	233.221	235.707	237.518	239.074
240.649					
%12157585.00	228.843	231.064	233.321	235.406	237.376
239.338					
%12158245.00	226.904	228.977	231.209	233.457	235.714
238.035					
%12158905.00	224.557	226.810	229.156	231.560	234.033
236.643					
%12159565.00	222.113	224.603	227.106	229.651	232.276
235.054					
%12160225.00	219.762	222.429	225.067	227.720	230.429
233.248					
%12160885.00	217.555	220.333	223.065	225.788	228.530
231.317					
%12161545.00	215.494	218.335	221.126	223.888	226.638
229.379					
%12162205.00	213.563	216.440	219.267	222.054	224.805
227.516					
%12162865.00	211.750	214.648	217.499	220.304	223.064
225.767					
%12163525.00	210.043	212.957	215.826	218.651	221.427
224.144					
%12164185.00	208.433	211.361	214.250	217.097	219.898
222.645					
%12164845.00	206.912	209.855	212.766	215.640	218.473
221.259					
%12165505.00	205.471	208.433	211.368	214.273	217.145
219.978					
%12166165.00	204.105	207.088	210.050	212.990	215.904
218.790					
%12166825.00	202.806	205.812	208.805	211.782	214.742
217.682					
%12167485.00	201.569	204.600	207.625	210.642	213.649
216.646					
%12168145.00	200.385	203.444	206.503	209.561	212.617
215.672					
%12168805.00	199.251	202.338	205.432	208.531	211.637
214.749					
%12169465.00	198.160	201.277	204.405	207.546	210.701
213.870					
%12170125.00	197.107	200.253	203.417	206.599	209.802
213.027					
%12170785.00	196.086	199.261	202.460	205.683	208.934
212.213					
%12171445.00	195.093	198.297	201.529	204.793	208.089
211.420					
%12172105.00	194.122	197.354	200.620	203.921	207.262

210.643					
%12172765.00	193.170	196.429	199.726	203.065	206.447
209.876					
%12173425.00	192.232	195.516	198.844	202.218	205.640
209.114					
%12174085.00	191.303	194.613	197.969	201.376	204.835
208.352					
%12174745.00	190.382	193.714	197.097	200.534	204.029
207.585					
%12175405.00	189.463	192.816	196.224	199.690	203.218
206.811					
%12176065.00	188.543	191.916	195.347	198.840	202.397
206.024					
%12176725.00	187.620	191.011	194.463	197.980	201.565
205.223					
%12177385.00	186.690	190.097	193.568	197.107	200.717
204.403					
%12178045.00	185.750	189.172	192.660	196.218	199.851
203.563					
%12178705.00	184.799	188.233	191.736	195.312	198.965
202.699					
%12179365.00	183.834	187.278	190.793	194.384	198.055
201.810					
%12180025.00	182.852	186.304	189.830	193.434	197.120
200.893					
%12180685.00	181.851	185.309	188.844	192.458	196.158
199.946					
%12181345.00	180.830	184.292	187.832	191.455	195.165
198.967					

Y [ft]	<- X [ft] ->				
	1060912	1061572	1062232	1062892	1063552
1064212					
%12182005.00	179.785	183.249	186.793	190.422	194.140
197.952					
%12182665.00	178.716	182.179	185.725	189.357	193.081
196.901					
%12183325.00	177.621	181.081	184.625	188.258	191.984
195.809					
%12183985.00	176.498	179.952	183.492	187.122	190.848
194.675					
%12184645.00	175.346	178.792	182.324	185.948	189.669
193.494					
%12185305.00	174.164	177.598	181.119	184.733	188.447
192.265					
%12185965.00	172.950	176.369	179.877	183.477	187.178
190.985					
%12186625.00	171.704	175.106	178.596	182.179	185.862
189.652					
%12187285.00	170.427	173.808	177.276	180.837	184.498
188.265					
%12187945.00	169.117	172.474	175.918	179.453	183.086
186.824					
%12188605.00	167.776	171.106	174.521	178.027	181.628
185.332					
%12189265.00	166.404	169.704	173.088	176.561	180.126
183.791					
%12189925.00	165.002	168.270	171.620	175.056	178.583
182.204					
%12190585.00	163.571	166.805	170.119	173.516	177.001
180.577					
%12191245.00	162.112	165.311	168.586	171.943	175.384
178.912					
%12191905.00	160.627	163.788	167.024	170.339	173.734
177.214					
%12192565.00	159.117	162.239	165.435	168.706	172.056
175.486					
%12193225.00	157.584	160.666	163.820	167.047	170.350
173.731					
%12193885.00	156.028	159.069	162.181	165.363	168.620
171.952					
%12194545.00	154.450	157.451	160.519	163.657	166.866
170.150					
%12195205.00	152.853	155.811	158.835	161.928	165.090
168.325					
%12195865.00	151.236	154.152	157.132	160.178	163.293
166.479					
%12196525.00	149.601	152.473	155.408	158.408	161.476
164.613					
%12197185.00	147.949	150.777	153.666	156.619	159.638
162.725					
%12197845.00	146.279	149.063	151.906	154.811	157.781
160.818					
%12198505.00	144.595	147.332	150.128	152.985	155.905

158.890

Y [ft]	<- X [ft] ->				
	1064872	1065532	1066192	1066852	1067512
1068172					
%12153625.00	251.032	248.619	247.139	246.954	247.313
247.703					
%12154285.00	251.141	249.059	247.442	246.970	246.949
246.984					
%12154945.00	246.612	247.038	246.765	246.600	246.571
246.539					
%12155605.00	244.631	245.476	245.891	246.111	246.231
246.253					
%12156265.00	243.292	244.398	245.208	245.734	246.018
246.112					
%12156925.00	242.223	243.667	244.839	245.630	246.026
246.134					
%12157585.00	241.318	243.244	244.903	245.973	246.355
246.327					
%12158245.00	240.486	243.093	245.627	247.128	247.109
246.631					
%12158905.00	239.518	242.917	247.349	250.389	248.129
246.779					
%12159565.00	238.126	241.814	247.120	251.958	247.723
246.261					
%12160225.00	236.254	239.530	242.942	245.132	245.219
244.958					
%12160885.00	234.159	237.004	239.627	241.578	242.689
243.357					
%12161545.00	232.090	234.706	237.088	239.071	240.607
241.822					
%12162205.00	230.160	232.687	235.022	237.097	238.892
240.461					

Y [ft]	<- X [ft] ->				
	1064872	1065532	1066192	1066852	1067512
1068172					
%12162865.00	228.394	230.911	233.277	235.459	237.452
239.280					
%12163525.00	226.788	229.336	231.766	234.062	236.222
238.259					
%12164185.00	225.326	227.928	230.438	232.848	235.159
237.378					
%12164845.00	223.991	226.660	229.258	231.781	234.232
236.614					
%12165505.00	222.768	225.510	228.199	230.835	233.417
235.952					
%12166165.00	221.643	224.461	227.243	229.987	232.697
235.375					
%12166825.00	220.602	223.498	226.372	229.223	232.055
234.870					
%12167485.00	219.633	222.607	225.572	228.528	231.477
234.425					
%12168145.00	218.725	221.778	224.831	227.888	230.952
234.026					
%12168805.00	217.869	220.998	224.139	227.294	230.467
233.664					
%12169465.00	217.055	220.259	223.484	226.734	230.012
233.326					
%12170125.00	216.276	219.552	222.858	226.198	229.578
233.004					
%12170785.00	215.523	218.868	222.252	225.680	229.156
232.687					
%12171445.00	214.790	218.201	221.660	225.169	228.736
232.367					
%12172105.00	214.069	217.544	221.072	224.660	228.312
232.036					
%12172765.00	213.356	216.890	220.485	224.145	227.877
231.688					
%12173425.00	212.644	216.235	219.891	223.619	227.425
231.316					
%12174085.00	211.929	215.572	219.286	223.077	226.952
230.917					
%12174745.00	211.207	214.899	218.666	222.515	226.453
230.486					
%12175405.00	210.473	214.210	218.027	221.929	225.924
230.020					
%12176065.00	209.724	213.502	217.364	221.316	225.364
229.516					
%12176725.00	208.957	212.773	216.676	220.673	224.769
228.971					
%12177385.00	208.169	212.020	215.960	219.997	224.136
228.384					
%12178045.00	207.357	211.239	215.214	219.287	223.465
227.754					
%12178705.00	206.519	210.429	214.435	218.541	222.754
227.079					
%12179365.00	205.653	209.589	213.622	217.758	222.002

226.360					
%12180025.00	204.757	208.715	212.774	216.937	221.210
225.597					
%12180685.00	203.828	207.807	211.889	216.077	220.376
224.791					
%12181345.00	202.864	206.862	210.965	215.176	219.501
223.942					
%12182005.00	201.863	205.878	210.000	214.234	218.584
223.052					
%12182665.00	200.823	204.851	208.992	213.248	217.624
222.122					
%12183325.00	199.739	203.780	207.936	212.214	216.617
221.148					
%12183985.00	198.610	202.659	206.829	211.127	215.558
220.127					
%12184645.00	197.430	201.484	205.665	209.980	214.439
219.048					
%12185305.00	196.197	200.251	204.436	208.763	213.245
217.895					
%12185965.00	194.907	198.953	203.135	207.466	211.962
216.644					
%12186625.00	193.557	197.588	201.756	206.078	210.573
215.267					
%12187285.00	192.146	196.153	200.296	204.593	209.065
213.741					
%12187945.00	190.675	194.648	198.755	203.010	207.435
212.054					
%12188605.00	189.145	193.076	197.135	201.334	205.690
210.221					

Y [ft]	<- X [ft] ->					
	1064872	1065532	1066192	1066852	1067512	1068172
%12189265.00	187.561	191.443	195.445	199.576	203.848	208.271
%12189925.00	185.926	189.754	193.694	197.751	201.931	206.238
%12190585.00	184.248	188.019	191.893	195.873	199.961	204.157
%12191245.00	182.531	186.243	190.051	193.956	197.957	202.050
%12191905.00	180.780	184.434	188.177	192.010	195.931	199.933
%12192565.00	178.999	182.596	186.278	190.043	193.891	197.814
%12193225.00	177.192	180.734	184.356	188.060	191.841	195.697
%12193885.00	175.361	178.849	182.416	186.061	189.783	193.580
%12194545.00	173.508	176.944	180.457	184.048	187.716	191.461
%12195205.00	171.634	175.018	178.479	182.019	185.637	189.334
%12195865.00	169.738	173.072	176.482	179.972	183.541	187.194
%12196525.00	167.822	171.104	174.464	177.903	181.425	185.033
%12197185.00	165.883	169.115	172.423	175.812	179.284	182.846
%12197845.00	163.924	167.103	170.358	173.694	177.115	180.626
%12198505.00	161.943	165.068	168.269	171.549	174.914	178.370

Y [ft]	<- X [ft] ->					
	1068832	1069492	1070152	1070812	1071472	1072132
%12153625.00	247.580	246.821	245.814	244.866	244.068	243.420
%12154285.00	246.811	246.355	245.728	245.074	244.475	243.962
%12154945.00	246.391	246.093	245.688	245.245	244.822	244.448
%12155605.00	246.163	245.971	245.709	245.423	245.147	244.905
%12156265.00	246.072	245.948	245.784	245.615	245.464	245.347
%12156925.00	246.090	245.992	245.892	245.816	245.776	245.778
%12157585.00	246.185	246.064	246.003	246.009	246.076	246.197

%12158245.00	246.272	246.099	246.077	246.170	246.350
246.599					
%12158905.00	246.194	246.012	246.066	246.273	246.586
246.976					
%12159565.00	245.771	245.729	245.938	246.304	246.777
247.327					
%12160225.00	244.972	245.240	245.687	246.260	246.924
247.654					
%12160885.00	243.951	244.605	245.343	246.158	247.036
247.964					
%12161545.00	242.887	243.913	244.953	246.025	247.130
248.267					
%12162205.00	241.885	243.236	244.562	245.888	247.226
248.578					
%12162865.00	240.986	242.615	244.203	245.774	247.340
248.909					
%12163525.00	240.199	242.070	243.896	245.698	247.487
249.271					
%12164185.00	239.520	241.605	243.651	245.671	247.676
249.673					
%12164845.00	238.940	241.221	243.470	245.698	247.913
250.121					
%12165505.00	238.446	240.910	243.351	245.779	248.199
250.616					
%12166165.00	238.029	240.665	243.290	245.911	248.533
251.158					
%12166825.00	237.676	240.476	243.279	246.088	248.909
251.745					
%12167485.00	237.375	240.335	243.309	246.303	249.322
252.368					
%12168145.00	237.117	240.230	243.371	246.546	249.761
253.019					
%12168805.00	236.889	240.149	243.452	246.804	250.213
253.684					
%12169465.00	236.680	240.083	243.541	247.065	250.662
254.343					

Y [ft]	<- X [ft] ->				
	1068832	1069492	1070152	1070812	1071472
1072132					
%12170125.00	236.481	240.019	243.626	247.313	251.091
254.976					
%12170785.00	236.280	239.946	243.693	247.534	251.483
255.558					
%12171445.00	236.070	239.854	243.732	247.715	251.820
256.067					
%12172105.00	235.841	239.736	243.733	247.846	252.090
256.488					
%12172765.00	235.587	239.584	243.690	247.919	252.286
256.811					
%12173425.00	235.302	239.392	243.597	247.929	252.404
257.039					
%12174085.00	234.982	239.157	243.451	247.877	252.447
257.176					
%12174745.00	234.624	238.875	243.250	247.760	252.417
257.231					
%12175405.00	234.224	238.545	242.993	247.580	252.315
257.210					
%12176065.00	233.779	238.163	242.678	247.335	252.143
257.115					
%12176725.00	233.288	237.729	242.304	247.023	251.898
256.943					
%12177385.00	232.749	237.241	241.868	246.642	251.577
256.687					
%12178045.00	232.162	236.697	241.369	246.191	251.175
256.340					
%12178705.00	231.524	236.097	240.807	245.666	250.689
255.893					
%12179365.00	230.838	235.443	240.183	245.070	250.117
255.344					
%12180025.00	230.104	234.736	239.501	244.407	249.466
254.695					
%12180685.00	229.324	233.980	238.764	243.683	248.743
253.959					
%12181345.00	228.501	233.181	237.983	242.909	247.964
253.155					
%12182005.00	227.639	232.344	237.165	242.100	247.147
252.308					
%12182665.00	226.740	231.476	236.323	241.271	246.312
251.441					
%12183325.00	225.805	230.583	235.468	240.442	245.486
250.584					
%12183985.00	224.832	229.667	234.612	239.638	244.702
249.773					
%12184645.00	223.812	228.725	233.767	238.888	244.013
249.062					
%12185305.00	222.725	227.740	232.928	238.230	243.503
248.557					
%12185965.00	221.537	226.668	232.060	237.683	243.331
248.485					
%12186625.00	220.200	225.428	231.037	237.152	243.770

249.494					
%12187285.00	218.665	223.913	229.622	236.105	244.406
255.374					
%12187945.00	216.910	222.065	227.627	233.803	240.907
247.193					
%12188605.00	214.955	219.926	225.169	230.691	236.287
241.191					
%12189265.00	212.856	217.610	222.521	227.524	232.439
236.981					
%12189925.00	210.673	215.224	219.864	224.526	229.103
233.470					
%12190585.00	208.453	212.834	217.269	221.710	226.090
230.346					
%12191245.00	206.226	210.470	214.754	219.044	223.298
227.478					
%12191905.00	204.009	208.144	212.316	216.501	220.670
224.797					
%12192565.00	201.807	205.856	209.946	214.057	218.169
222.262					
%12193225.00	199.621	203.603	207.631	211.691	215.767
219.843					
%12193885.00	197.447	201.376	205.359	209.387	213.445
217.520					
%12194545.00	195.279	199.166	203.118	207.126	211.182
215.273					
%12195205.00	193.110	196.963	200.892	204.893	208.960
213.085					
%12195865.00	190.930	194.753	198.665	202.666	206.756
210.932					

Y [ft]	<- X [ft] ->					
	1068832	1069492	1070152	1070812	1071472	1072132
%12196525.00	188.731	192.525	196.419	200.422	204.541	208.781
%12197185.00	186.503	190.263	194.136	198.136	202.280	206.587
%12197845.00	184.237	187.957	191.799	195.781	199.932	204.287
%12198505.00	181.927	185.596	189.392	193.336	197.460	201.812

Y [ft]	<- X [ft] ->					
	1072792	1073452	1074112	1074772	1075432	1076092
%12153625.00	242.894	242.454	242.068	241.710	241.358	240.996
%12154285.00	243.531	243.168	242.853	242.568	242.296	242.026
%12154945.00	244.130	243.864	243.640	243.445	243.266	243.094
%12155605.00	244.706	244.549	244.429	244.336	244.261	244.195
%12156265.00	245.268	245.228	245.220	245.240	245.277	245.326
%12156925.00	245.822	245.903	246.017	246.156	246.315	246.485
%12157585.00	246.366	246.576	246.818	247.086	247.373	247.671
%12158245.00	246.901	247.246	247.625	248.029	248.451	248.884
%12158905.00	247.423	247.914	248.438	248.986	249.551	250.126
%12159565.00	247.933	248.581	249.260	249.960	250.675	251.398
%12160225.00	248.434	249.250	250.092	250.953	251.826	252.703
%12160885.00	248.929	249.924	250.940	251.969	253.006	254.045
%12161545.00	249.430	250.612	251.809	253.014	254.222	255.427
%12162205.00	249.944	251.321	252.706	254.093	255.478	256.856
%12162865.00	250.482	252.059	253.637	255.212	256.780	258.337
%12163525.00	251.054	252.834	254.610	256.379	258.136	259.876
%12164185.00	251.666	253.653	255.632	257.600	259.552	261.482
%12164845.00	252.324	254.521	256.708	258.882	261.036	263.162

%12165505.00	253.031	255.442	257.845	260.232	262.596
264.927					
%12166165.00	253.788	256.419	259.045	261.657	264.242
266.787					
%12166825.00	254.594	257.452	260.313	263.161	265.983
268.757					
%12167485.00	255.442	258.538	261.647	264.753	267.832
270.855					
%12168145.00	256.323	259.668	263.045	266.433	269.802
273.106					
%12168805.00	257.222	260.828	264.495	268.202	271.909
275.546					
%12169465.00	258.118	261.994	265.973	270.044	274.163
278.228					
%12170125.00	258.982	263.129	267.436	271.915	276.549
281.226					
%12170785.00	259.782	264.185	268.809	273.711	278.964
284.585					
%12171445.00	260.485	265.110	270.003	275.264	281.085
287.916					
%12172105.00	261.067	265.866	270.945	276.407	282.447
289.524					
%12172765.00	261.520	266.443	271.625	277.128	283.028
289.352					
%12173425.00	261.851	266.863	272.097	277.570	283.270
289.083					
%12174085.00	262.076	267.160	272.435	277.890	283.485
289.117					
%12174745.00	262.213	267.368	272.695	278.176	283.769
289.405					
%12175405.00	262.272	267.507	272.908	278.460	284.128
289.863					
%12176065.00	262.259	267.581	273.080	278.743	284.542
290.434					
%12176725.00	262.169	267.586	273.202	279.011	284.991
291.091					

Y [ft]	<- X [ft] ->				
	1072792	1073452	1074112	1074772	1075432
%12177385.00	261.990	267.503	273.245	279.230	285.450
%12178045.00	261.708	267.305	273.168	279.339	285.863
%12178705.00	261.306	266.960	272.909	279.233	286.063
%12179365.00	260.774	266.446	272.417	278.782	285.730
%12180025.00	260.115	265.759	271.675	277.934	284.661
%12180685.00	259.345	264.926	270.727	276.780	283.103
%12181345.00	258.493	263.990	269.655	275.486	281.441
%12182005.00	257.589	262.997	268.535	274.186	279.891
%12182665.00	256.663	261.984	267.414	272.943	278.524
%12183325.00	255.740	260.969	266.300	271.757	277.329
%12183985.00	254.845	259.955	265.168	270.560	276.203
%12184645.00	254.016	258.942	263.964	269.224	274.896
%12185305.00	253.317	257.930	262.629	267.608	273.064
%12185965.00	252.859	256.910	261.107	265.643	270.610
%12186625.00	252.749	255.767	259.319	263.351	267.763
%12187285.00	252.310	254.092	257.131	260.772	264.754
%12187945.00	249.166	251.437	254.464	257.946	261.684
%12188605.00	244.883	248.114	251.442	254.956	258.605
%12189265.00	241.010	244.703	248.301	251.915	255.564
%12189925.00	237.569	241.451	245.212	248.920	252.604
%12190585.00	234.447	238.403	242.253	246.031	249.757
%12191245.00	231.562	235.548	239.447	243.275	247.043
%12191905.00	228.864	232.863	236.795	240.661	244.467
%12192565.00	226.319	230.330	234.288	238.189	242.032
%12193225.00	223.902	227.931	231.918	235.854	239.734
%12193885.00	221.595	225.654	229.679	233.655	237.573

241.430					
%12194545.00	219.382	223.488	227.566	231.592	235.549
239.436					
%12195205.00	217.250	221.429	225.584	229.676	233.673
237.575					
%12195865.00	215.179	219.469	223.745	227.934	231.972
235.856					
%12196525.00	213.141	217.596	222.073	226.429	230.510
234.301					
%12197185.00	211.081	215.770	220.593	225.300	229.443
232.949					
%12197845.00	208.903	213.864	219.259	224.888	229.199
231.793					
%12198505.00	206.475	211.604	217.566	225.604	231.091
230.291					

Y [ft] <- X [ft] ->

	1076752	1077412	1078072	1078732	1079392
1080052					
%12153625.00	240.619	240.222	239.808	239.376	238.930
238.469					
%12154285.00	241.748	241.459	241.157	240.841	240.511
240.165					
%12154945.00	242.921	242.742	242.554	242.354	242.142
241.914					
%12155605.00	244.133	244.068	243.996	243.915	243.823
243.716					
%12156265.00	245.380	245.434	245.483	245.524	245.554
245.572					
%12156925.00	246.662	246.839	247.013	247.179	247.336
247.480					
%12157585.00	247.976	248.282	248.585	248.881	249.168
249.442					

Y [ft] <- X [ft] ->

	1076752	1077412	1078072	1078732	1079392	1080052
%12158245.00	249.324	249.764	250.201	250.631	251.051	251.458
%12158905.00	250.706	251.286	251.861	252.428	252.985	253.530
%12159565.00	252.124	252.848	253.567	254.276	254.974	255.658
%12160225.00	253.581	254.455	255.321	256.176	257.018	257.845
%12160885.00	255.081	256.109	257.127	258.132	259.121	260.093
%12161545.00	256.626	257.814	258.989	260.147	261.286	262.407
%12162205.00	258.223	259.576	260.910	262.225	263.518	264.789
%12162865.00	259.877	261.399	262.898	264.373	265.822	267.245
%12163525.00	261.596	263.290	264.957	266.595	268.203	269.780
%12164185.00	263.385	265.258	267.097	268.901	270.668	272.401
%12164845.00	265.256	267.311	269.325	271.297	273.227	275.116
%12165505.00	267.217	269.460	271.652	273.793	275.885	277.931
%12166165.00	269.282	271.717	274.090	276.401	278.654	280.856
%12166825.00	271.467	274.101	276.654	279.132	281.543	283.898
%12167485.00	273.795	276.633	279.364	282.000	284.559	287.061
%12168145.00	276.298	279.346	282.245	285.020	287.708	290.344
%12168805.00	279.028	282.292	285.333	288.207	290.989	293.738
%12169465.00	282.076	285.558	288.675	291.568	294.384	297.215
%12170125.00	285.621	289.315	292.332	295.081	297.848	300.728
%12170785.00	290.094	293.941	296.309	298.636	301.278	304.203
%12171445.00	296.803	300.213	300.178	301.926	304.513	307.560
%12172105.00	298.756	302.388	302.535	304.536	307.403	310.747
%12172765.00	295.617	300.211	303.320	306.436	309.927	313.764
%12173425.00	294.677	299.613	303.912	308.001	312.193	316.629
%12174085.00	294.618	299.831	304.753	309.527	314.315	319.285
%12174745.00	294.996	300.478	305.847	311.143	316.394	

321.651					
%12175405.00	295.617	301.368	307.133	312.927	318.637
323.949					
%12176065.00	296.380	302.379	308.506	314.894	321.460
327.005					
%12176725.00	297.242	303.420	309.759	316.682	325.165
333.408					
%12177385.00	298.251	304.494	310.663	317.313	325.606
333.952					
%12178045.00	299.627	305.878	311.309	316.716	322.427
327.211					
%12178705.00	301.915	308.486	311.967	315.709	319.929
323.993					
%12179365.00	304.533	314.135	311.807	314.243	317.741
321.549					
%12180025.00	300.254	306.470	309.108	311.988	315.413
319.154					
%12180685.00	296.058	301.485	305.636	309.276	312.899
316.625					
%12181345.00	293.098	298.217	302.651	306.616	310.372
314.061					
%12182005.00	290.900	295.826	300.238	304.237	307.988
311.611					
%12182665.00	289.296	294.089	298.347	302.188	305.806
309.341					
%12183325.00	288.291	293.025	296.971	300.435	303.775
307.186					
%12183985.00	288.069	292.947	296.146	298.844	301.734
304.962					

Y [ft]	<- X [ft] ->					
	1076752	1077412	1078072	1078732	1079392	1080052
%12184645.00	288.935	295.259	295.629	297.050	299.429	302.431
%12185305.00	287.594	295.649	293.452	294.439	296.620	299.448
%12185965.00	281.874	286.489	288.853	290.885	293.295	296.071
%12186625.00	277.027	281.038	284.220	286.974	289.692	292.500
%12187285.00	272.954	276.718	280.082	283.147	286.068	288.933
%12187945.00	269.322	272.951	276.351	279.542	282.577	285.497
%12188605.00	265.971	269.527	272.933	276.181	279.284	282.255
%12189265.00	262.827	266.353	269.766	273.051	276.205	279.229
%12189925.00	259.858	263.384	266.814	270.135	273.338	276.418
%12190585.00	257.051	260.596	264.056	267.418	270.674	273.816
%12191245.00	254.399	257.976	261.474	264.885	268.200	271.410
%12191905.00	251.897	255.514	259.059	262.525	265.904	269.189
%12192565.00	249.539	253.201	256.798	260.326	263.776	267.142
%12193225.00	247.320	251.028	254.682	258.277	261.806	265.259
%12193885.00	245.231	248.985	252.697	256.367	259.984	263.532
%12194545.00	243.265	247.057	250.828	254.581	258.302	261.961
%12195205.00	241.410	245.221	249.046	252.897	256.755	260.561
%12195865.00	239.649	243.441	247.305	251.275	255.329	259.366
%12196525.00	237.955	241.655	245.525	249.631	253.980	258.447
%12197185.00	236.270	239.762	243.579	247.808	252.546	257.854
%12197845.00	234.441	237.606	241.302	245.569	250.586	256.945
%12198505.00	232.120	234.999	238.558	242.726	247.599	253.476

Y [ft]	<- X [ft] ->				
	1080712	1081372	1082032	1082692	1083352	1084012

%12153625.00	237.993	237.500	236.985	236.441	235.860
235.232					
%12154285.00	239.804	239.424	239.022	238.593	238.132
237.634					
%12154945.00	241.671	241.409	241.126	240.819	240.484
240.120					
%12155605.00	243.594	243.454	243.295	243.113	242.909
242.680					
%12156265.00	245.574	245.559	245.527	245.474	245.401
245.309					
%12156925.00	247.610	247.724	247.820	247.899	247.959
248.002					
%12157585.00	249.703	249.947	250.176	250.387	250.581
250.759					
%12158245.00	251.852	252.230	252.593	252.938	253.267
253.579					
%12158905.00	254.060	254.574	255.072	255.554	256.019
256.467					
%12159565.00	256.327	256.979	257.615	258.235	258.837
259.423					
%12160225.00	258.655	259.448	260.224	260.984	261.726
262.451					
%12160885.00	261.047	261.983	262.901	263.802	264.685
265.553					
%12161545.00	263.507	264.587	265.648	266.691	267.717
268.729					
%12162205.00	266.037	267.263	268.468	269.654	270.824
271.980					
%12162865.00	268.642	270.015	271.364	272.693	274.005
275.305					
%12163525.00	271.328	272.847	274.341	275.811	277.263
278.704					
%12164185.00	274.100	275.767	277.403	279.013	280.601
282.175					
%12164845.00	276.966	278.780	280.559	282.305	284.023
285.722					

Y [ft] <- X [ft] ->

	1080712	1081372	1082032	1082692	1083352	1084012
%12165505.00	279.934	281.895	283.816	285.698	287.541	289.353
%12166165.00	283.011	285.122	287.188	289.205	291.171	293.085
%12166825.00	286.205	288.469	290.685	292.845	294.936	296.947
%12167485.00	289.520	291.942	294.321	296.640	298.871	300.984
%12168145.00	292.952	295.542	298.104	300.615	303.023	305.262
%12168805.00	296.489	299.256	302.033	304.789	307.449	309.883
%12169465.00	300.100	303.053	306.078	309.158	312.214	315.016
%12170125.00	303.738	306.881	310.171	313.647	317.329	320.964
%12170785.00	307.347	310.673	314.198	318.037	322.490	328.140
%12171445.00	310.887	314.395	318.061	322.007	326.655	333.354
%12172105.00	314.366	318.097	321.811	325.511	329.402	333.544
%12172765.00	317.846	321.964	325.742	328.946	331.793	334.424
%12173425.00	321.380	326.323	330.501	332.823	334.359	335.962
%12174085.00	324.741	331.355	338.237	337.301	336.787	337.496
%12174745.00	327.220	334.181	343.908	339.480	338.144	338.493
%12175405.00	328.777	333.437	337.073	337.998	338.147	338.771
%12176065.00	330.461	333.128	335.319	336.697	337.589	338.518
%12176725.00	332.548	333.251	334.638	335.929	336.983	337.974
%12177385.00	332.424	332.900	334.208	335.494	336.488	337.296
%12178045.00	329.879	331.932	333.935	335.461	336.239	336.593
%12178705.00	327.560	330.927	334.225	336.370	336.451	335.885
%12179365.00	325.491	329.858	335.478	340.367	337.014	334.897
%12180025.00	323.178	327.777	333.999	340.675	335.413	332.990
%12180685.00	320.492	324.547	328.621	331.246	331.100	330.137
%12181345.00	317.714	321.242	324.333	326.406	327.178	327.108
%12182005.00	315.125	318.412	321.201	323.157	324.152	

324.398					
%12182665.00	312.824	316.149	319.017	321.010	321.953
322.132					
%12183325.00	310.736	314.389	317.817	320.067	320.576
320.251					
%12183985.00	308.599	312.809	317.828	321.388	319.918
318.456					
%12184645.00	306.015	310.450	317.004	326.937	318.266
316.084					
%12185305.00	302.787	306.669	311.041	314.030	313.604
312.763					
%12185965.00	299.133	302.365	305.446	307.676	308.681
309.037					
%12186625.00	295.385	298.240	300.855	302.958	304.433
305.437					
%12187285.00	291.745	294.441	296.907	299.026	300.749
302.129					
%12187945.00	288.303	290.960	293.409	295.595	297.493
299.125					
%12188605.00	285.091	287.770	290.262	292.536	294.579
296.401					
%12189265.00	282.114	284.847	287.409	289.782	291.957
293.937					
%12189925.00	279.366	282.170	284.817	287.295	289.595
291.716					
%12190585.00	276.834	279.721	282.463	285.052	287.476
289.730					
%12191245.00	274.508	277.484	280.330	283.036	285.589
287.976					

Y [ft]	<- X [ft] ->				
	1080712	1081372	1082032	1082692	1083352
%12191905.00	272.372	275.446	278.402	281.234	283.926
%12192565.00	270.415	273.590	276.663	279.631	282.480
%12193225.00	268.625	271.902	275.093	278.204	281.234
%12193885.00	266.994	270.368	273.666	276.917	280.148
%12194545.00	265.524	268.979	272.352	275.708	279.133
%12195205.00	264.237	267.743	271.123	274.498	278.031
%12195865.00	263.206	266.714	269.968	273.201	276.655
%12196525.00	262.620	266.028	268.889	271.747	274.901
%12197185.00	263.055	265.984	267.804	270.034	272.780
%12197845.00	267.421	266.396	266.177	267.854	270.314
%12198505.00	260.175	262.245	263.134	265.030	267.521

Y [ft]	<- X [ft] ->				
	1084672	1085332	1085992	1086652	1087312
%12153625.00	234.550	233.811	233.020	232.186	231.322
%12154285.00	237.096	236.520	235.911	235.282	234.649
%12154945.00	239.727	239.309	238.874	238.436	238.016
%12155605.00	242.431	242.165	241.892	241.626	241.393
%12156265.00	245.200	245.079	244.955	244.841	244.760
%12156925.00	248.030	248.048	248.062	248.081	248.122
%12157585.00	250.922	251.073	251.217	251.359	251.503
%12158245.00	253.877	254.160	254.431	254.690	254.936
%12158905.00	256.899	257.315	257.714	258.093	258.448
%12159565.00	259.992	260.544	261.075	261.583	262.059
%12160225.00	263.160	263.852	264.522	265.167	265.778

%12160885.00	266.405	267.241	268.058	268.851	269.611
270.326					
%12161545.00	269.728	270.713	271.685	272.637	273.561
274.441					
%12162205.00	273.127	274.267	275.401	276.526	277.631
278.697					
%12162865.00	276.600	277.896	279.198	280.509	281.822
283.109					
%12163525.00	280.142	281.591	283.063	284.571	286.119
287.687					
%12164185.00	283.749	285.339	286.970	288.673	290.481
292.410					
%12164845.00	287.416	289.127	290.890	292.758	294.806
297.148					
%12165505.00	291.147	292.947	294.796	296.759	298.943
301.552					
%12166165.00	294.957	296.809	298.682	300.641	302.787
305.280					
%12166825.00	298.876	300.740	302.575	304.437	306.393
308.499					
%12167485.00	302.956	304.794	306.532	308.226	309.923
311.631					
%12168145.00	307.273	309.045	310.625	312.092	313.510
314.892					
%12168805.00	311.947	313.594	314.924	316.089	317.201
318.303					
%12169465.00	317.188	318.578	319.476	320.220	320.975
321.797					
%12170125.00	323.466	324.171	324.249	324.414	324.762
325.277					
%12170785.00	332.425	330.284	328.954	328.508	328.473
328.656					
%12171445.00	340.836	334.788	332.944	332.325	332.077
331.912					
%12172105.00	336.331	336.372	336.015	335.927	335.730
335.161					

Y [ft] <- X [ft] ->

	1084672	1085332	1085992	1086652	1087312	1087972
%12172765.00	336.474	337.756	338.774	339.749	339.949	338.695
%12173425.00	337.638	339.373	341.460	344.337	346.281	342.797
%12174085.00	338.860	340.732	343.362	347.915	360.704	345.794
%12174745.00	339.682	341.488	343.899	346.785	348.153	345.011
%12175405.00	339.967	341.698	343.866	345.964	346.497	344.304
%12176065.00	339.762	341.471	343.766	346.657	348.383	344.974
%12176725.00	339.139	340.711	343.028	347.140	380.715	345.418
%12177385.00	338.167	339.328	340.997	343.346	344.860	341.618
%12178045.00	336.945	337.503	338.279	339.015	338.916	337.304
%12178705.00	335.537	335.477	335.563	335.536	335.038	333.867
%12179365.00	333.867	333.338	333.001	332.620	331.997	331.036
%12180025.00	331.785	331.071	330.545	330.026	329.390	328.578
%12180685.00	329.320	328.687	328.149	327.619	327.033	326.354
%12181345.00	326.724	326.268	325.804	325.331	324.829	324.282
%12182005.00	324.234	323.903	323.522	323.128	322.726	322.309
%12182665.00	321.943	321.631	321.302	320.987	320.689	320.403
%12183325.00	319.804	319.419	319.115	318.879	318.691	318.538
%12183985.00	317.635	317.174	316.914	316.774	316.710	316.696
%12184645.00	315.185	314.792	314.650	314.648	314.730	314.866
%12185305.00	312.347	312.236	312.308	312.491	312.745	313.045
%12185965.00	309.275	309.561	309.913	310.318	310.763	311.237
%12186625.00	306.202	306.874	307.518	308.158	308.801	309.452
%12187285.00	303.271	304.267	305.179	306.043	306.879	307.702
%12187945.00	300.541	301.797	302.940	304.005	305.019	306.001
%12188605.00	298.028	299.492	300.829	302.069	303.238	304.360
%12189265.00	295.734	297.370	298.867	300.251	301.550	

302.789

%12189925.00	293.660	295.439	297.068	298.569	299.968
301.296					
%12190585.00	291.807	293.710	295.447	297.037	298.505
299.887					
%12191245.00	290.183	292.200	294.025	295.674	297.176
298.573					
%12191905.00	288.804	290.933	292.829	294.505	295.997
297.361					
%12192565.00	287.696	289.951	291.906	293.566	294.990
296.263					
%12193225.00	286.897	289.327	291.331	292.908	294.175
295.278					
%12193885.00	286.461	289.199	291.252	292.600	293.555
294.388					
%12194545.00	286.418	289.874	291.991	292.700	293.066
293.526					
%12195205.00	286.517	292.138	294.419	292.987	292.467
292.562					
%12195865.00	285.483	293.172	295.747	292.142	291.338
291.359					
%12196525.00	282.612	286.923	289.264	289.445	289.564
289.914					
%12197185.00	279.323	282.545	284.973	286.503	287.576
288.426					
%12197845.00	276.222	279.171	281.790	283.996	285.821
287.196					
%12198505.00	273.287	276.243	279.119	281.900	284.540
286.628					

Y [ft] <- X [ft] ->

	1088632	1089292	1089952	1090612	1091272
1091932					

Y [ft]	<- X [ft] ->				
	1088632	1089292	1089952	1090612	1091272
1091932					
%12153625.00	229.538	228.594	227.532	226.200	224.426
222.172					
%12154285.00	233.447	232.901	232.330	231.480	229.862
227.335					
%12154945.00	237.377	237.276	237.430	237.695	236.491
233.012					
%12155605.00	241.208	241.458	242.308	244.933	246.470
238.646					
%12156265.00	244.854	245.194	245.981	247.549	247.190
242.395					
%12156925.00	248.347	248.580	248.876	248.934	247.818
245.171					
%12157585.00	251.806	251.930	251.921	251.536	250.425
248.450					
%12158245.00	255.346	255.446	255.368	254.960	254.035
252.460					
%12158905.00	259.026	259.193	259.204	258.975	258.388
257.260					
%12159565.00	262.865	263.158	263.347	263.415	263.345
262.993					
%12160225.00	266.855	267.302	267.691	268.071	268.593
269.663					
%12160885.00	270.987	271.587	272.143	272.711	273.473
275.069					
%12161545.00	275.260	276.008	276.684	277.300	277.846
278.147					
%12162205.00	279.694	280.591	281.374	282.032	282.450
282.131					
%12162865.00	284.319	285.386	286.275	287.042	287.772
287.993					
%12163525.00	289.193	290.480	291.417	292.149	293.314
297.022					
%12164185.00	294.392	296.094	296.956	297.062	297.298
298.285					
%12164845.00	299.916	302.833	303.560	301.923	300.253
298.368					
%12165505.00	305.080	311.541	312.531	306.471	303.262
300.324					
%12166165.00	308.411	312.403	312.894	309.356	306.220
303.067					
%12166825.00	310.718	312.588	312.949	311.590	309.341
306.410					
%12167485.00	313.252	314.503	315.001	314.584	313.217
310.612					
%12168145.00	316.189	317.283	318.064	318.519	318.477
316.388					
%12168805.00	319.397	320.465	321.531	322.828	325.458
326.421					
%12169465.00	322.711	323.746	324.942	326.354	328.241
327.280					
%12170125.00	325.978	326.941	328.238	329.598	329.491

326.132
%12170785.00 329.060 329.839 331.326 334.119 334.667
327.835
%12171445.00 331.858 332.144 333.209 336.275 338.056
328.656
%12172105.00 334.404 333.804 333.578 333.505 331.768
327.336
%12172765.00 336.826 335.097 333.586 331.947 329.541
326.133
%12173425.00 339.063 336.162 333.695 331.275 328.577
325.477
%12174085.00 340.526 336.867 333.814 330.979 328.133
325.175
%12174745.00 340.830 337.098 333.801 330.779 327.888
325.043
%12175405.00 340.661 336.961 333.589 330.524 327.672
324.957
%12176065.00 340.448 336.523 333.134 330.128 327.389
324.837
%12176725.00 339.629 335.634 332.374 329.537 326.984
324.636
%12177385.00 337.557 334.169 331.282 328.735 326.436
324.331
%12178045.00 334.841 332.300 329.925 327.748 325.753
323.920
%12178705.00 332.188 330.308 328.427 326.635 324.960
323.411
%12179365.00 329.780 328.358 326.890 325.453 324.089
322.823

Y [ft]	<- X [ft] ->				
	1088632	1089292	1089952	1090612	1091272
%12180025.00	327.597	326.504	325.367	324.242	323.167
%12180685.00	325.583	324.745	323.880	323.024	322.210
%12181345.00	323.689	323.064	322.428	321.808	321.228
%12182005.00	321.879	321.440	321.007	320.596	320.226
%12182665.00	320.125	319.858	319.607	319.386	319.206
%12183325.00	318.409	318.304	318.224	318.176	318.169
%12183985.00	316.718	316.770	316.851	316.966	317.120
%12184645.00	315.042	315.251	315.489	315.759	316.064
%12185305.00	313.381	313.746	314.138	314.558	315.008
%12185965.00	311.736	312.258	312.802	313.370	313.961
%12186625.00	310.114	310.791	311.486	312.200	312.933
%12187285.00	308.523	309.350	310.192	311.052	311.930
%12187945.00	306.969	307.939	308.921	309.927	310.956
%12188605.00	305.460	306.557	307.671	308.818	310.007
%12189265.00	303.997	305.202	306.431	307.709	309.060
%12189925.00	302.584	303.868	305.184	306.571	308.070
%12190585.00	301.221	302.548	303.913	305.366	306.969
%12191245.00	299.910	301.237	302.601	304.060	305.685
%12191905.00	298.655	299.933	301.244	302.641	304.185
%12192565.00	297.459	298.639	299.847	301.125	302.508
%12193225.00	296.319	297.357	298.427	299.549	300.736
%12193885.00	295.219	296.085	296.996	297.952	298.943
%12194545.00	294.117	294.807	295.563	296.361	297.180
%12195205.00	292.958	293.504	294.128	294.792	295.468
%12195865.00	291.698	292.169	292.697	293.251	293.814
%12196525.00	290.363	290.823	291.279	291.741	292.215

292.683
%12197185.00 289.067 289.525 289.892 290.256 290.659
291.090
%12197845.00 288.004 288.355 288.537 288.761 289.108
289.567
%12198505.00 287.467 287.368 287.154 287.168 287.472
288.051

Y [ft] <- X [ft] ->

	1092592	1093252	1093912	1094572	1095232	1095892
%12153625.00	219.582	216.830	214.024	211.211	208.409	205.627
%12154285.00	224.357	221.294	218.263	215.282	212.344	209.445
%12154945.00	229.279	225.810	222.541	219.394	216.325	213.309
%12155605.00	234.010	230.232	226.795	223.522	220.338	217.214
%12156265.00	238.157	234.456	230.998	227.657	224.382	221.157
%12156925.00	241.918	238.562	235.194	231.826	228.470	225.143
%12157585.00	245.817	242.775	239.491	236.081	232.625	229.179
%12158245.00	250.199	247.325	244.015	240.478	236.867	233.269
%12158905.00	255.319	252.427	248.868	245.046	241.193	237.401
%12159565.00	261.620	258.343	254.075	249.742	245.560	241.543
%12160225.00	270.757	265.233	259.379	254.398	249.877	245.643

Y [ft]	<- X [ft] ->				
	1092592	1093252	1093912	1094572	1095232
1095892					
%12160885.00	279.068	270.617	264.047	258.767	254.043
249.652					
%12161545.00	277.104	273.087	267.856	262.774	258.014
253.540					
%12162205.00	280.161	276.317	271.512	266.576	261.821
257.307					
%12162865.00	285.481	280.562	275.335	270.292	265.502
260.961					
%12163525.00	293.120	284.995	279.078	273.876	269.054
264.506					
%12164185.00	294.795	288.091	282.366	277.237	272.461
267.943					
%12164845.00	295.000	290.252	285.246	280.390	275.738
271.284					
%12165505.00	296.808	292.609	288.060	283.454	278.933
274.552					
%12166165.00	299.477	295.401	291.017	286.536	282.097
277.771					
%12166825.00	302.777	298.611	294.176	289.681	285.253
280.952					
%12167485.00	306.743	302.200	297.499	292.868	288.388
284.085					
%12168145.00	311.484	306.031	300.861	296.017	291.457
287.145					
%12168805.00	316.474	309.667	304.030	299.007	294.394
290.094					
%12169465.00	319.264	312.478	306.769	301.722	297.135
292.896					
%12170125.00	320.411	314.449	309.011	304.111	299.645
295.526					
%12170785.00	321.581	315.949	310.835	306.180	301.915
297.975					
%12171445.00	322.343	317.058	312.310	307.965	303.960
300.246					
%12172105.00	322.409	317.781	313.491	309.507	305.803
302.352					
%12172765.00	322.218	318.263	314.456	310.856	307.475
304.310					
%12173425.00	322.105	318.663	315.290	312.060	309.004
306.134					
%12174085.00	322.122	319.054	316.047	313.156	310.414
307.837					
%12174745.00	322.222	319.445	316.748	314.164	311.719
309.428					
%12175405.00	322.341	319.816	317.395	315.092	312.925
310.908					
%12176065.00	322.428	320.143	317.978	315.938	314.034
312.278					
%12176725.00	322.450	320.403	318.486	316.699	315.047
313.538					
%12177385.00	322.387	320.584	318.914	317.374	315.966

314.693					
%12178045.00	322.232	320.680	319.257	317.963	316.795
315.753					
%12178705.00	321.988	320.690	319.517	318.467	317.540
316.730					
%12179365.00	321.663	320.619	319.694	318.890	318.208
317.639					
%12180025.00	321.265	320.468	319.788	319.231	318.799
318.487					
%12180685.00	320.800	320.240	319.797	319.483	319.307
319.271					
%12181345.00	320.272	319.934	319.715	319.634	319.711
319.964					
%12182005.00	319.682	319.547	319.532	319.663	319.974
320.508					
%12182665.00	319.034	319.079	319.241	319.552	320.055
320.818					
%12183325.00	318.332	318.533	318.842	319.290	319.921
320.809					
%12183985.00	317.584	317.919	318.344	318.886	319.578
320.473					
%12184645.00	316.803	317.253	317.771	318.373	319.077
319.900					
%12185305.00	316.005	316.558	317.154	317.798	318.494
319.233					
%12185965.00	315.209	315.860	316.527	317.210	317.903
318.590					
%12186625.00	314.434	315.185	315.924	316.647	317.353
318.036					

Y [ft] <- X [ft] ->

	1092592	1093252	1093912	1094572	1095232	1095892
%12187285.00	313.704	314.563	315.377	316.138	316.860	317.572
%12187945.00	313.039	314.028	314.926	315.711	316.416	317.130
%12188605.00	312.461	313.628	314.635	315.414	316.008	316.589
%12189265.00	311.982	313.432	314.632	315.363	315.662	315.847
%12189925.00	311.564	313.516	315.191	315.840	315.467	314.880
%12190585.00	311.029	313.813	316.985	317.558	315.413	313.633
%12191245.00	309.980	313.398	320.260	321.002	314.619	311.832
%12191905.00	308.122	310.893	314.258	314.589	311.692	309.272
%12192565.00	305.732	307.522	308.968	309.144	307.979	306.314
%12193225.00	303.256	304.426	305.226	305.342	304.701	303.487
%12193885.00	300.911	301.740	302.291	302.420	302.042	301.111
%12194545.00	298.744	299.386	299.846	300.066	299.980	299.403
%12195205.00	296.737	297.264	297.693	298.051	298.402	298.636
%12195865.00	294.862	295.293	295.666	296.079	296.828	298.775
%12196525.00	293.105	293.439	293.672	293.889	294.362	295.776
%12197185.00	291.484	291.741	291.767	291.550	291.153	290.471
%12197845.00	290.041	290.327	290.167	289.426	288.145	286.281
%12198505.00	288.806	289.420	289.230	287.870	285.719	283.054

Y [ft] <- X [ft] ->

	1096552	1097212	1097872	1098532	1099192	1099852
%12153625.00	202.865	200.125	197.408	194.716	192.048	189.404
%12154285.00	206.578	203.742	200.935	198.158	195.410	192.692
%12154945.00	210.337	207.402	204.504	201.640	198.811	196.016
%12155605.00	214.137	211.103	208.111	205.159	202.247	199.374

%12156265.00	217.976	214.842	211.754	208.712	205.716
202.765					
%12156925.00	221.855	218.616	215.429	212.295	209.214
206.184					
%12157585.00	225.773	222.421	219.131	215.904	212.737
209.628					
%12158245.00	229.725	226.252	222.855	219.532	216.280
213.094					
%12158905.00	233.700	230.098	226.590	223.172	219.836
216.575					
%12159565.00	237.675	233.941	230.325	226.815	223.400
220.069					
%12160225.00	241.619	237.762	234.046	230.452	226.963
223.568					
%12160885.00	245.503	241.543	237.741	234.072	230.520
227.068					
%12161545.00	249.305	245.268	241.397	237.669	234.064
230.565					
%12162205.00	253.019	248.928	245.009	241.236	237.590
234.056					
%12162865.00	256.643	252.522	248.571	244.770	241.097
237.538					
%12163525.00	260.181	256.048	252.085	248.269	244.582
241.010					
%12164185.00	263.634	259.510	255.549	251.733	248.046
244.472					
%12164845.00	267.013	262.912	258.967	255.164	251.488
247.925					
%12165505.00	270.327	266.260	262.342	258.563	254.910
251.369					
%12166165.00	273.589	269.559	265.677	261.932	258.313
254.805					
%12166825.00	276.803	272.812	268.971	265.270	261.696
258.233					
%12167485.00	279.963	276.012	272.222	268.577	265.060
261.655					

Y [ft] <- X [ft] ->

	1096552	1097212	1097872	1098532	1099192	1099852
%12168145.00	283.052	279.153	275.425	271.848	268.403	265.070
%12168805.00	286.049	282.219	278.572	275.081	271.724	268.479
%12169465.00	288.933	285.199	281.655	278.272	275.023	271.885
%12170125.00	291.688	288.082	284.670	281.418	278.300	275.289
%12170785.00	294.305	290.863	287.611	284.519	281.557	278.697
%12171445.00	296.784	293.539	290.478	287.574	284.797	282.116
%12172105.00	299.130	296.111	293.271	290.583	288.021	285.553
%12172765.00	301.350	298.581	295.986	293.544	291.230	289.013
%12173425.00	303.451	300.949	298.620	296.450	294.418	292.495
%12174085.00	305.436	303.212	301.164	299.287	297.568	295.985
%12174745.00	307.305	305.359	303.598	302.028	300.651	299.452
%12175405.00	309.055	307.380	305.901	304.638	303.615	302.843
%12176065.00	310.681	309.261	308.043	307.064	306.382	306.069
%12176725.00	312.181	310.993	310.001	309.252	308.833	308.913
%12177385.00	313.560	312.579	311.770	311.171	310.864	311.027
%12178045.00	314.836	314.044	313.380	312.859	312.507	312.382
%12178705.00	316.030	315.425	314.897	314.425	313.973	313.472
%12179365.00	317.169	316.771	316.403	316.010	315.515	314.786
%12180025.00	318.276	318.126	317.973	317.735	317.320	316.591
%12180685.00	319.359	319.524	319.672	319.681	319.465	318.994
%12181345.00	320.397	320.975	321.565	321.919	321.897	321.814
%12182005.00	321.316	322.433	323.753	324.686	324.506	324.089
%12182665.00	321.952	323.655	326.248	329.123	327.489	324.830
%12183325.00	322.088	324.041	327.505	338.334	329.264	324.115
%12183985.00	321.654	323.256	325.420	327.276	325.453	322.043
%12184645.00	320.854	321.906	322.860	323.105	321.943	

	319.684					
%12185305.00	319.977	320.627	320.976	320.713	319.614	317.764
%12185965.00	319.216	319.668	319.757	319.276	318.122	316.371
%12186625.00	318.656	319.103	319.165	318.592	317.293	315.427
%12187285.00	318.289	318.948	319.274	318.727	317.091	314.829
%12187945.00	317.983	319.100	320.334	320.175	317.528	314.392
%12188605.00	317.431	318.977	322.346	325.591	318.020	313.609
%12189265.00	316.296	317.435	319.988	321.434	315.830	311.732
%12189925.00	314.562	314.640	314.872	314.076	311.556	308.716
%12190585.00	312.440	311.584	310.717	309.387	307.427	305.172
%12191245.00	310.022	308.570	307.153	305.546	303.673	301.600
%12191905.00	307.337	305.600	303.881	302.084	300.197	298.242
%12192565.00	304.538	302.694	300.773	298.800	296.851	295.050
%12193225.00	301.868	299.938	297.797	295.576	293.439	291.632
%12193885.00	299.576	297.467	294.976	292.353	289.815	287.568

Y [ft]	<- X [ft] ->				
	1096552	1097212	1097872	1098532	1099192
%12194545.00	297.946	295.449	292.349	289.126	286.002
%12195205.00	297.568	294.079	289.875	285.867	282.105
%12195865.00	301.084	293.057	287.205	282.456	278.164
%12196525.00	296.694	289.674	283.742	278.752	274.171
%12197185.00	288.512	284.447	279.605	274.808	270.149
%12197845.00	283.556	279.837	275.468	270.846	266.169
%12198505.00	279.830	275.997	271.669	267.047	262.302

Y [ft]	<- X [ft] ->				
	1100512	1101172	1101832	1102492	1103152
%12153625.00	186.785	184.190	181.619	179.071	176.545
%12154285.00	190.001	187.339	184.703	182.092	179.506
%12154945.00	193.253	190.522	187.820	185.147	182.501
%12155605.00	196.538	193.738	190.971	188.236	185.530
%12156265.00	199.855	196.986	194.154	191.357	188.592
%12156925.00	203.202	200.264	197.368	194.510	191.687
%12157585.00	206.574	203.569	200.610	197.693	194.813
%12158245.00	209.969	206.899	203.880	200.906	197.972
%12158905.00	213.383	210.251	207.175	204.147	201.161
%12159565.00	216.813	213.623	210.493	207.415	204.382
%12160225.00	220.254	217.012	213.834	210.710	207.633
%12160885.00	223.704	220.416	217.195	214.031	210.916
%12161545.00	227.159	223.833	220.576	217.378	214.231
%12162205.00	230.617	227.261	223.976	220.752	217.579
%12162865.00	234.076	230.700	227.396	224.153	220.961
217.811					

%12163525.00	237.537	234.149	230.835	227.582	224.380
221.219					
%12164185.00	240.998	237.610	234.295	231.042	227.838
224.674					
%12164845.00	244.461	241.083	237.778	234.533	231.338
228.180					
%12165505.00	247.926	244.569	241.284	238.059	234.881
231.740					
%12166165.00	251.395	248.070	244.816	241.620	238.472
235.358					
%12166825.00	254.868	251.587	248.375	245.221	242.112
239.037					
%12167485.00	258.347	255.121	251.964	248.862	245.804
242.779					
%12168145.00	261.833	258.676	255.584	252.546	249.550
246.587					
%12168805.00	265.328	262.253	259.239	256.275	253.352
250.460					
%12169465.00	268.836	265.857	262.933	260.053	257.209
254.397					
%12170125.00	272.361	269.495	266.673	263.884	261.123
258.394					
%12170785.00	275.913	273.178	270.471	267.778	265.098
262.441					
%12171445.00	279.502	276.921	274.346	271.754	269.142
266.532					
%12172105.00	283.143	280.750	278.331	275.846	273.282
270.667					
%12172765.00	286.853	284.696	282.478	280.123	277.580
274.875					
%12173425.00	290.640	288.791	286.860	284.703	282.164
279.233					
%12174085.00	294.498	293.052	291.561	289.803	287.306
283.880					
%12174745.00	298.396	297.433	296.571	295.791	293.753
288.951					

Y [ft] <- X [ft] ->

	1100512	1101172	1101832	1102492	1103152	1103812
%12175405.00	302.288	301.829	301.477	302.334	305.964	293.724
%12176065.00	306.161	306.359	305.770	304.730	302.528	295.224
%12176725.00	309.830	312.005	310.868	305.679	300.677	294.960
%12177385.00	312.126	315.967	314.579	306.178	300.284	294.710
%12178045.00	312.534	312.574	310.236	305.289	299.933	294.546
%12178705.00	312.743	311.344	308.627	304.554	299.722	294.539
%12179365.00	313.591	311.608	308.592	304.602	299.928	294.831
%12180025.00	315.284	313.024	309.652	305.413	300.639	295.511
%12180685.00	318.026	315.715	311.674	306.828	301.785	296.607
%12181345.00	322.185	320.669	314.455	308.469	303.151	298.099
%12182005.00	325.760	329.298	316.292	309.571	304.352	299.900
%12182665.00	323.373	320.782	315.121	309.560	304.905	301.414
%12183325.00	320.896	317.503	313.276	308.758	304.521	301.011
%12183985.00	318.812	315.469	311.760	307.742	303.559	299.257
%12184645.00	316.957	313.951	310.645	306.965	302.761	297.868
%12185305.00	315.426	312.799	309.959	306.785	302.765	297.378
%12185965.00	314.224	311.897	309.596	307.458	304.500	298.031
%12186625.00	313.256	311.025	309.043	308.148	313.995	299.044
%12187285.00	312.407	310.013	307.748	305.823	303.431	295.900
%12187945.00	311.569	308.954	306.192	302.805	298.178	291.881
%12188605.00	310.550	308.074	305.322	301.033	295.228	288.725
%12189265.00	308.984	307.341	306.426	300.952	293.073	285.908
%12189925.00	306.447	305.345	308.247	300.112	290.314	282.837
%12190585.00	302.994	301.034	298.689	293.379	286.185	279.252
%12191245.00	299.350	296.691	293.058	287.943	281.770	275.366
%12191905.00	296.131	293.394	289.289	283.815	277.678	

						271.433
%12192565.00	293.508	291.728	287.152	280.464	273.822	267.491
%12193225.00	290.708	293.216	286.534	276.990	269.830	263.442
%12193885.00	285.906	284.822	279.706	272.123	265.373	259.196
%12194545.00	280.178	276.900	272.267	266.510	260.571	254.791
%12195205.00	274.830	270.849	266.265	261.132	255.751	250.348
%12195865.00	269.936	265.636	261.037	256.151	251.089	245.971
%12196525.00	265.368	260.891	256.269	251.497	246.622	241.706
%12197185.00	261.023	256.441	251.797	247.088	242.331	237.560
%12197845.00	256.843	252.190	247.529	242.857	238.183	233.521
%12198505.00	252.787	248.075	243.399	238.755	234.144	229.572

Y [ft] <- X [ft] ->

	1104472	1105132	1105792	1106452	1107112
%12153625.00	171.554	169.088	166.639	164.208	161.792
%12154285.00	174.401	171.879	169.376	166.892	164.423
%12154945.00	177.282	174.705	172.148	169.610	167.089
%12155605.00	180.197	177.565	174.955	172.364	169.790

Y [ft] <- X [ft] ->

	1104472	1105132	1105792	1106452	1107112
%12156265.00	183.147	180.461	177.798	175.154	172.528
%12156925.00	186.131	183.393	180.677	177.982	175.304
%12157585.00	189.151	186.361	183.594	180.848	178.119
%12158245.00	192.206	189.367	186.550	183.755	180.976
%12158905.00	195.298	192.411	189.547	186.704	183.877
%12159565.00	198.428	195.495	192.587	189.697	186.823
%12160225.00	201.596	198.622	195.671	192.738	189.820
%12160885.00	204.804	201.792	198.803	195.830	192.869
%12161545.00	208.054	205.010	201.986	198.976	195.976
%12162205.00	211.350	208.278	205.224	202.182	199.145
%12162865.00	214.694	211.599	208.521	205.451	202.383
%12163525.00	218.089	214.980	211.883	208.791	205.696
%12164185.00	221.539	218.423	215.316	212.208	209.092
%12164845.00	225.049	221.935	218.825	215.710	212.580
%12165505.00	228.624	225.521	222.419	219.306	216.171
%12166165.00	232.267	229.187	226.104	223.006	219.877
%12166825.00	235.983	232.938	229.888	226.818	223.711
%12167485.00	239.775	236.779	233.777	230.753	227.687
%12168145.00	243.645	240.713	237.776	234.816	231.814
%12168805.00	247.593	244.741	241.887	239.012	236.097
%12169465.00	251.616	248.858	246.110	243.343	240.529
%12170125.00	255.703	253.057	250.444	247.820	245.115
%12170785.00	259.834	257.308	254.875	252.484	249.940
%12171445.00	263.975	261.547	259.333	257.377	255.351
%12172105.00	268.082	265.658	263.586	262.225	262.301
%12172765.00	272.129	269.524	267.278	265.768	266.071
%12173425.00	276.133	273.135	270.395	267.885	265.084
%12174085.00	280.113	276.546	273.299	270.096	266.195
%12174745.00	283.928	279.670	276.147	273.046	269.041
%12175405.00	287.021	282.136	278.514	276.548	275.882
%12176065.00	288.701	283.540	279.530	276.956	274.629
%12176725.00	289.198	283.964	279.308	274.970	269.916
%12177385.00	289.207	283.882	278.730	273.544	267.934
%12178045.00	289.127	283.699	278.246	272.670	266.837
%12178705.00	289.160	283.640	277.989	272.186	266.205
%12179365.00	289.444	283.824	278.002	272.009	265.880
%12180025.00	290.075	284.332	278.313	272.100	265.781
%12180685.00	291.146	285.253	278.954	272.428	265.847
%12181345.00	292.811	286.753	279.964	272.943	266.004
%12182005.00	295.509	289.245	281.314	273.502	266.130

Y [ft] <- X [ft] ->

	1104472	1105132	1105792	1106452	1107112
%12182665.00	300.461	293.574	282.466	273.774	266.059
%12183325.00	298.800	292.116	281.988	273.385	265.655
%12183985.00	294.456	288.023	280.227	272.395	264.928
%12184645.00	292.182	285.643	278.491	271.184	264.009
%12185305.00	290.972	284.103	277.048	269.982	263.022
%12185965.00	290.327	282.915	275.776	268.828	262.031
%12186625.00	289.459	281.642	274.490	267.682	261.067
%12187285.00	287.493	279.969	273.045	266.499	260.156
%12187945.00	284.814	277.901	271.385	265.249	259.352
%12188605.00	282.050	275.568	269.476	263.857	258.690
%12189265.00	279.234	272.982	267.215	262.079	257.884
%12189925.00	276.184	270.067	264.472	259.528	255.610
%12190585.00	272.801	266.796	261.236	256.159	251.588
%12191245.00	269.148	263.235	257.651	252.372	247.287
%12191905.00	265.341	259.491	253.888	248.488	243.187
%12192565.00	261.442	255.643	250.055	244.627	239.282
%12193225.00	257.453	251.729	246.201	240.814	235.514
%12193885.00	253.365	247.768	242.344	237.048	231.840
%12194545.00	249.202	243.780	238.496	233.321	228.233
%12195205.00	245.020	239.793	234.667	229.632	224.677
%12195865.00	240.874	235.836	230.871	225.982	221.165
%12196525.00	236.797	231.929	227.118	222.372	217.693
%12197185.00	232.802	228.082	223.414	218.804	214.258
%12197845.00	228.888	224.297	219.758	215.277	210.857
%12198505.00	225.044	220.567	216.147	211.787	207.489

CALCULATION OF DRAWDOWN IN A HOMOGENEOUS, ISOTROPIC, CONFINED, LEAKY
CONFINED OR UNCONFINED AQUIFER WITH MULTIPLE PRODUCTION AND INJECTION
WELLS AND UNIFORM REGIONAL FLOW

Hassayampa Ranch 100 yr Aquifer Impact Analysis

********** INPUT DATA **********

UNCONFINED AQUIFER - THEIS EQUATION WITH JACOB'S CORRECTION

WATER TABLE CORRECTION APPLIED; DRAWDOWNS EXCEED 10% OF SATURATED THICKNESS

AQUIFER THICKNESS	=	650 [ft]
TRANSMISSIVITY	=	54000 [gpd/ft]
STORAGE COEFFICIENT	=	.13
REGIONAL FLOW GRADIENT (positive--downwards--in flow direction)	=	0
REGIONAL FLOW DIRECTION (horizontal angle in degrees counter-clockwise from positive x-axis)	=	0
REGIONAL FLOW OFFSET AT ORIGIN (positive in downwards direction)	=	0 [ft]

WATER TABLE CORRECTION APPLIED; DRAWDOWNS EXCEED 10% OF SATURATED THICKNESS

AQUIFER THICKNESS	=	650 [ft]

PUMPING/INJECTION WELL DATA

WELL NO. 1

```
                    X-COORDINATE  =  1095112 [ft]
                    Y-COORDINATE  =  1.217124E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 2

```
                    X-COORDINATE  =  1095112 [ft]
                    Y-COORDINATE  =  1.217256E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 3

```
                    X-COORDINATE  =**1095060** [ft]
                    Y-COORDINATE  =  1.217133E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 4

```
                    X-COORDINATE  =  1099480 [ft]
                    Y-COORDINATE  =  1.217376E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 5

```
                    X-COORDINATE  =  1101548 [ft]
                    Y-COORDINATE  =  1.217251E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 6

```
                    X-COORDINATE  =  1100750 [ft]
                    Y-COORDINATE  =  1.217108E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

Well identified as having the maximum impact

WELL NO. 7

```
                    X-COORDINATE  =  1070523 [ft]
                    Y-COORDINATE  =  1.214166E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
  TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 8

```
                    X-COORDINATE  =  1072903 [ft]
                    Y-COORDINATE  =  1.214206E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
  TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

WELL NO. 9

```
                    X-COORDINATE  =  1073229 [ft]
                    Y-COORDINATE  =  1.214046E+07 [ft]
           PUMPING/INJECTION RATE  =  1113120 [gpd]
  TIME SINCE START PUMPING/INJECTION  =  36500 [day]
```

---------- Drawdown in [ft] ----------

Y [ft] <- X [ft] ->

	1045072	1045732	1046392	1047052	1047712	1048372
%12153625.00	15.962	16.301	16.648	17.002	17.363	17.731
%12154285.00	15.931	16.269	16.613	16.964	17.322	17.687
%12154945.00	15.896	16.232	16.574	16.922	17.277	17.639
%12155605.00	15.858	16.191	16.530	16.876	17.228	17.587
%12156265.00	15.816	16.146	16.483	16.826	17.176	17.532
%12156925.00	15.770	16.098	16.432	16.773	17.119	17.472
%12157585.00	15.721	16.046	16.378	16.716	17.059	17.409
%12158245.00	15.668	15.991	16.320	16.655	16.996	17.342
%12158905.00	15.613	15.933	16.260	16.592	16.929	17.273
%12159565.00	15.555	15.872	16.196	16.525	16.860	17.200
%12160225.00	15.493	15.809	16.129	16.456	16.787	17.124
%12160885.00	15.429	15.742	16.060	16.383	16.712	17.046
%12161545.00	15.362	15.673	15.988	16.308	16.634	16.965
%12162205.00	15.293	15.601	15.913	16.231	16.554	16.882
%12162865.00	15.222	15.526	15.836	16.151	16.471	16.796
%12163525.00	15.148	15.450	15.757	16.069	16.386	16.708
%12164185.00	15.071	15.371	15.675	15.985	16.299	16.618
%12164845.00	14.993	15.290	15.592	15.898	16.209	16.525
%12165505.00	14.912	15.207	15.506	15.809	16.118	16.431
%12166165.00	14.830	15.121	15.418	15.719	16.024	16.335
%12166825.00	14.745	15.034	15.328	15.626	15.929	16.236
%12167485.00	14.659	14.945	15.236	15.532	15.832	16.136
%12168145.00	14.570	14.854	15.143	15.435	15.732	16.034
%12168805.00	14.480	14.762	15.047	15.337	15.632	15.930
%12169465.00	14.388	14.667	14.950	15.237	15.529	15.825
%12170125.00	14.295	14.571	14.851	15.136	15.425	15.718
%12170785.00	14.200	14.473	14.751	15.033	15.319	15.609
%12171445.00	14.103	14.374	14.649	14.928	15.212	15.499
%12172105.00	14.005	14.273	14.546	14.822	15.103	15.387
%12172765.00	13.905	14.171	14.441	14.714	14.992	15.274
%12173425.00	13.804	14.067	14.334	14.605	14.880	15.159
%12174085.00	13.701	13.962	14.226	14.495	14.767	15.043
%12174745.00	13.598	13.855	14.117	14.383	14.652	14.925
%12175405.00	13.492	13.748	14.006	14.269	14.536	14.807
%12176065.00	13.386	13.638	13.895	14.155	14.419	14.686
%12176725.00	13.278	13.528	13.782	14.039	14.300	14.565
%12177385.00	13.169	13.417	13.667	13.922	14.180	14.442
%12178045.00	13.059	13.304	13.552	13.804	14.059	14.318
%12178705.00	12.948	13.190	13.435	13.684	13.937	14.193

Y [ft] <- X [ft] ->

	1045072	1045732	1046392	1047052	1047712	1048372
%12179365.00	12.836	13.075	13.318	13.564	13.813	14.067
%12180025.00	12.723	12.959	13.199	13.442	13.689	13.939
%12180685.00	12.609	12.842	13.079	13.320	13.564	13.811
%12181345.00	12.494	12.725	12.959	13.196	13.437	13.682
%12182005.00	12.378	12.606	12.837	13.072	13.310	13.551
%12182665.00	12.261	12.486	12.715	12.947	13.182	13.420
%12183325.00	12.143	12.366	12.592	12.820	13.053	13.288
%12183985.00	12.025	12.245	12.468	12.694	12.923	13.155
%12184645.00	11.906	12.123	12.343	12.566	12.792	13.022
%12185305.00	11.786	12.000	12.218	12.438	12.661	12.887
%12185965.00	11.666	11.877	12.092	12.309	12.529	12.752
%12186625.00	11.545	11.754	11.965	12.179	12.396	12.617
%12187285.00	11.424	11.629	11.838	12.049	12.263	12.481
%12187945.00	11.302	11.505	11.710	11.919	12.130	12.344
%12188605.00	11.179	11.379	11.582	11.788	11.996	12.207
%12189265.00	11.057	11.254	11.454	11.656	11.862	12.069
%12189925.00	10.934	11.128	11.325	11.525	11.727	11.932
%12190585.00	10.810	11.002	11.196	11.393	11.592	11.794
%12191245.00	10.687	10.876	11.067	11.261	11.457	11.655
%12191905.00	10.563	10.749	10.937	11.128	11.321	11.517
%12192565.00	10.439	10.622	10.808	10.996	11.186	11.378
%12193225.00	10.315	10.496	10.678	10.863	11.050	11.240
%12193885.00	10.191	10.369	10.548	10.730	10.915	11.101
%12194545.00	10.067	10.242	10.419	10.598	10.779	10.962
%12195205.00	9.943	10.115	10.289	10.465	10.644	10.824
%12195865.00	9.819	9.988	10.160	10.333	10.508	10.686
%12196525.00	9.696	9.862	10.030	10.201	10.373	10.547
%12197185.00	9.572	9.736	9.901	10.069	10.238	10.410
%12197845.00	9.448	9.609	9.772	9.937	10.103	10.272
%12198505.00	9.325	9.484	9.644	9.805	9.969	10.135

Y [ft] <- X [ft] ->

	1049032	1049692	1050352	1051012	1051672	1052332
%12153625.00	18.106	18.489	18.879	19.277	19.683	20.097
%12154285.00	18.060	18.439	18.826	19.220	19.621	20.030
%12154945.00	18.008	18.384	18.767	19.157	19.554	19.959
%12155605.00	17.953	18.326	18.705	19.091	19.484	19.883
%12156265.00	17.894	18.263	18.638	19.020	19.409	19.804
%12156925.00	17.831	18.196	18.568	18.946	19.331	19.721
%12157585.00	17.765	18.126	18.494	18.869	19.249	19.635
%12158245.00	17.695	18.053	18.417	18.788	19.164	19.546
%12158905.00	17.622	17.977	18.337	18.704	19.076	19.454
%12159565.00	17.546	17.897	18.254	18.617	18.985	19.359

Y [ft]	<- X [ft] ->					
	1049032	1049692	1050352	1051012	1051672	1052332
%12160225.00	17.467	17.815	18.169	18.528	18.892	19.262
%12160885.00	17.386	17.730	18.080	18.436	18.796	19.162
%12161545.00	17.301	17.643	17.989	18.341	18.698	19.060
%12162205.00	17.215	17.553	17.896	18.245	18.598	18.956
%12162865.00	17.126	17.461	17.801	18.146	18.495	18.850
%12163525.00	17.035	17.367	17.703	18.045	18.391	18.742
%12164185.00	16.942	17.270	17.604	17.942	18.285	18.632
%12164845.00	16.846	17.172	17.502	17.837	18.176	18.521
%12165505.00	16.749	17.071	17.398	17.730	18.066	18.407
%12166165.00	16.649	16.969	17.293	17.621	17.954	18.292
%12166825.00	16.548	16.864	17.185	17.511	17.841	18.175
%12167485.00	16.445	16.758	17.076	17.399	17.726	18.057
%12168145.00	16.340	16.651	16.965	17.285	17.609	17.937
%12168805.00	16.234	16.541	16.853	17.169	17.490	17.815
%12169465.00	16.125	16.430	16.739	17.052	17.370	17.692
%12170125.00	16.015	16.317	16.623	16.933	17.248	17.567
%12170785.00	15.904	16.203	16.506	16.813	17.125	17.441
%12171445.00	15.791	16.087	16.387	16.691	17.000	17.313
%12172105.00	15.676	15.969	16.266	16.568	16.873	17.183
%12172765.00	15.560	15.850	16.144	16.443	16.745	17.052
%12173425.00	15.442	15.730	16.021	16.316	16.616	16.920
%12174085.00	15.323	15.608	15.896	16.188	16.485	16.786
%12174745.00	15.203	15.484	15.770	16.059	16.353	16.650
%12175405.00	15.081	15.359	15.642	15.928	16.219	16.514
%12176065.00	14.958	15.233	15.513	15.796	16.084	16.375
%12176725.00	14.833	15.106	15.382	15.663	15.947	16.236
%12177385.00	14.708	14.977	15.251	15.528	15.809	16.095
%12178045.00	14.581	14.847	15.118	15.392	15.670	15.952
%12178705.00	14.453	14.716	14.984	15.255	15.530	15.809
%12179365.00	14.324	14.584	14.848	15.116	15.388	15.664
%12180025.00	14.193	14.451	14.712	14.977	15.245	15.518
%12180685.00	14.062	14.316	14.574	14.836	15.102	15.371
%12181345.00	13.929	14.181	14.436	14.694	14.957	15.222
%12182005.00	13.796	14.044	14.296	14.552	14.810	15.073
%12182665.00	13.662	13.907	14.156	14.408	14.663	14.922
%12183325.00	13.527	13.769	14.014	14.263	14.515	14.771
%12183985.00	13.391	13.630	13.872	14.117	14.366	14.619
%12184645.00	13.254	13.490	13.729	13.971	14.217	14.466
%12185305.00	13.117	13.349	13.585	13.824	14.066	14.312
%12185965.00	12.979	13.208	13.440	13.676	13.915	14.157

Y [ft] <- X [ft] ->

	1049032	1049692	1050352	1051012	1051672	1052332
%12186625.00	12.840	13.066	13.295	13.528	13.763	14.002
%12187285.00	12.701	12.924	13.150	13.379	13.611	13.846
%12187945.00	12.561	12.781	13.003	13.229	13.458	13.689
%12188605.00	12.421	12.637	12.857	13.079	13.304	13.532
%12189265.00	12.280	12.493	12.710	12.929	13.150	13.375
%12189925.00	12.139	12.349	12.562	12.778	12.996	13.217
%12190585.00	11.998	12.205	12.414	12.627	12.842	13.059
%12191245.00	11.857	12.060	12.267	12.475	12.687	12.901
%12191905.00	11.715	11.915	12.119	12.324	12.532	12.743
%12192565.00	11.573	11.771	11.970	12.172	12.377	12.584
%12193225.00	11.432	11.626	11.822	12.021	12.222	12.426
%12193885.00	11.290	11.481	11.674	11.869	12.067	12.267
%12194545.00	11.148	11.336	11.526	11.718	11.912	12.109
%12195205.00	11.006	11.191	11.378	11.567	11.758	11.951
%12195865.00	10.865	11.047	11.230	11.416	11.603	11.793
%12196525.00	10.724	10.902	11.083	11.265	11.449	11.636
%12197185.00	10.583	10.758	10.935	11.114	11.295	11.478
%12197845.00	10.442	10.614	10.788	10.964	11.142	11.322
%12198505.00	10.302	10.471	10.642	10.815	10.989	11.165

Y [ft] <- X [ft] ->

	1052992	1053652	1054312	1054972	1055632	1056292
%12153625.00	20.518	20.947	21.384	21.828	22.280	22.740
%12154285.00	20.446	20.870	21.301	21.739	22.184	22.637
%12154945.00	20.370	20.788	21.214	21.646	22.085	22.530
%12155605.00	20.290	20.703	21.122	21.549	21.981	22.420
%12156265.00	20.205	20.613	21.028	21.448	21.875	22.307
%12156925.00	20.118	20.521	20.930	21.345	21.765	22.191
%12157585.00	20.027	20.425	20.829	21.239	21.654	22.074
%12158245.00	19.933	20.327	20.726	21.130	21.540	21.954
%12158905.00	19.837	20.226	20.620	21.019	21.424	21.833
%12159565.00	19.738	20.122	20.512	20.906	21.306	21.710
%12160225.00	19.637	20.017	20.402	20.792	21.186	21.586
%12160885.00	19.533	19.909	20.290	20.675	21.065	21.460
%12161545.00	19.427	19.799	20.176	20.557	20.943	21.333
%12162205.00	19.319	19.687	20.060	20.437	20.819	21.205
%12162865.00	19.210	19.574	19.943	20.316	20.694	21.076
%12163525.00	19.098	19.459	19.824	20.193	20.567	20.946
%12164185.00	18.985	19.342	19.703	20.069	20.439	20.814
%12164845.00	18.870	19.223	19.581	19.943	20.310	20.681
%12165505.00	18.753	19.103	19.457	19.816	20.180	20.547
%12166165.00	18.634	18.981	19.332	19.688	20.048	20.412
%12166825.00	18.514	18.858	19.206	19.558	19.915	20.276

Y [ft]	<- X [ft] ->					
	1052992	1053652	1054312	1054972	1055632	1056292
%12167485.00	18.393	18.733	19.078	19.427	19.780	20.138
%12168145.00	18.270	18.607	18.948	19.294	19.644	19.999
%12168805.00	18.145	18.479	18.817	19.160	19.507	19.858
%12169465.00	18.018	18.349	18.684	19.024	19.368	19.717
%12170125.00	17.890	18.218	18.550	18.887	19.228	19.573
%12170785.00	17.761	18.086	18.415	18.748	19.086	19.428
%12171445.00	17.630	17.952	18.278	18.608	18.943	19.282
%12172105.00	17.498	17.816	18.139	18.466	18.798	19.134
%12172765.00	17.363	17.679	17.999	18.323	18.652	18.985
%12173425.00	17.228	17.540	17.857	18.178	18.504	18.834
%12174085.00	17.091	17.400	17.714	18.032	18.354	18.681
%12174745.00	16.952	17.259	17.569	17.884	18.203	18.527
%12175405.00	16.812	17.116	17.423	17.734	18.050	18.371
%12176065.00	16.671	16.971	17.275	17.583	17.896	18.213
%12176725.00	16.528	16.825	17.126	17.431	17.740	18.054
%12177385.00	16.384	16.678	16.975	17.277	17.583	17.893
%12178045.00	16.239	16.529	16.823	17.121	17.424	17.731
%12178705.00	16.092	16.379	16.669	16.965	17.264	17.567
%12179365.00	15.944	16.227	16.515	16.806	17.102	17.402
%12180025.00	15.794	16.074	16.359	16.647	16.939	17.235
%12180685.00	15.644	15.920	16.201	16.486	16.774	17.067
%12181345.00	15.492	15.765	16.042	16.323	16.608	16.897
%12182005.00	15.339	15.609	15.883	16.160	16.441	16.727
%12182665.00	15.185	15.452	15.722	15.996	16.273	16.555
%12183325.00	15.030	15.293	15.560	15.830	16.104	16.381
%12183985.00	14.875	15.134	15.397	15.663	15.933	16.207
%12184645.00	14.718	14.974	15.233	15.496	15.762	16.032
%12185305.00	14.560	14.813	15.068	15.327	15.590	15.856
%12185965.00	14.402	14.651	14.903	15.158	15.417	15.679
%12186625.00	14.243	14.488	14.736	14.988	15.243	15.501
%12187285.00	14.084	14.325	14.570	14.817	15.068	15.322
%12187945.00	13.924	14.161	14.402	14.646	14.893	15.143
%12188605.00	13.763	13.997	14.234	14.474	14.717	14.963
%12189265.00	13.602	13.832	14.066	14.302	14.541	14.783
%12189925.00	13.441	13.668	13.897	14.129	14.364	14.602
%12190585.00	13.279	13.502	13.728	13.956	14.187	14.421
%12191245.00	13.118	13.337	13.559	13.783	14.010	14.240
%12191905.00	12.956	13.171	13.389	13.610	13.833	14.059
%12192565.00	12.794	13.006	13.220	13.437	13.656	13.878
%12193225.00	12.632	12.840	13.051	13.264	13.479	13.697

Y [ft] <- X [ft] ->

	1052992	1053652	1054312	1054972	1055632	1056292
%12193885.00	12.470	12.674	12.881	13.090	13.302	13.516
%12194545.00	12.308	12.509	12.712	12.918	13.125	13.335
%12195205.00	12.146	12.344	12.543	12.745	12.949	13.155
%12195865.00	11.985	12.179	12.375	12.573	12.773	12.975
%12196525.00	11.824	12.014	12.206	12.401	12.597	12.795
%12197185.00	11.663	11.850	12.039	12.229	12.422	12.616
%12197845.00	11.503	11.686	11.871	12.058	12.247	12.437
%12198505.00	11.343	11.523	11.705	11.888	12.073	12.259

Y [ft] <- X [ft] ->

	1056952	1057612	1058272	1058932	1059592	1060252
%12153625.00	23.207	23.681	24.162	24.649	25.141	25.639
%12154285.00	23.096	23.562	24.033	24.511	24.994	25.481
%12154945.00	22.982	23.439	23.903	24.371	24.844	25.322
%12155605.00	22.864	23.315	23.770	24.230	24.694	25.162
%12156265.00	22.745	23.188	23.635	24.088	24.544	25.003
%12156925.00	22.623	23.059	23.500	23.945	24.393	24.845
%12157585.00	22.499	22.929	23.363	23.801	24.243	24.687
%12158245.00	22.373	22.797	23.225	23.657	24.092	24.530
%12158905.00	22.247	22.665	23.087	23.513	23.942	24.374
%12159565.00	22.119	22.531	22.948	23.369	23.792	24.219
%12160225.00	21.989	22.397	22.809	23.224	23.643	24.064
%12160885.00	21.859	22.262	22.669	23.079	23.493	23.910
%12161545.00	21.728	22.126	22.529	22.935	23.344	23.756
%12162205.00	21.596	21.990	22.388	22.790	23.195	23.603
%12162865.00	21.462	21.853	22.247	22.645	23.046	23.450
%12163525.00	21.328	21.714	22.105	22.499	22.897	23.298
%12164185.00	21.193	21.576	21.962	22.353	22.747	23.145
%12164845.00	21.056	21.436	21.819	22.206	22.597	22.992
%12165505.00	20.919	21.295	21.675	22.059	22.447	22.838
%12166165.00	20.781	21.153	21.530	21.911	22.296	22.684
%12166825.00	20.641	21.010	21.384	21.762	22.144	22.530
%12167485.00	20.500	20.866	21.237	21.612	21.991	22.374
%12168145.00	20.358	20.721	21.089	21.461	21.837	22.217
%12168805.00	20.214	20.575	20.939	21.308	21.682	22.059
%12169465.00	20.069	20.427	20.788	21.154	21.525	21.900
%12170125.00	19.923	20.277	20.636	20.999	21.367	21.739
%12170785.00	19.775	20.126	20.482	20.843	21.208	21.577
%12171445.00	19.626	19.974	20.327	20.684	21.046	21.413
%12172105.00	19.475	19.820	20.170	20.524	20.883	21.247
%12172765.00	19.322	19.664	20.011	20.363	20.719	21.080
%12173425.00	19.168	19.507	19.851	20.199	20.552	20.910
%12174085.00	19.012	19.348	19.689	20.034	20.384	20.739

Y [ft]	<- X [ft] ->					
	1056952	1057612	1058272	1058932	1059592	1060252
%12174745.00	18.855	19.187	19.525	19.867	20.214	20.565
%12175405.00	18.695	19.025	19.359	19.698	20.041	20.390
%12176065.00	18.535	18.861	19.191	19.527	19.867	20.212
%12176725.00	18.372	18.695	19.022	19.354	19.691	20.033
%12177385.00	18.208	18.527	18.851	19.180	19.513	19.851
%12178045.00	18.042	18.358	18.678	19.003	19.333	19.667
%12178705.00	17.875	18.187	18.504	18.825	19.151	19.481
%12179365.00	17.706	18.015	18.327	18.645	18.967	19.294
%12180025.00	17.536	17.840	18.150	18.463	18.781	19.104
%12180685.00	17.364	17.665	17.970	18.280	18.594	18.913
%12181345.00	17.191	17.488	17.789	18.095	18.405	18.720
%12182005.00	17.016	17.309	17.607	17.908	18.214	18.525
%12182665.00	16.840	17.129	17.423	17.720	18.022	18.328
%12183325.00	16.663	16.948	17.238	17.531	17.829	18.130
%12183985.00	16.485	16.766	17.051	17.341	17.634	17.931
%12184645.00	16.305	16.583	16.864	17.149	17.438	17.730
%12185305.00	16.125	16.398	16.675	16.956	17.240	17.529
%12185965.00	15.944	16.213	16.486	16.762	17.042	17.326
%12186625.00	15.762	16.027	16.295	16.567	16.843	17.122
%12187285.00	15.579	15.840	16.104	16.372	16.642	16.917
%12187945.00	15.396	15.652	15.912	16.175	16.442	16.711
%12188605.00	15.212	15.464	15.720	15.978	16.240	16.505
%12189265.00	15.028	15.276	15.527	15.781	16.038	16.298
%12189925.00	14.843	15.087	15.333	15.583	15.836	16.091
%12190585.00	14.658	14.898	15.140	15.385	15.633	15.884
%12191245.00	14.473	14.708	14.946	15.187	15.430	15.676
%12191905.00	14.288	14.519	14.752	14.988	15.227	15.469
%12192565.00	14.102	14.329	14.558	14.790	15.024	15.261
%12193225.00	13.917	14.140	14.365	14.592	14.822	15.054
%12193885.00	13.732	13.950	14.171	14.394	14.619	14.847
%12194545.00	13.547	13.761	13.978	14.196	14.417	14.640
%12195205.00	13.363	13.573	13.785	13.999	14.215	14.434
%12195865.00	13.179	13.385	13.592	13.802	14.014	14.228
%12196525.00	12.995	13.197	13.401	13.606	13.814	14.023
%12197185.00	12.812	13.010	13.209	13.411	13.614	13.819
%12197845.00	12.629	12.823	13.019	13.216	13.415	13.616
%12198505.00	12.448	12.638	12.829	13.022	13.217	13.413

Y [ft]	<- X [ft] ->					
	1060912	1061572	1062232	1062892	1063552	1064212
%12153625.00	26.141	26.647	27.155	27.664	28.173	28.680
%12154285.00	25.972	26.465	26.961	27.457	27.953	28.447
%12154945.00	25.802	26.285	26.770	27.254	27.739	28.221

Y [ft] <- X [ft] ->

	1060912	1061572	1062232	1062892	1063552	1064212
%12155605.00	25.633	26.107	26.581	27.056	27.530	28.002
%12156265.00	25.466	25.930	26.395	26.861	27.326	27.789
%12156925.00	25.299	25.756	26.213	26.670	27.127	27.583
%12157585.00	25.134	25.583	26.033	26.484	26.934	27.382
%12158245.00	24.971	25.413	25.856	26.300	26.744	27.187
%12158905.00	24.808	25.245	25.682	26.121	26.559	26.997
%12159565.00	24.647	25.078	25.511	25.944	26.378	26.812
%12160225.00	24.488	24.914	25.341	25.770	26.200	26.630
%12160885.00	24.329	24.751	25.174	25.599	26.025	26.452
%12161545.00	24.171	24.589	25.008	25.430	25.853	26.277
%12162205.00	24.014	24.428	24.844	25.262	25.682	26.104
%12162865.00	23.858	24.268	24.681	25.097	25.514	25.933
%12163525.00	23.702	24.109	24.519	24.932	25.347	25.764
%12164185.00	23.546	23.950	24.358	24.768	25.181	25.596
%12164845.00	23.390	23.791	24.196	24.604	25.015	25.429
%12165505.00	23.234	23.632	24.035	24.441	24.850	25.262
%12166165.00	23.077	23.473	23.873	24.277	24.684	25.096
%12166825.00	22.919	23.313	23.711	24.113	24.519	24.928
%12167485.00	22.761	23.153	23.548	23.948	24.352	24.760
%12168145.00	22.602	22.991	23.384	23.782	24.184	24.591
%12168805.00	22.442	22.828	23.219	23.615	24.016	24.421
%12169465.00	22.280	22.664	23.053	23.447	23.845	24.249
%12170125.00	22.116	22.498	22.885	23.276	23.673	24.074
%12170785.00	21.952	22.331	22.715	23.104	23.499	23.898
%12171445.00	21.785	22.162	22.543	22.930	23.322	23.720
%12172105.00	21.616	21.990	22.369	22.754	23.143	23.539
%12172765.00	21.446	21.817	22.193	22.575	22.962	23.355
%12173425.00	21.273	21.642	22.015	22.394	22.779	23.169
%12174085.00	21.099	21.464	21.835	22.211	22.592	22.980
%12174745.00	20.922	21.284	21.652	22.025	22.403	22.788
%12175405.00	20.743	21.102	21.466	21.836	22.211	22.593
%12176065.00	20.562	20.918	21.279	21.645	22.017	22.395
%12176725.00	20.379	20.731	21.088	21.451	21.820	22.194
%12177385.00	20.194	20.542	20.896	21.255	21.619	21.990
%12178045.00	20.007	20.351	20.701	21.056	21.417	21.783
%12178705.00	19.817	20.158	20.503	20.855	21.211	21.573
%12179365.00	19.625	19.962	20.304	20.651	21.003	21.361
%12180025.00	19.432	19.764	20.102	20.444	20.792	21.146
%12180685.00	19.236	19.565	19.898	20.236	20.579	20.928
%12181345.00	19.039	19.363	19.692	20.025	20.364	20.708

Y [ft]	<- X [ft] ->					
	1060912	1061572	1062232	1062892	1063552	1064212
%12182005.00	18.840	19.159	19.483	19.812	20.146	20.485
%12182665.00	18.639	18.954	19.273	19.598	19.927	20.261
%12183325.00	18.436	18.747	19.062	19.381	19.705	20.034
%12183985.00	18.232	18.538	18.848	19.163	19.482	19.805
%12184645.00	18.027	18.328	18.633	18.943	19.256	19.575
%12185305.00	17.821	18.117	18.417	18.721	19.030	19.343
%12185965.00	17.613	17.904	18.199	18.499	18.802	19.109
%12186625.00	17.404	17.691	17.981	18.275	18.573	18.875
%12187285.00	17.195	17.476	17.761	18.050	18.342	18.639
%12187945.00	16.984	17.261	17.541	17.824	18.111	18.402
%12188605.00	16.773	17.045	17.320	17.598	17.880	18.165
%12189265.00	16.562	16.828	17.098	17.371	17.647	17.927
%12189925.00	16.350	16.611	16.876	17.144	17.414	17.688
%12190585.00	16.138	16.394	16.654	16.916	17.181	17.449
%12191245.00	15.925	16.177	16.431	16.688	16.948	17.211
%12191905.00	15.713	15.959	16.209	16.461	16.715	16.972
%12192565.00	15.500	15.742	15.986	16.233	16.482	16.734
%12193225.00	15.288	15.525	15.764	16.006	16.249	16.495
%12193885.00	15.076	15.308	15.542	15.779	16.017	16.258
%12194545.00	14.865	15.092	15.321	15.552	15.786	16.021
%12195205.00	14.654	14.876	15.101	15.327	15.555	15.785
%12195865.00	14.444	14.661	14.881	15.102	15.325	15.549
%12196525.00	14.234	14.447	14.662	14.878	15.096	15.315
%12197185.00	14.025	14.234	14.443	14.655	14.868	15.082
%12197845.00	13.818	14.021	14.226	14.433	14.641	14.850
%12198505.00	13.611	13.810	14.010	14.212	14.415	14.620

Y [ft]	<- X [ft] ->					
	1064872	1065532	1066192	1066852	1067512	1068172
%12153625.00	29.183	29.681	30.171	30.651	31.118	31.572
%12154285.00	28.937	29.422	29.899	30.368	30.825	31.269
%12154945.00	28.700	29.173	29.640	30.099	30.548	30.985
%12155605.00	28.471	28.935	29.393	29.844	30.286	30.718
%12156265.00	28.250	28.706	29.157	29.601	30.038	30.465
%12156925.00	28.036	28.485	28.930	29.369	29.802	30.227
%12157585.00	27.829	28.273	28.713	29.148	29.577	30.000
%12158245.00	27.629	28.068	28.504	28.935	29.362	29.784
%12158905.00	27.434	27.869	28.302	28.731	29.157	29.578
%12159565.00	27.245	27.676	28.106	28.534	28.958	29.380
%12160225.00	27.060	27.489	27.917	28.343	28.767	29.189
%12160885.00	26.879	27.306	27.732	28.157	28.581	29.004
%12161545.00	26.701	27.126	27.551	27.976	28.401	28.824
%12162205.00	26.526	26.950	27.374	27.799	28.224	28.649

Y [ft]	<- X [ft] ->					
	1064872	1065532	1066192	1066852	1067512	1068172
%12162865.00	26.354	26.777	27.200	27.625	28.051	28.477
%12163525.00	26.184	26.605	27.028	27.453	27.880	28.308
%12164185.00	26.015	26.435	26.858	27.283	27.711	28.140
%12164845.00	25.846	26.266	26.689	27.114	27.543	27.974
%12165505.00	25.678	26.097	26.520	26.946	27.375	27.808
%12166165.00	25.510	25.929	26.351	26.777	27.207	27.641
%12166825.00	25.342	25.760	26.182	26.608	27.038	27.473
%12167485.00	25.173	25.590	26.011	26.437	26.868	27.304
%12168145.00	25.002	25.419	25.839	26.265	26.697	27.133
%12168805.00	24.831	25.246	25.666	26.092	26.523	26.960
%12169465.00	24.657	25.071	25.490	25.915	26.346	26.784
%12170125.00	24.481	24.894	25.312	25.736	26.167	26.604
%12170785.00	24.304	24.715	25.131	25.555	25.984	26.421
%12171445.00	24.123	24.532	24.948	25.369	25.798	26.233
%12172105.00	23.940	24.347	24.761	25.181	25.608	26.042
%12172765.00	23.754	24.159	24.571	24.989	25.414	25.847
%12173425.00	23.565	23.968	24.377	24.793	25.216	25.646
%12174085.00	23.373	23.773	24.180	24.593	25.014	25.442
%12174745.00	23.178	23.575	23.979	24.389	24.807	25.232
%12175405.00	22.980	23.374	23.774	24.181	24.596	25.018
%12176065.00	22.779	23.169	23.566	23.970	24.381	24.799
%12176725.00	22.574	22.961	23.354	23.754	24.161	24.576
%12177385.00	22.366	22.749	23.138	23.534	23.937	24.348
%12178045.00	22.156	22.534	22.919	23.311	23.709	24.115
%12178705.00	21.942	22.316	22.696	23.084	23.477	23.878
%12179365.00	21.725	22.094	22.470	22.853	23.242	23.637
%12180025.00	21.505	21.870	22.241	22.618	23.002	23.392
%12180685.00	21.282	21.642	22.008	22.380	22.759	23.144
%12181345.00	21.057	21.412	21.773	22.139	22.512	22.891
%12182005.00	20.830	21.179	21.535	21.896	22.262	22.635
%12182665.00	20.600	20.944	21.294	21.649	22.010	22.376
%12183325.00	20.368	20.706	21.050	21.400	21.754	22.114
%12183985.00	20.133	20.467	20.805	21.148	21.496	21.850
%12184645.00	19.897	20.225	20.557	20.894	21.236	21.583
%12185305.00	19.660	19.982	20.308	20.639	20.974	21.314
%12185965.00	19.421	19.737	20.057	20.381	20.710	21.044
%12186625.00	19.180	19.490	19.804	20.122	20.445	20.771
%12187285.00	18.939	19.243	19.551	19.862	20.178	20.498
%12187945.00	18.696	18.994	19.296	19.601	19.910	20.223
%12188605.00	18.453	18.745	19.040	19.339	19.642	19.948

Y [ft]	<- X [ft] ->					
	1064872	1065532	1066192	1066852	1067512	1068172
%12189265.00	18.209	18.495	18.784	19.077	19.373	19.672
%12189925.00	17.965	18.245	18.528	18.814	19.103	19.396
%12190585.00	17.721	17.995	18.271	18.551	18.834	19.119
%12191245.00	17.476	17.744	18.015	18.288	18.564	18.843
%12191905.00	17.232	17.494	17.758	18.026	18.295	18.567
%12192565.00	16.987	17.244	17.502	17.763	18.026	18.292
%12193225.00	16.744	16.994	17.247	17.502	17.758	18.017
%12193885.00	16.501	16.745	16.992	17.241	17.491	17.743
%12194545.00	16.258	16.497	16.738	16.981	17.225	17.471
%12195205.00	16.016	16.250	16.485	16.722	16.960	17.200
%12195865.00	15.776	16.004	16.233	16.464	16.696	16.930
%12196525.00	15.536	15.759	15.982	16.207	16.434	16.661
%12197185.00	15.298	15.515	15.733	15.953	16.173	16.395
%12197845.00	15.061	15.272	15.485	15.699	15.914	16.130
%12198505.00	14.825	15.032	15.239	15.448	15.657	15.867

Y [ft]	<- X [ft] ->					
	1068832	1069492	1070152	1070812	1071472	1072132
%12153625.00	32.008	32.426	32.822	33.196	33.546	33.872
%12154285.00	31.698	32.111	32.505	32.880	33.233	33.566
%12154945.00	31.409	31.818	32.211	32.587	32.945	33.285
%12155605.00	31.138	31.545	31.938	32.317	32.679	33.026
%12156265.00	30.883	31.289	31.684	32.065	32.433	32.787
%12156925.00	30.643	31.049	31.445	31.830	32.204	32.566
%12157585.00	30.415	30.823	31.221	31.610	31.990	32.360
%12158245.00	30.199	30.608	31.010	31.404	31.789	32.167
%12158905.00	29.994	30.404	30.809	31.208	31.600	31.986
%12159565.00	29.797	30.210	30.618	31.022	31.421	31.815
%12160225.00	29.608	30.023	30.436	30.845	31.250	31.652
%12160885.00	29.425	29.843	30.260	30.674	31.086	31.496
%12161545.00	29.247	29.669	30.090	30.509	30.928	31.345
%12162205.00	29.074	29.499	29.924	30.349	30.774	31.199
%12162865.00	28.905	29.333	29.762	30.192	30.623	31.056
%12163525.00	28.738	29.169	29.602	30.037	30.475	30.914
%12164185.00	28.572	29.007	29.444	29.884	30.327	30.773
%12164845.00	28.408	28.846	29.287	29.731	30.179	30.632
%12165505.00	28.244	28.684	29.129	29.577	30.031	30.490
%12166165.00	28.079	28.522	28.970	29.423	29.881	30.345
%12166825.00	27.913	28.359	28.809	29.266	29.728	30.198
%12167485.00	27.746	28.193	28.646	29.106	29.572	30.046
%12168145.00	27.576	28.025	28.480	28.942	29.412	29.890
%12168805.00	27.403	27.853	28.310	28.775	29.248	29.729
%12169465.00	27.228	27.678	28.137	28.603	29.078	29.562

Y [ft] <- X [ft] ->

	1068832	1069492	1070152	1070812	1071472	1072132
%12170125.00	27.048	27.499	27.958	28.426	28.902	29.388
%12170785.00	26.864	27.316	27.775	28.243	28.721	29.208
%12171445.00	26.677	27.127	27.587	28.055	28.533	29.021
%12172105.00	26.484	26.934	27.393	27.861	28.338	28.826
%12172765.00	26.287	26.736	27.193	27.660	28.136	28.624
%12173425.00	26.085	26.532	26.987	27.452	27.928	28.413
%12174085.00	25.878	26.322	26.776	27.239	27.712	28.195
%12174745.00	25.666	26.107	26.558	27.018	27.488	27.969
%12175405.00	25.448	25.887	26.334	26.791	27.258	27.735
%12176065.00	25.226	25.661	26.104	26.557	27.020	27.493
%12176725.00	24.998	25.429	25.869	26.317	26.776	27.244
%12177385.00	24.766	25.192	25.627	26.071	26.524	26.987
%12178045.00	24.529	24.950	25.380	25.819	26.266	26.724
%12178705.00	24.287	24.703	25.128	25.560	26.002	26.453
%12179365.00	24.041	24.451	24.870	25.297	25.732	26.176
%12180025.00	23.790	24.195	24.607	25.028	25.456	25.894
%12180685.00	23.535	23.934	24.340	24.753	25.175	25.605
%12181345.00	23.277	23.669	24.068	24.475	24.889	25.311
%12182005.00	23.014	23.400	23.793	24.192	24.598	25.012
%12182665.00	22.749	23.128	23.513	23.905	24.304	24.709
%12183325.00	22.480	22.852	23.230	23.615	24.005	24.403
%12183985.00	22.209	22.574	22.945	23.321	23.704	24.092
%12184645.00	21.936	22.293	22.656	23.025	23.399	23.779
%12185305.00	21.660	22.010	22.365	22.726	23.092	23.463
%12185965.00	21.382	21.725	22.072	22.425	22.782	23.144
%12186625.00	21.102	21.438	21.778	22.122	22.471	22.824
%12187285.00	20.822	21.150	21.482	21.818	22.159	22.503
%12187945.00	20.540	20.860	21.185	21.513	21.845	22.181
%12188605.00	20.257	20.570	20.887	21.207	21.531	21.858
%12189265.00	19.974	20.280	20.589	20.901	21.216	21.535
%12189925.00	19.691	19.989	20.290	20.595	20.902	21.211
%12190585.00	19.407	19.698	19.992	20.288	20.587	20.889
%12191245.00	19.124	19.408	19.694	19.983	20.274	20.567
%12191905.00	18.841	19.118	19.397	19.678	19.961	20.245
%12192565.00	18.559	18.829	19.100	19.374	19.649	19.926
%12193225.00	18.278	18.540	18.805	19.071	19.338	19.607
%12193885.00	17.998	18.253	18.511	18.769	19.029	19.290
%12194545.00	17.718	17.967	18.218	18.469	18.722	18.976
%12195205.00	17.441	17.683	17.927	18.171	18.417	18.663
%12195865.00	17.164	17.400	17.637	17.875	18.113	18.352

Y [ft] <- X [ft] ->

	1068832	1069492	1070152	1070812	1071472	1072132
%12196525.00	16.890	17.119	17.350	17.581	17.812	18.044
%12197185.00	16.617	16.840	17.064	17.289	17.514	17.739
%12197845.00	16.346	16.564	16.781	16.999	17.218	17.436
%12198505.00	16.078	16.289	16.501	16.712	16.924	17.136

Y [ft] <- X [ft] ->

	1072792	1073452	1074112	1074772	1075432	1076092
%12153625.00	34.172	34.447	34.698	34.925	35.130	35.313
%12154285.00	33.876	34.164	34.432	34.678	34.905	35.113
%12154945.00	33.605	33.906	34.189	34.454	34.701	34.933
%12155605.00	33.356	33.670	33.968	34.250	34.518	34.771
%12156265.00	33.127	33.454	33.766	34.065	34.351	34.625
%12156925.00	32.916	33.254	33.580	33.896	34.200	34.494
%12157585.00	32.720	33.070	33.410	33.740	34.062	34.376
%12158245.00	32.537	32.898	33.252	33.598	33.936	34.268
%12158905.00	32.365	32.738	33.105	33.465	33.821	34.171
%12159565.00	32.204	32.587	32.967	33.342	33.713	34.081
%12160225.00	32.050	32.445	32.837	33.226	33.613	33.997
%12160885.00	31.903	32.309	32.713	33.116	33.517	33.919
%12161545.00	31.762	32.178	32.594	33.010	33.426	33.844
%12162205.00	31.624	32.050	32.478	32.906	33.337	33.770
%12162865.00	31.490	31.925	32.364	32.805	33.249	33.697
%12163525.00	31.356	31.802	32.250	32.703	33.161	33.623
%12164185.00	31.223	31.678	32.137	32.601	33.071	33.547
%12164845.00	31.090	31.552	32.021	32.496	32.978	33.467
%12165505.00	30.954	31.425	31.902	32.387	32.880	33.382
%12166165.00	30.816	31.294	31.780	32.274	32.777	33.291
%12166825.00	30.674	31.159	31.652	32.155	32.668	33.192
%12167485.00	30.528	31.019	31.519	32.030	32.551	33.085
%12168145.00	30.377	30.873	31.379	31.896	32.426	32.968
%12168805.00	30.220	30.720	31.232	31.755	32.291	32.841
%12169465.00	30.056	30.560	31.076	31.604	32.146	32.702
%12170125.00	29.885	30.392	30.911	31.444	31.990	32.551
%12170785.00	29.706	30.216	30.738	31.273	31.822	32.387
%12171445.00	29.520	30.031	30.554	31.091	31.643	32.210
%12172105.00	29.325	29.836	30.360	30.898	31.451	32.020
%12172765.00	29.122	29.633	30.156	30.694	31.247	31.816
%12173425.00	28.910	29.420	29.942	30.479	31.030	31.598
%12174085.00	28.690	29.197	29.717	30.252	30.801	31.366
%12174745.00	28.461	28.965	29.482	30.013	30.559	31.120
%12175405.00	28.224	28.724	29.237	29.764	30.305	30.862
%12176065.00	27.978	28.474	28.982	29.503	30.039	30.590
%12176725.00	27.723	28.214	28.717	29.233	29.762	30.306

Y [ft]	<- X [ft] ->					
	1072792	1073452	1074112	1074772	1075432	1076092
%12177385.00	27.461	27.946	28.443	28.952	29.474	30.010
%12178045.00	27.191	27.670	28.159	28.661	29.175	29.703
%12178705.00	26.914	27.386	27.868	28.361	28.867	29.385
%12179365.00	26.630	27.094	27.568	28.053	28.550	29.058
%12180025.00	26.340	26.796	27.261	27.737	28.224	28.722
%12180685.00	26.043	26.491	26.947	27.414	27.890	28.377
%12181345.00	25.741	26.180	26.627	27.084	27.550	28.025
%12182005.00	25.434	25.864	26.302	26.748	27.203	27.667
%12182665.00	25.122	25.543	25.971	26.407	26.851	27.303
%12183325.00	24.807	25.218	25.636	26.061	26.494	26.934
%12183985.00	24.487	24.888	25.296	25.711	26.132	26.561
%12184645.00	24.164	24.556	24.954	25.358	25.768	26.184
%12185305.00	23.839	24.221	24.609	25.002	25.400	25.804
%12185965.00	23.512	23.884	24.261	24.643	25.031	25.423
%12186625.00	23.182	23.545	23.912	24.284	24.660	25.040
%12187285.00	22.852	23.205	23.562	23.922	24.287	24.656
%12187945.00	22.520	22.864	23.210	23.561	23.915	24.272
%12188605.00	22.188	22.522	22.859	23.199	23.542	23.888
%12189265.00	21.856	22.180	22.507	22.837	23.170	23.504
%12189925.00	21.524	21.839	22.156	22.476	22.798	23.122
%12190585.00	21.192	21.498	21.806	22.116	22.428	22.741
%12191245.00	20.862	21.159	21.457	21.758	22.060	22.363
%12191905.00	20.532	20.820	21.110	21.401	21.693	21.986
%12192565.00	20.204	20.484	20.764	21.046	21.329	21.612
%12193225.00	19.877	20.149	20.421	20.694	20.967	21.241
%12193885.00	19.553	19.816	20.079	20.344	20.608	20.873
%12194545.00	19.230	19.485	19.741	19.996	20.252	20.508
%12195205.00	18.910	19.157	19.405	19.652	19.900	20.147
%12195865.00	18.592	18.832	19.071	19.311	19.550	19.789
%12196525.00	18.277	18.509	18.741	18.973	19.204	19.435
%12197185.00	17.964	18.189	18.414	18.639	18.862	19.085
%12197845.00	17.655	17.873	18.091	18.308	18.524	18.740
%12198505.00	17.348	17.560	17.771	17.981	18.190	18.398

Y [ft]	<- X [ft] ->					
	1076752	1077412	1078072	1078732	1079392	1080052
%12153625.00	35.478	35.626	35.759	35.878	35.986	36.083
%12154285.00	35.305	35.481	35.643	35.793	35.932	36.063
%12154945.00	35.149	35.352	35.543	35.722	35.892	36.053
%12155605.00	35.011	35.239	35.457	35.664	35.863	36.054
%12156265.00	34.888	35.141	35.384	35.618	35.845	36.065
%12156925.00	34.779	35.054	35.322	35.583	35.837	36.086
%12157585.00	34.681	34.980	35.272	35.558	35.839	36.115

Y [ft]	<- X [ft] ->					
	1076752	1077412	1078072	1078732	1079392	1080052
%12158245.00	34.594	34.915	35.230	35.541	35.848	36.152
%12158905.00	34.516	34.858	35.196	35.531	35.863	36.194
%12159565.00	34.445	34.808	35.168	35.527	35.884	36.242
%12160225.00	34.381	34.763	35.145	35.527	35.909	36.293
%12160885.00	34.320	34.722	35.125	35.530	35.937	36.346
%12161545.00	34.263	34.684	35.107	35.534	35.965	36.400
%12162205.00	34.206	34.646	35.090	35.539	35.993	36.452
%12162865.00	34.150	34.608	35.071	35.541	36.018	36.502
%12163525.00	34.092	34.567	35.049	35.540	36.039	36.547
%12164185.00	34.031	34.523	35.023	35.533	36.054	36.586
%12164845.00	33.965	34.473	34.991	35.520	36.061	36.616
%12165505.00	33.894	34.417	34.951	35.498	36.059	36.635
%12166165.00	33.816	34.352	34.902	35.466	36.046	36.642
%12166825.00	33.729	34.278	34.842	35.422	36.019	36.635
%12167485.00	33.632	34.194	34.771	35.365	35.978	36.611
%12168145.00	33.525	34.097	34.686	35.293	35.920	36.569
%12168805.00	33.406	33.987	34.586	35.205	35.844	36.507
%12169465.00	33.274	33.863	34.471	35.099	35.749	36.424
%12170125.00	33.129	33.724	34.339	34.975	35.634	36.319
%12170785.00	32.969	33.570	34.190	34.832	35.498	36.189
%12171445.00	32.795	33.399	34.023	34.669	35.339	36.036
%12172105.00	32.606	33.212	33.838	34.486	35.158	35.857
%12172765.00	32.402	33.008	33.634	34.282	34.955	35.654
%12173425.00	32.183	32.787	33.411	34.058	34.729	35.426
%12174085.00	31.948	32.550	33.171	33.814	34.481	35.173
%12174745.00	31.699	32.296	32.912	33.550	34.211	34.897
%12175405.00	31.435	32.026	32.636	33.267	33.920	34.597
%12176065.00	31.157	31.741	32.344	32.966	33.610	34.276
%12176725.00	30.865	31.441	32.035	32.648	33.280	33.934
%12177385.00	30.561	31.128	31.712	32.313	32.933	33.574
%12178045.00	30.245	30.801	31.374	31.963	32.570	33.196
%12178705.00	29.917	30.463	31.023	31.600	32.192	32.802
%12179365.00	29.579	30.113	30.661	31.223	31.801	32.394
%12180025.00	29.231	29.753	30.288	30.836	31.398	31.974
%12180685.00	28.875	29.384	29.905	30.438	30.984	31.543
%12181345.00	28.511	29.007	29.514	30.032	30.561	31.102
%12182005.00	28.140	28.623	29.116	29.618	30.131	30.653
%12182665.00	27.764	28.233	28.711	29.198	29.694	30.198
%12183325.00	27.382	27.838	28.301	28.772	29.252	29.738
%12183985.00	26.996	27.438	27.887	28.343	28.805	29.275

Y [ft]	<- X [ft] ->					
	1076752	1077412	1078072	1078732	1079392	1080052
%12184645.00	26.606	27.035	27.469	27.910	28.356	28.808
%12185305.00	26.214	26.629	27.049	27.475	27.905	28.340
%12185965.00	25.820	26.222	26.628	27.038	27.453	27.871
%12186625.00	25.424	25.813	26.205	26.601	27.001	27.403
%12187285.00	25.028	25.404	25.783	26.164	26.549	26.935
%12187945.00	24.632	24.995	25.360	25.728	26.098	26.470
%12188605.00	24.236	24.587	24.939	25.294	25.650	26.006
%12189265.00	23.841	24.180	24.520	24.861	25.203	25.546
%12189925.00	23.448	23.774	24.102	24.431	24.760	25.089
%12190585.00	23.056	23.371	23.688	24.004	24.320	24.636
%12191245.00	22.666	22.971	23.276	23.580	23.884	24.188
%12191905.00	22.279	22.573	22.867	23.160	23.453	23.744
%12192565.00	21.895	22.179	22.462	22.744	23.025	23.305
%12193225.00	21.514	21.788	22.060	22.332	22.603	22.871
%12193885.00	21.137	21.401	21.663	21.925	22.185	22.443
%12194545.00	20.763	21.017	21.270	21.522	21.772	22.020
%12195205.00	20.393	20.638	20.882	21.125	21.365	21.603
%12195865.00	20.027	20.263	20.498	20.732	20.963	21.192
%12196525.00	19.665	19.893	20.119	20.344	20.567	20.786
%12197185.00	19.307	19.527	19.745	19.962	20.176	20.387
%12197845.00	18.953	19.166	19.376	19.585	19.791	19.994
%12198505.00	18.605	18.810	19.012	19.213	19.411	19.607

Y [ft]	<- X [ft] ->					
	1080712	1081372	1082032	1082692	1083352	1084012
%12153625.00	36.173	36.255	36.331	36.401	36.467	36.527
%12154285.00	36.184	36.299	36.408	36.511	36.609	36.701
%12154945.00	36.206	36.353	36.494	36.629	36.759	36.884
%12155605.00	36.238	36.416	36.588	36.755	36.917	37.074
%12156265.00	36.280	36.488	36.692	36.890	37.084	37.273
%12156925.00	36.330	36.568	36.803	37.033	37.259	37.481
%12157585.00	36.388	36.656	36.921	37.183	37.442	37.696
%12158245.00	36.452	36.751	37.047	37.340	37.631	37.919
%12158905.00	36.523	36.851	37.178	37.503	37.827	38.149
%12159565.00	36.599	36.956	37.313	37.670	38.028	38.385
%12160225.00	36.678	37.064	37.452	37.841	38.233	38.625
%12160885.00	36.758	37.174	37.592	38.014	38.440	38.868
%12161545.00	36.839	37.284	37.733	38.188	38.648	39.112
%12162205.00	36.919	37.392	37.872	38.360	38.854	39.356
%12162865.00	36.995	37.497	38.007	38.528	39.058	39.597
%12163525.00	37.066	37.596	38.137	38.690	39.255	39.833
%12164185.00	37.130	37.687	38.258	38.844	39.444	40.060
%12164845.00	37.185	37.768	38.369	38.986	39.621	40.275

Y [ft]	<- X [ft] ->					
	1080712	1081372	1082032	1082692	1083352	1084012
%12165505.00	37.228	37.837	38.466	39.114	39.784	40.475
%12166165.00	37.257	37.891	38.547	39.225	39.928	40.656
%12166825.00	37.270	37.928	38.609	39.316	40.050	40.814
%12167485.00	37.266	37.945	38.650	39.383	40.147	40.944
%12168145.00	37.242	37.940	38.667	39.424	40.215	41.043
%12168805.00	37.195	37.911	38.657	39.436	40.251	41.106
%12169465.00	37.125	37.856	38.618	39.415	40.251	41.130
%12170125.00	37.031	37.773	38.548	39.361	40.213	41.111
%12170785.00	36.910	37.661	38.446	39.270	40.135	41.047
%12171445.00	36.761	37.519	38.311	39.142	40.015	40.936
%12172105.00	36.586	37.346	38.141	38.975	39.852	40.777
%12172765.00	36.382	37.142	37.937	38.770	39.646	40.569
%12173425.00	36.151	36.908	37.699	38.528	39.398	40.313
%12174085.00	35.893	36.644	37.428	38.248	39.108	40.012
%12174745.00	35.609	36.351	37.125	37.933	38.779	39.667
%12175405.00	35.300	36.030	36.791	37.585	38.414	39.281
%12176065.00	34.967	35.684	36.429	37.205	38.014	38.858
%12176725.00	34.612	35.313	36.041	36.797	37.583	38.402
%12177385.00	34.236	34.921	35.629	36.364	37.125	37.916
%12178045.00	33.841	34.508	35.196	35.908	36.643	37.404
%12178705.00	33.430	34.077	34.744	35.431	36.140	36.871
%12179365.00	33.004	33.631	34.275	34.938	35.619	36.319
%12180025.00	32.565	33.171	33.793	34.430	35.084	35.753
%12180685.00	32.114	32.699	33.298	33.910	34.536	35.176
%12181345.00	31.654	32.218	32.794	33.381	33.980	34.590
%12182005.00	31.186	31.729	32.282	32.845	33.417	33.998
%12182665.00	30.712	31.234	31.765	32.303	32.849	33.402
%12183325.00	30.233	30.734	31.243	31.758	32.278	32.804
%12183985.00	29.750	30.232	30.719	31.211	31.707	32.207
%12184645.00	29.265	29.727	30.193	30.663	31.136	31.611
%12185305.00	28.779	29.222	29.668	30.117	30.567	31.018
%12185965.00	28.293	28.717	29.144	29.572	30.001	30.429
%12186625.00	27.807	28.214	28.622	29.030	29.439	29.846
%12187285.00	27.323	27.713	28.103	28.493	28.881	29.268
%12187945.00	26.842	27.215	27.588	27.959	28.330	28.697
%12188605.00	26.363	26.720	27.077	27.432	27.784	28.134
%12189265.00	25.889	26.230	26.571	26.909	27.245	27.578
%12189925.00	25.418	25.745	26.070	26.394	26.714	27.030
%12190585.00	24.951	25.265	25.576	25.884	26.189	26.490
%12191245.00	24.490	24.790	25.087	25.382	25.673	25.959

Y [ft]	<- X [ft] ->					
	1080712	1081372	1082032	1082692	1083352	1084012
%12191905.00	24.033	24.321	24.605	24.887	25.164	25.436
%12192565.00	23.583	23.858	24.130	24.399	24.663	24.923
%12193225.00	23.138	23.401	23.662	23.918	24.171	24.418
%12193885.00	22.698	22.951	23.200	23.446	23.687	23.922
%12194545.00	22.265	22.507	22.746	22.981	23.211	23.436
%12195205.00	21.838	22.070	22.299	22.523	22.743	22.958
%12195865.00	21.418	21.640	21.859	22.074	22.284	22.489
%12196525.00	21.003	21.217	21.427	21.632	21.833	22.029
%12197185.00	20.595	20.800	21.001	21.198	21.390	21.577
%12197845.00	20.194	20.391	20.583	20.772	20.956	21.134
%12198505.00	19.799	19.988	20.173	20.353	20.529	20.700

Y [ft]	<- X [ft] ->					
	1084672	1085332	1085992	1086652	1087312	1087972
%12153625.00	36.584	36.635	36.682	36.723	36.758	36.786
%12154285.00	36.789	36.872	36.949	37.020	37.084	37.140
%12154945.00	37.003	37.117	37.225	37.327	37.421	37.507
%12155605.00	37.226	37.372	37.512	37.645	37.770	37.886
%12156265.00	37.458	37.636	37.808	37.974	38.131	38.279
%12156925.00	37.698	37.910	38.116	38.314	38.505	38.686
%12157585.00	37.947	38.193	38.433	38.667	38.892	39.108
%12158245.00	38.204	38.485	38.761	39.030	39.292	39.544
%12158905.00	38.469	38.786	39.098	39.405	39.705	39.996
%12159565.00	38.740	39.094	39.445	39.791	40.131	40.462
%12160225.00	39.017	39.409	39.800	40.187	40.568	40.943
%12160885.00	39.298	39.730	40.161	40.591	41.017	41.438
%12161545.00	39.581	40.054	40.528	41.003	41.476	41.945
%12162205.00	39.865	40.379	40.898	41.420	41.943	42.464
%12162865.00	40.146	40.704	41.269	41.840	42.415	42.992
%12163525.00	40.423	41.025	41.638	42.260	42.891	43.526
%12164185.00	40.691	41.339	42.001	42.677	43.365	44.063
%12164845.00	40.949	41.641	42.354	43.085	43.834	44.598
%12165505.00	41.190	41.929	42.692	43.480	44.292	45.126
%12166165.00	41.412	42.196	43.010	43.855	44.731	45.638
%12166825.00	41.609	42.438	43.302	44.204	45.145	46.126
%12167485.00	41.777	42.648	43.561	44.519	45.524	46.580
%12168145.00	41.910	42.821	43.780	44.791	45.858	46.987
%12168805.00	42.005	42.952	43.952	45.012	46.137	47.334
%12169465.00	42.056	43.034	44.071	45.173	46.349	47.607
%12170125.00	42.059	43.062	44.129	45.266	46.483	47.793
%12170785.00	42.011	43.033	44.122	45.284	46.533	47.880
%12171445.00	41.910	42.944	44.045	45.223	46.490	47.858
%12172105.00	41.755	42.792	43.898	45.080	46.351	47.725

Y [ft]	<- X [ft] ->					
	1084672	1085332	1085992	1086652	1087312	1087972
%12172765.00	41.544	42.579	43.679	44.855	46.117	47.478
%12173425.00	41.280	42.304	43.391	44.550	45.790	47.123
%12174085.00	40.964	41.971	43.037	44.170	45.377	46.669
%12174745.00	40.600	41.583	42.621	43.720	44.886	46.127
%12175405.00	40.191	41.146	42.151	43.210	44.327	45.509
%12176065.00	39.740	40.664	41.631	42.646	43.711	44.829
%12176725.00	39.254	40.143	41.070	42.037	43.047	44.100
%12177385.00	38.736	39.588	40.473	41.392	42.345	43.333
%12178045.00	38.191	39.006	39.848	40.718	41.615	42.538
%12178705.00	37.624	38.400	39.199	40.021	40.863	41.725
%12179365.00	37.039	37.777	38.533	39.308	40.097	40.901
%12180025.00	36.439	37.140	37.855	38.583	39.323	40.071
%12180685.00	35.828	36.492	37.168	37.852	38.545	39.241
%12181345.00	35.210	35.839	36.476	37.119	37.766	38.415
%12182005.00	34.586	35.181	35.782	36.386	36.991	37.595
%12182665.00	33.960	34.523	35.089	35.656	36.222	36.785
%12183325.00	33.333	33.866	34.399	34.931	35.461	35.985
%12183985.00	32.708	33.211	33.714	34.214	34.710	35.199
%12184645.00	32.086	32.562	33.035	33.505	33.969	34.426
%12185305.00	31.469	31.918	32.364	32.806	33.241	33.667
%12185965.00	30.857	31.281	31.702	32.117	32.525	32.924
%12186625.00	30.251	30.652	31.049	31.440	31.823	32.196
%12187285.00	29.652	30.032	30.407	30.774	31.134	31.483
%12187945.00	29.061	29.421	29.774	30.121	30.459	30.786
%12188605.00	28.479	28.819	29.153	29.480	29.798	30.105
%12189265.00	27.905	28.228	28.543	28.851	29.150	29.439
%12189925.00	27.341	27.646	27.945	28.236	28.517	28.789
%12190585.00	26.785	27.075	27.358	27.632	27.898	28.154
%12191245.00	26.240	26.514	26.782	27.042	27.292	27.533
%12191905.00	25.703	25.964	26.218	26.463	26.700	26.927
%12192565.00	25.177	25.424	25.665	25.898	26.121	26.336
%12193225.00	24.660	24.895	25.123	25.344	25.556	25.758
%12193885.00	24.152	24.376	24.593	24.802	25.003	25.194
%12194545.00	23.655	23.868	24.074	24.272	24.462	24.643
%12195205.00	23.167	23.369	23.565	23.753	23.934	24.105
%12195865.00	22.688	22.881	23.067	23.246	23.417	23.580
%12196525.00	22.219	22.403	22.580	22.750	22.913	23.067
%12197185.00	21.759	21.934	22.103	22.265	22.419	22.566
%12197845.00	21.308	21.475	21.636	21.790	21.937	22.076
%12198505.00	20.866	21.026	21.179	21.326	21.466	21.598

Y [ft]	<- X [ft] ->					
	1088632	1089292	1089952	1090612	1091272	1091932

Y [ft] <- X [ft] ->

	1088632	1089292	1089952	1090612	1091272	1091932
%12153625.00	36.806	36.817	36.819	36.810	36.789	36.755
%12154285.00	37.188	37.226	37.253	37.268	37.270	37.257
%12154945.00	37.583	37.649	37.703	37.743	37.769	37.779
%12155605.00	37.992	38.087	38.169	38.237	38.288	38.322
%12156265.00	38.416	38.542	38.653	38.749	38.828	38.888
%12156925.00	38.856	39.014	39.156	39.283	39.391	39.478
%12157585.00	39.312	39.504	39.680	39.838	39.977	40.094
%12158245.00	39.785	40.013	40.224	40.418	40.590	40.739
%12158905.00	40.275	40.541	40.791	41.021	41.230	41.413
%12159565.00	40.783	41.090	41.380	41.651	41.899	42.120
%12160225.00	41.307	41.659	41.994	42.308	42.599	42.862
%12160885.00	41.849	42.248	42.631	42.994	43.331	43.640
%12161545.00	42.407	42.857	43.293	43.708	44.098	44.456
%12162205.00	42.980	43.486	43.979	44.452	44.900	45.315
%12162865.00	43.566	44.133	44.689	45.226	45.738	46.217
%12163525.00	44.163	44.797	45.422	46.030	46.615	47.166
%12164185.00	44.768	45.473	46.175	46.863	47.530	48.164
%12164845.00	45.375	46.159	46.945	47.723	48.484	49.213
%12165505.00	45.980	46.849	47.727	48.606	49.473	50.313
%12166165.00	46.573	47.534	48.515	49.506	50.496	51.466
%12166825.00	47.147	48.205	49.296	50.414	51.544	52.667
%12167485.00	47.687	48.847	50.058	51.314	52.605	53.910
%12168145.00	48.181	49.444	50.780	52.186	53.657	55.177
%12168805.00	48.611	49.976	51.436	52.999	54.667	56.434
%12169465.00	48.959	50.418	51.998	53.715	55.586	57.623
%12170125.00	49.208	50.747	52.431	54.286	56.346	58.654
%12170785.00	49.342	50.940	52.701	54.662	56.873	59.403
%12171445.00	49.347	50.979	52.784	54.804	57.097	59.752
%12172105.00	49.218	50.855	52.664	54.687	56.982	59.632
%12172765.00	48.954	50.567	52.342	54.315	56.532	59.056
%12173425.00	48.563	50.127	51.835	53.712	55.791	58.106
%12174085.00	48.056	49.551	51.167	52.920	54.826	56.896
%12174745.00	47.449	48.861	50.371	51.986	53.708	55.532
%12175405.00	46.758	48.081	49.478	50.951	52.495	54.096
%12176065.00	46.002	47.232	48.517	49.854	51.233	52.638
%12176725.00	45.196	46.334	47.512	48.722	49.954	51.190
%12177385.00	44.353	45.404	46.481	47.575	48.676	49.769
%12178045.00	43.486	44.454	45.437	46.428	47.415	48.385
%12178705.00	42.604	43.495	44.393	45.290	46.177	47.041
%12179365.00	41.715	42.535	43.356	44.170	44.968	45.741

Y [ft]	<- X [ft] ->					
	1088632	1089292	1089952	1090612	1091272	1091932
%12180025.00	40.825	41.580	42.331	43.070	43.791	44.485
%12180685.00	39.939	40.635	41.322	41.995	42.648	43.272
%12181345.00	39.062	39.702	40.333	40.947	41.539	42.102
%12182005.00	38.195	38.786	39.365	39.926	40.464	40.974
%12182665.00	37.341	37.887	38.419	38.933	39.423	39.886
%12183325.00	36.502	37.007	37.497	37.968	38.416	38.836
%12183985.00	35.679	36.146	36.598	37.031	37.441	37.824
%12184645.00	34.872	35.305	35.723	36.121	36.497	36.848
%12185305.00	34.083	34.485	34.871	35.239	35.584	35.905
%12185965.00	33.311	33.685	34.043	34.382	34.700	34.995
%12186625.00	32.557	32.905	33.237	33.551	33.845	34.116
%12187285.00	31.821	32.145	32.454	32.745	33.016	33.266
%12187945.00	31.102	31.405	31.692	31.962	32.213	32.444
%12188605.00	30.401	30.683	30.951	31.202	31.435	31.648
%12189265.00	29.717	29.981	30.231	30.464	30.681	30.878
%12189925.00	29.049	29.297	29.530	29.748	29.949	30.133
%12190585.00	28.398	28.630	28.848	29.052	29.240	29.410
%12191245.00	27.763	27.981	28.185	28.376	28.551	28.710
%12191905.00	27.144	27.348	27.540	27.719	27.882	28.030
%12192565.00	26.540	26.732	26.912	27.080	27.233	27.371
%12193225.00	25.950	26.132	26.301	26.458	26.601	26.731
%12193885.00	25.376	25.546	25.706	25.853	25.988	26.109
%12194545.00	24.815	24.976	25.126	25.265	25.391	25.505
%12195205.00	24.268	24.420	24.562	24.692	24.811	24.918
%12195865.00	23.734	23.878	24.012	24.135	24.247	24.347
%12196525.00	23.213	23.349	23.475	23.592	23.697	23.791
%12197185.00	22.704	22.833	22.953	23.062	23.162	23.251
%12197845.00	22.207	22.330	22.443	22.547	22.641	22.724
%12198505.00	21.723	21.839	21.946	22.044	22.133	22.212

Y [ft]	<- X [ft] ->					
	1092592	1093252	1093912	1094572	1095232	1095892
%12153625.00	36.706	36.643	36.563	36.466	36.351	36.217
%12154285.00	37.229	37.184	37.120	37.038	36.936	36.813
%12154945.00	37.772	37.746	37.701	37.634	37.546	37.434
%12155605.00	38.338	38.333	38.306	38.256	38.182	38.083
%12156265.00	38.927	38.944	38.938	38.905	38.847	38.760
%12156925.00	39.543	39.584	39.599	39.586	39.543	39.471
%12157585.00	40.187	40.254	40.291	40.299	40.274	40.216
%12158245.00	40.862	40.956	41.019	41.048	41.043	41.001
%12158905.00	41.569	41.693	41.783	41.837	41.852	41.827
%12159565.00	42.311	42.469	42.589	42.669	42.707	42.700
%12160225.00	43.092	43.285	43.439	43.548	43.611	43.624

Y [ft] <- X [ft] ->

	1092592	1093252	1093912	1094572	1095232	1095892
%12160885.00	43.913	44.147	44.337	44.479	44.568	44.603
%12161545.00	44.778	45.057	45.288	45.466	45.586	45.645
%12162205.00	45.691	46.021	46.298	46.516	46.670	46.756
%12162865.00	46.655	47.043	47.372	47.636	47.828	47.943
%12163525.00	47.674	48.128	48.517	48.833	49.068	49.217
%12164185.00	48.753	49.283	49.742	50.118	50.402	50.587
%12164845.00	49.896	50.516	51.056	51.502	51.842	52.067
%12165505.00	51.107	51.834	52.472	53.001	53.404	53.673
%12166165.00	52.393	53.250	54.006	54.634	55.110	55.425
%12166825.00	53.756	54.774	55.679	56.428	56.990	57.350
%12167485.00	55.198	56.421	57.517	58.423	59.084	59.483
%12168145.00	56.711	58.202	59.562	60.679	61.461	61.875
%12168805.00	58.274	60.125	61.864	63.299	64.234	64.607
%12169465.00	59.828	62.161	64.483	66.466	67.629	67.801
%12170125.00	61.256	64.193	67.427	70.535	72.175	71.634
%12170785.00	62.359	65.910	70.343	76.061	79.688	76.017
%12171445.00	62.909	66.813	71.969	79.863	88.036	78.681
%12172105.00	62.768	66.603	71.474	77.624	81.411	77.857
%12172765.00	61.976	65.413	69.531	74.700	79.566	75.411
%12173425.00	60.696	63.585	66.741	69.886	71.797	71.574
%12174085.00	59.128	61.489	63.865	65.984	67.405	67.960
%12174745.00	57.437	59.371	61.229	62.849	64.057	64.811
%12175405.00	55.725	57.333	58.845	60.169	61.226	61.997
%12176065.00	54.040	55.401	56.668	57.785	58.710	59.431
%12176725.00	52.407	53.574	54.655	55.613	56.420	57.065
%12177385.00	50.834	51.845	52.777	53.605	54.308	54.873
%12178045.00	49.321	50.205	51.016	51.734	52.345	52.836
%12178705.00	47.869	48.646	49.355	49.982	50.513	50.938
%12179365.00	46.477	47.162	47.786	48.334	48.797	49.164
%12180025.00	45.141	45.749	46.299	46.781	47.185	47.503
%12180685.00	43.859	44.401	44.888	45.312	45.666	45.942
%12181345.00	42.629	43.113	43.546	43.922	44.233	44.473
%12182005.00	41.448	41.882	42.269	42.602	42.876	43.086
%12182665.00	40.315	40.705	41.050	41.347	41.590	41.774
%12183325.00	39.225	39.577	39.887	40.152	40.367	40.529
%12183985.00	38.177	38.495	38.775	39.012	39.204	39.347
%12184645.00	37.169	37.458	37.710	37.923	38.094	38.221
%12185305.00	36.198	36.461	36.689	36.882	37.035	37.147
%12185965.00	35.263	35.502	35.710	35.884	36.021	36.121
%12186625.00	34.361	34.580	34.769	34.926	35.050	35.139

Y [ft] <- X [ft] ->

	1092592	1093252	1093912	1094572	1095232	1095892
%12187285.00	33.491	33.692	33.864	34.007	34.119	34.198
%12187945.00	32.652	32.835	32.993	33.123	33.224	33.295
%12188605.00	31.840	32.009	32.153	32.272	32.364	32.427
%12189265.00	31.056	31.211	31.344	31.452	31.536	31.593
%12189925.00	30.297	30.440	30.562	30.662	30.738	30.789
%12190585.00	29.562	29.695	29.808	29.899	29.968	30.014
%12191245.00	28.851	28.974	29.078	29.162	29.225	29.267
%12191905.00	28.162	28.276	28.372	28.449	28.507	28.545
%12192565.00	27.493	27.599	27.688	27.760	27.813	27.847
%12193225.00	26.845	26.944	27.026	27.092	27.141	27.171
%12193885.00	26.216	26.308	26.385	26.445	26.490	26.518
%12194545.00	25.605	25.691	25.762	25.819	25.859	25.885
%12195205.00	25.011	25.092	25.158	25.210	25.248	25.271
%12195865.00	24.435	24.510	24.572	24.620	24.655	24.676
%12196525.00	23.874	23.944	24.002	24.047	24.079	24.098
%12197185.00	23.328	23.394	23.449	23.491	23.520	23.537
%12197845.00	22.797	22.860	22.910	22.949	22.977	22.992
%12198505.00	22.281	22.339	22.387	22.423	22.449	22.463

Y [ft] <- X [ft] ->

	1096552	1097212	1097872	1098532	1099192	1099852
%12153625.00	36.065	35.893	35.701	35.489	35.258	35.007
%12154285.00	36.670	36.504	36.317	36.108	35.877	35.625
%12154945.00	37.300	37.142	36.959	36.753	36.523	36.269
%12155605.00	37.958	37.807	37.629	37.425	37.195	36.939
%12156265.00	38.646	38.503	38.330	38.128	37.898	37.639
%12156925.00	39.367	39.232	39.064	38.864	38.633	38.370
%12157585.00	40.124	39.997	39.834	39.636	39.403	39.136
%12158245.00	40.920	40.802	40.644	40.447	40.212	39.939
%12158905.00	41.760	41.650	41.497	41.301	41.063	40.783
%12159565.00	42.647	42.546	42.398	42.202	41.960	41.672
%12160225.00	43.585	43.495	43.351	43.155	42.907	42.609
%12160885.00	44.581	44.501	44.362	44.165	43.910	43.599
%12161545.00	45.641	45.572	45.437	45.237	44.973	44.648
%12162205.00	46.771	46.713	46.582	46.378	46.104	45.761
%12162865.00	47.979	47.933	47.805	47.597	47.309	46.946
%12163525.00	49.275	49.241	49.115	48.900	48.596	48.208
%12164185.00	50.669	50.647	50.522	50.297	49.974	49.558
%12164845.00	52.174	52.163	52.037	51.799	51.453	51.003
%12165505.00	53.804	53.802	53.670	53.416	53.044	52.557
%12166165.00	55.578	55.577	55.435	55.159	54.757	54.230
%12166825.00	57.515	57.504	57.339	57.038	56.606	56.038
%12167485.00	59.638	59.592	59.389	59.056	58.598	57.999

Y [ft]	<- X [ft] ->					
	1096552	1097212	1097872	1098532	1099192	1099852
%12168145.00	61.973	61.846	61.576	61.208	60.741	60.138
%12168805.00	64.545	64.248	63.865	63.462	63.029	62.487
%12169465.00	67.355	66.735	66.175	65.747	65.428	65.096
%12170125.00	70.313	69.151	68.352	67.920	67.825	67.990
%12170785.00	73.025	71.195	70.169	69.766	69.937	70.866
%12171445.00	74.636	72.471	71.393	71.076	71.387	72.446
%12172105.00	74.605	72.727	71.885	71.797	72.183	72.766
%12172765.00	73.181	71.975	71.624	72.036	72.838	72.986
%12173425.00	70.812	70.385	70.580	71.701	74.376	73.825
%12174085.00	68.058	68.185	68.679	69.902	72.546	71.736
%12174745.00	65.260	65.632	66.119	66.804	67.393	66.834
%12175405.00	62.545	62.966	63.334	63.623	63.640	63.093
%12176065.00	59.967	60.355	60.611	60.703	60.536	60.011
%12176725.00	57.549	57.881	58.057	58.054	57.827	57.337
%12177385.00	55.295	55.571	55.692	55.643	55.402	54.952
%12178045.00	53.198	53.425	53.508	53.436	53.200	52.792
%12178705.00	51.247	51.433	51.489	51.407	51.182	50.813
%12179365.00	49.428	49.580	49.616	49.531	49.321	48.986
%12180025.00	47.727	47.853	47.874	47.788	47.593	47.289
%12180685.00	46.135	46.238	46.248	46.163	45.982	45.706
%12181345.00	44.638	44.723	44.725	44.642	44.474	44.222
%12182005.00	43.228	43.298	43.293	43.213	43.057	42.826
%12182665.00	41.896	41.953	41.944	41.867	41.721	41.509
%12183325.00	40.635	40.682	40.669	40.594	40.459	40.263
%12183985.00	39.438	39.477	39.460	39.389	39.262	39.081
%12184645.00	38.300	38.331	38.313	38.244	38.125	37.957
%12185305.00	37.216	37.241	37.220	37.154	37.043	36.886
%12185965.00	36.181	36.201	36.179	36.115	36.010	35.864
%12186625.00	35.191	35.207	35.184	35.123	35.023	34.886
%12187285.00	34.244	34.255	34.232	34.173	34.079	33.950
%12187945.00	33.335	33.343	33.319	33.262	33.173	33.052
%12188605.00	32.462	32.468	32.443	32.389	32.304	32.190
%12189265.00	31.623	31.626	31.601	31.549	31.469	31.361
%12189925.00	30.815	30.816	30.792	30.741	30.665	30.563
%12190585.00	30.037	30.036	30.012	29.963	29.890	29.794
%12191245.00	29.287	29.284	29.260	29.213	29.143	29.052
%12191905.00	28.562	28.558	28.534	28.488	28.422	28.335
%12192565.00	27.861	27.857	27.833	27.789	27.725	27.643
%12193225.00	27.184	27.179	27.155	27.112	27.052	26.973
%12193885.00	26.529	26.523	26.499	26.458	26.400	26.325

Y [ft] <- X [ft] ->

	1096552	1097212	1097872	1098532	1099192	1099852
%12194545.00	25.894	25.887	25.864	25.824	25.769	25.697
%12195205.00	25.279	25.271	25.249	25.210	25.157	25.088
%12195865.00	24.682	24.674	24.652	24.615	24.564	24.498
%12196525.00	24.103	24.095	24.073	24.037	23.988	23.925
%12197185.00	23.541	23.533	23.511	23.477	23.429	23.369
%12197845.00	22.996	22.987	22.966	22.932	22.886	22.829
%12198505.00	22.465	22.456	22.435	22.403	22.359	22.304

Y [ft] <- X [ft] ->

	1100512	1101172	1101832	1102492	1103152	1103812
%12153625.00	34.737	34.448	34.142	33.819	33.479	33.125
%12154285.00	35.352	35.059	34.747	34.415	34.067	33.701
%12154945.00	35.992	35.693	35.373	35.033	34.674	34.297
%12155605.00	36.658	36.353	36.025	35.674	35.303	34.913
%12156265.00	37.353	37.040	36.702	36.340	35.955	35.551
%12156925.00	38.078	37.756	37.407	37.032	36.632	36.211
%12157585.00	38.836	38.504	38.142	37.752	37.336	36.896
%12158245.00	39.630	39.286	38.910	38.503	38.067	37.606
%12158905.00	40.464	40.106	39.713	39.286	38.829	38.344
%12159565.00	41.340	40.966	40.553	40.104	39.623	39.111
%12160225.00	42.262	41.870	41.435	40.960	40.450	39.909
%12160885.00	43.235	42.821	42.360	41.857	41.315	40.739
%12161545.00	44.264	43.825	43.334	42.797	42.218	41.603
%12162205.00	45.354	44.885	44.359	43.783	43.162	42.502
%12162865.00	46.510	46.007	45.442	44.821	44.151	43.440
%12163525.00	47.740	47.197	46.585	45.912	45.187	44.417
%12164185.00	49.052	48.462	47.796	47.063	46.272	45.434
%12164845.00	50.454	49.811	49.082	48.278	47.411	46.494
%12165505.00	51.958	51.253	50.450	49.563	48.606	47.597
%12166165.00	53.576	52.801	51.912	50.925	49.862	48.743
%12166825.00	55.327	54.472	53.481	52.374	51.180	49.929
%12167485.00	57.235	56.291	55.176	53.918	52.563	51.153
%12168145.00	59.338	58.298	57.025	55.572	54.010	52.403
%12168805.00	61.703	60.562	59.070	57.343	55.509	53.659
%12169465.00	64.466	63.214	61.366	59.229	57.031	54.884
%12170125.00	67.960	66.536	63.943	61.174	58.509	56.018
%12170785.00	73.264	70.984	66.591	63.017	59.824	56.971
%12171445.00	74.707	72.998	68.715	64.539	60.817	57.633
%12172105.00	73.364	73.697	71.077	65.525	61.276	57.882
%12172765.00	72.605	73.214	71.172	65.148	60.959	57.629
%12173425.00	71.062	69.308	66.823	63.292	59.886	56.896
%12174085.00	68.499	66.174	63.794	61.118	58.390	55.813
%12174745.00	65.170	63.246	61.191	58.991	56.735	54.527

Y [ft] <- X [ft] ->

	1100512	1101172	1101832	1102492	1103152	1103812
%12175405.00	61.965	60.475	58.776	56.942	55.039	53.137
%12176065.00	59.114	57.920	56.517	54.976	53.355	51.706
%12176725.00	56.579	55.586	54.410	53.102	51.709	50.272
%12177385.00	54.295	53.449	52.447	51.323	50.116	48.856
%12178045.00	52.214	51.482	50.615	49.640	48.584	47.472
%12178705.00	50.301	49.659	48.901	48.046	47.115	46.129
%12179365.00	48.530	47.962	47.292	46.537	45.710	44.830
%12180025.00	46.881	46.374	45.778	45.105	44.367	43.577
%12180685.00	45.338	44.883	44.350	43.746	43.083	42.370
%12181345.00	43.888	43.478	42.998	42.454	41.855	41.209
%12182005.00	42.523	42.151	41.716	41.223	40.679	40.092
%12182665.00	41.232	40.893	40.497	40.048	39.553	39.016
%12183325.00	40.009	39.699	39.337	38.927	38.473	37.981
%12183985.00	38.847	38.562	38.230	37.854	37.437	36.985
%12184645.00	37.740	37.478	37.172	36.826	36.442	36.025
%12185305.00	36.685	36.443	36.160	35.840	35.486	35.100
%12185965.00	35.677	35.452	35.190	34.894	34.565	34.207
%12186625.00	34.712	34.503	34.260	33.984	33.679	33.346
%12187285.00	33.788	33.592	33.366	33.109	32.825	32.514
%12187945.00	32.900	32.718	32.506	32.266	32.001	31.711
%12188605.00	32.047	31.876	31.678	31.454	31.205	30.934
%12189265.00	31.227	31.066	30.880	30.670	30.437	30.182
%12189925.00	30.436	30.285	30.110	29.913	29.694	29.454
%12190585.00	29.674	29.531	29.367	29.181	28.975	28.749
%12191245.00	28.938	28.804	28.648	28.473	28.279	28.066
%12191905.00	28.228	28.100	27.954	27.788	27.605	27.404
%12192565.00	27.541	27.420	27.281	27.125	26.951	26.762
%12193225.00	26.876	26.762	26.630	26.482	26.318	26.138
%12193885.00	26.232	26.124	25.999	25.858	25.703	25.532
%12194545.00	25.609	25.506	25.387	25.253	25.106	24.944
%12195205.00	25.004	24.906	24.793	24.666	24.526	24.372
%12195865.00	24.418	24.324	24.217	24.096	23.962	23.816
%12196525.00	23.849	23.759	23.657	23.542	23.414	23.275
%12197185.00	23.296	23.210	23.113	23.003	22.882	22.749
%12197845.00	22.759	22.677	22.584	22.479	22.363	22.237
%12198505.00	22.237	22.158	22.069	21.969	21.859	21.738

Y [ft] <- X [ft] ->

	1104472	1105132	1105792	1106452	1107112
%12153625.00	32.756	32.374	31.981	31.577	31.163
%12154285.00	33.321	32.927	32.520	32.102	31.673
%12154945.00	33.904	33.496	33.074	32.640	32.196
%12155605.00	34.505	34.082	33.644	33.193	32.732

Y [ft]	<- X [ft] ->				
	1104472	1105132	1105792	1106452	1107112
%12156265.00	35.127	34.686	34.231	33.761	33.281
%12156925.00	35.769	35.310	34.834	34.345	33.844
%12157585.00	36.434	35.954	35.456	34.944	34.420
%12158245.00	37.122	36.618	36.096	35.560	35.011
%12158905.00	37.835	37.305	36.756	36.192	35.615
%12159565.00	38.574	38.014	37.435	36.841	36.234
%12160225.00	39.340	38.747	38.134	37.506	36.866
%12160885.00	40.133	39.504	38.854	38.189	37.512
%12161545.00	40.957	40.285	39.594	38.887	38.170
%12162205.00	41.810	41.092	40.354	39.601	38.839
%12162865.00	42.695	41.924	41.133	40.330	39.518
%12163525.00	43.612	42.781	41.931	41.070	40.205
%12164185.00	44.561	43.661	42.745	41.821	40.896
%12164845.00	45.541	44.563	43.573	42.578	41.587
%12165505.00	46.551	45.485	44.410	43.337	42.275
%12166165.00	47.590	46.421	45.251	44.092	42.952
%12166825.00	48.650	47.364	46.087	44.833	43.609
%12167485.00	49.724	48.303	46.908	45.551	44.238
%12168145.00	50.797	49.223	47.698	46.231	44.825
%12168805.00	51.846	50.101	48.436	46.855	45.357
%12169465.00	52.836	50.907	49.098	47.404	45.816
%12170125.00	53.717	51.601	49.653	47.854	46.186
%12170785.00	54.424	52.138	50.070	48.183	46.449
%12171445.00	54.884	52.470	50.315	48.368	46.590
%12172105.00	55.030	52.557	50.365	48.394	46.599
%12172765.00	54.822	52.379	50.209	48.254	46.472
%12173425.00	54.274	51.945	49.852	47.951	46.210
%12174085.00	53.448	51.290	49.315	47.499	45.822
%12174745.00	52.428	50.462	48.628	46.919	45.323
%12175405.00	51.284	49.510	47.825	46.233	44.730
%12176065.00	50.071	48.476	46.938	45.465	44.059
%12176725.00	48.825	47.393	45.994	44.637	43.329
%12177385.00	47.572	46.286	45.014	43.768	42.555
%12178045.00	46.328	45.171	44.014	42.871	41.749
%12178705.00	45.105	44.061	43.009	41.960	40.922
%12179365.00	43.910	42.965	42.006	41.043	40.084
%12180025.00	42.747	41.889	41.013	40.128	39.241
%12180685.00	41.619	40.837	40.035	39.221	38.400
%12181345.00	40.525	39.812	39.076	38.325	37.564
%12182005.00	39.468	38.814	38.137	37.443	36.738

Y [ft]	<- X [ft] ->				
	1104472	1105132	1105792	1106452	1107112
%12182665.00	38.445	37.844	37.220	36.578	35.923
%12183325.00	37.456	36.903	36.326	35.731	35.122
%12183985.00	36.501	35.990	35.456	34.903	34.335
%12184645.00	35.578	35.104	34.609	34.094	33.564
%12185305.00	34.685	34.246	33.785	33.305	32.810
%12185965.00	33.822	33.414	32.984	32.536	32.072
%12186625.00	32.988	32.607	32.205	31.786	31.352
%12187285.00	32.180	31.824	31.448	31.056	30.648
%12187945.00	31.398	31.065	30.713	30.344	29.961
%12188605.00	30.641	30.328	29.998	29.652	29.291
%12189265.00	29.907	29.614	29.303	28.977	28.637
%12189925.00	29.196	28.920	28.627	28.320	27.999
%12190585.00	28.506	28.246	27.970	27.680	27.377
%12191245.00	27.837	27.591	27.331	27.057	26.770
%12191905.00	27.187	26.955	26.709	26.450	26.178
%12192565.00	26.557	26.337	26.104	25.858	25.601
%12193225.00	25.944	25.736	25.515	25.282	25.037
%12193885.00	25.348	25.151	24.941	24.720	24.488
%12194545.00	24.769	24.582	24.383	24.173	23.952
%12195205.00	24.206	24.028	23.839	23.639	23.429
%12195865.00	23.658	23.489	23.309	23.118	22.918
%12196525.00	23.125	22.964	22.792	22.610	22.420
%12197185.00	22.606	22.452	22.288	22.115	21.933
%12197845.00	22.100	21.953	21.797	21.632	21.458
%12198505.00	21.607	21.467	21.318	21.160	20.994